

APPENDIX D

Wetland Mitigation Details



**Wetland Mitigation Specifications and Drawing Notes**  
**Courtyard at Upper Nyack**  
February 1, 2005

The mitigation site for impacts to regulated wetlands at the Courtyard at Upper Nyack proposal is an upland/wetland buffer area and existing detention basin on a separate parcel on the west side of Route 9W, directly across from the project site.

A wetland mitigation plan was prepared. This plan shows expanded wetlands and creation of new wetland areas adjacent to an existing detention basin. In total, this plan will add an additional 0.54 acres of wetland. An additional 0.23 acres is proposed to the east of Route 9W on the project site. This area is intended to offset the loss of 0.49 acres due to the proposed development.

The mitigation concept for the proposed Courtyard at Upper Nyack property is to regrade a portion of the hill on the west side of Route 9W to create a series of depressional areas that will pick up runoff and hillside seepage. This site is owned by the Christian Theological Alliance, but the applicant has reached an agreement with the owners to utilize a portion of the property for wetland mitigation. Considering the runoff from the adjacent property to the south and the long slope from the Christian Alliance building, this will provide enough regular input of water to saturate the area and promote the growth of wetland tolerant plants. All of the species shown on the list will tolerate wet conditions, and have also been chosen to be attractive to people and wildlife.

Soil erosion and sediment control fencing will be installed at the outer and down slope limits of the proposed wetland expansion. The location of the proposed wetland will be cleared as necessary, but with an eye toward preserving large trees to the extent possible. Some trees will be removed due to an inability to survive the future inundations. Other trees, specifically the large elms, will be preserved since periodic inundation is typical for this species. Vegetative materials will be hauled to the general construction stockpile areas for recycling on site or for off-site disposal.

Where available, the upper one foot of topsoil will be stripped from the site and set aside from other site grading materials. The temporary storage area will be an upland site either removed from wetlands by 100 feet, within other areas cleared for site development and/or separated from same by a soil erosion and sediment control fence. The topsoil material will be free from all stones larger than 3 inches and any recognizable vegetative materials exceeding one foot in length.

All excavations will be to finished grade elevations as indicated in the mitigation drawings. Per the above, topsoil will be stripped from the site and stockpiled for use in finishing grading.

All grading efforts will proceed from one edge backward to the far edge. To gain access for topsoil placement, such material will be used to create temporary "roadways" at least one foot deep and the topsoil spread laterally from such access locations. Only tracked equipment will be used and always on a minimum of one foot of material. The contractor will notify the property owner's and Village's engineer/environmental monitor, who will make an inspection of the soil and hydrological conditions prior to the topsoil placement work. The stockpiled topsoil will be returned to the site to create a planting surface for

the wetland mitigation as described above. Finished soils at the invert of the mitigation sites will be of landscape quality.

The planting area associated with the mitigation proposal will receive an application of lime several weeks to one month prior to planting. The finished surfaces will be smooth within specified tolerances in uniform levels or slopes between points where elevations are indicated or between such point and existing grades. The accepted grading tolerance will be a smooth and even surface, free of voids, and within 0.25 feet of the specified elevation. During the course of earthwork, inspections will be schedule at a frequency to be determined by the engineer/environmental consultant but no less than weekly.

Any deviation from this grading specification will be obtained in writing from the Office of the Village Engineer and Tim Miller Associates.

***Planting Details***

Planting specifications for the mitigation wetland were defined according to the newly graded elevations within each wetland. Mitigation areas were designed in some instances to have low-lying depression areas that will retain shallow open water habitat and a surrounding flat emergent habitat. All wetland planting (except for the outer edges) will proceed by hand. Materials will be brought to the site in good condition (see below) and then placed in central drop locations. The materials will then be hand-carried to their planting locations and in turn, planted by hand. Only rounded, shallow planting shovels will be used in this effort.

Criteria for selecting plant material included (1) the plant's ability to withstand saturation and inundation; (2) its demonstrated survival on this site and other nearby sites; (3) its successful establishment in other wetland replacement projects; (4) the plant must be native and non-invasive; and (5) whether the plant material is available at nurseries in the same region as the site. See Table 1 for complete plant species list.

| <b><i>Table 1</i></b>                          |                          |                        |
|------------------------------------------------|--------------------------|------------------------|
| <b><i>WETLAND MITIGATION PLANTING LIST</i></b> |                          |                        |
| SD                                             | Salix discolor           | Pussy Willow           |
| CSe                                            | Cornus sericea           | Redosier dogwood       |
| CR                                             | Cornus amomum            | Silky Dogwood          |
| JE                                             | Juncus effuses           | Soft rush              |
| IV                                             | Ilex verticillata        | Winterberry holly      |
| ST                                             | Scirpus tabernaemontanii | Softstem bulrush       |
| ARu                                            | Acer rubrum              | Red Maple              |
| VC                                             | Vaccinium corymbosum     | High bush blueberry    |
| VT                                             | Viburnum trilobum        | American cranberrybush |
| CS                                             | Carex stricta            | Tussock sedge          |
| VD                                             | Viburnum dentatum        | Arrowwood              |
| ASe                                            | Alnus serrulata          | Speckled alder         |
| <i>Source: Tim Miller Associates, Inc.</i>     |                          |                        |

It must be noted that field adjustments are always necessary in these types of projects, and although the plant quantities will not change, their exact location in the field may change based on final grading and site conditions.

Once the appropriate planting locations are cleared and excavated, the planting bed will be prepared. This will include the addition of approximately six inches of the topsoil layer that was either previously removed and stockpiled or imported to the site. This layer will provide a nutrient-rich environment in which to plant peat pots, seedlings (plugs) and saplings.

Planting will be done in spring or early summer (between April 1 and July 1). Shrubs may also be planted in the late summer to early fall (September 1 to October 30). In all cases, a hole will be dug twice as deep as either the peat pot or root ball. The only shovels allowed are rounded, shallow spades. A small amount of slow release, (10-5-5 or equivalent) fertilizer will be placed in each hole. The hole will then be backfilled with a thin layer of rich, organic topsoil, the plant placed inside, the hole backfilled to the top and then gently tamped down. Trees will be planted on 12 to 15 foot centers and alternated with shrubs on 6 foot centers. Herbaceous species will be planted in clumps of 2 to 3 individuals on 3 foot centers.

Fiber or peat pots will be either planted immediately after being delivered to the job site or stored in a secure, central location. If stored before planting, they will be out of direct exposure to the sun and wind and kept moist until the time for planting (i.e., a means of watering will be provided and watering will occur daily). Plants will be well rooted through the sides and bottoms of peat pots, and firmly contained therein. Herbaceous species will have three stems per pot; shrubs will be erect and 3 -4 feet tall. Plugs will also be planted immediately upon delivery. If this is not possible, they will be stored out of direct exposure to the sun and wind and kept moist (i.e., a means of watering will then be provided and watering will occur daily). The plugs will have solid soil/root masses with the soil in place and the roots will appear clean and white in coloration. Plugs containing shoots that are soft and mushy or appear otherwise rotten and stems that are brittle will not be accepted. Plug cell size will not be less than 1.25 by 1.25 inches.

Container-grown plant material delivered to the job site will be inspected to assure moist soil/root masses. Any dry and light weight plants will not be accepted. As with peat pots and plugs, if not planted immediately the container will be stored out of the sun and wind and kept moist (i.e., a means of watering then will be provided and watering will occur daily). When removed from the containers, the plants will be the size of the specified container. If in leaf, the plants will appear healthy with no spots, leaf damage, discoloration, insects or fungus. If not in leaf, the buds will be firm and free of damage, discoloration, insects or fungus. Containers will be a minimum of quart size for shrubs and gallon size for trees. The contractor/inspector will not and follow the added size specification in that area.

Bare roots plants will be shipped from the nursery immediately after lifting from the field and will be planted immediately upon arrival at the site. If they cannot be planted as soon as arriving at the site, they will be stored in the shade, protected from sun and wind, and kept moist by the use of straw, peat moss, compost, or other suitable materials. Plants not having an abundance of well developed terminal buds on the leaders and branches will be rejected. The stems and branches of all plants will be

turgid and the cambium healthy or the plants rejected. Any bare root plants that are in leaf or have leaflets will be rejected.

Stockpiled hydric soils stripped from filled wetland areas on site will be used as appropriate to provide an organic topsoil in areas where re-grading leaves sandy subsoils on the surface. This will also provide a seedbank from existing site plants for natural re-vegetation of mitigation areas. Healthy trees located in the mitigation areas that have a wetland indicator status of FAC or FACW (common wooded wetland species) will be preserved where possible, including red maple, American elm, and green ash. Wetland tolerant shrub species that are common on the site, including spicebush, witch hazel and winterberry will be planted under the remaining canopy as necessary. Other northeast species that are not common on this site but provide wildlife and aesthetic values will also be used, including highbush blueberry, American cranberrybush, arrowwood and wild raisin.

### ***Monitoring and Maintenance***

At least one pre-construction meeting will occur between the chosen grading and/or planting contractor/subcontractor and the site environmental monitor prior to beginning construction (a) on site and (b) on the mitigation site. Monitoring during active construction will take place daily on the first three to seven days and then on a weekly basis thereafter. One to three days of daily inspection will re-occur at the beginning of grading, construction, final grading and placement of topsoil, fertilization of the planting surface, planting delivery and beginning of the planting. The construction monitor will have experience in wetland construction and a Bachelor of Science degree in Natural and/or Physical Resources.

Monitoring and maintenance efforts for the mitigation wetlands will take place over a three year period following construction, and thereafter as needed depending on the results of the initial monitoring. This will include bi-weekly visits for the first growing season, and then twice a year for the next two years, with additional inspections as required depending on conditions. The applicant's environmental monitor will conduct a survey of the site and site conditions will be noted and adjusted as necessary.

### ***Monitoring Reports***

Monitoring will be based on the target objectives established for the wetland creation/pond expansion area. Hydrology, vegetation and observed functions will be documented and reported on twice annually for the first two years following construction and annually for the remaining three years unless released from this requirement by the reviewing agencies. The natural vegetation, provision of wildlife habitat, and nutrient uptake processes that the basin is designed to support will be monitored annually through simple observation of the new wetlands. Photographs of the mitigation areas will be taken at least once per year during the growing season (July and August are preferred times from established photo stations). Inspection of the new wetlands will include assessment of:

1. Percent vegetative cover of the wetland by submerged and emergent vegetation; percent of vegetative cover in the shrub planting areas. A vegetative cover of at least 80 percent total coverage with 70 percent species survival will be achieved in all created wetlands by the end of the second

growing season. The percent coverage and any need for replacement plantings shall include consideration for any native wetland species which have "volunteered" onto the site. When this criteria is met it will be assumed that nutrient uptake is high, based on biomass and plant success.

2. Percent of shrub species plantings that produce flowers and fruits during each growing season. By the end of the first full growing season, 25 percent of the fruiting species will have bloomed and produced fruit. By the end of the second growing season, the survival will be up to 50 percent.
3. Percent cover of exotic invasive species (Purple loose strife or Common reed) within the wetlands. Invasive species shall be removed by hand when observed, or selectively treated with a general herbicide by a qualified wetland professional during the appropriate season.
4. Survival of planted species will be calculated, with a mitigation goal of at least 75 percent of the species planted.
5. Use of the wetland and its surrounding shrub plantings by songbird species, amphibians, and reptiles will be noted. Evidence of wetland dependent mammals will also be noted. Coarse woody debris (logs and branches) may be left within the mitigation wetlands to provide additional habitat.

Wetland monitoring data forms (attached) will be filled out for each monitoring plot within the created wetland during each inspection. Copies of the Wetland Monitoring Data Forms will be submitted to the Village after completion. Inspections will be summarized in an annual report, including photographs, which shall be submitted to the regulatory agencies. Field changes to grading within the wetland, replanting, or modifications to the hydrology within the wetland will be reviewed by the appropriate regulatory agencies and described in the annual report.



**Plan Notes**

1. Nuisance and non-native vegetation will be removed, including phragmites, multi-floral rose, ailanthus.
2. Dumped material and debris will be removed from remaining wetland and mitigation area, and area brought to specified grade with four to six inches of topsoil.
3. All red maple and American elm trees in mitigation area greater than 4 inches in diameter will be preserved.
4. Wetland seed mix will be used as specified to supplement plantings at a rate of 2 pounds per acre. One pound of seed will be used for this site.
5. The area chosen for mitigation is generally a depressional area along Route 9W with occasional stream overflow. Hydrology will be provided by seasonal high groundwater, groundwater seepage under Route 9W, occasional flooding of the adjacent watercourse, and normal precipitation.

TL 59.20-2-1  
IPLE BETH TORAH, INC.



**Grading Plan**  
 On-site Wetland Mitigation Plan  
 prepared for  
**Courtyard at Upper Nyack**  
 Village of Upper Nyack, NY  
 Prepared by:  
 Tim Miller Associates, Inc.  
 12/13/04 Scale 1" = 30'



**Plant List**

- AC - Amelanchier canadensis (shadblow)
- Aru - Acer rubrum (red maple)
- Ase - Alnus serrulata (speckled alder)
- CA - Clethra alnifolia (summersweet)
- Cse - Cornus sericea (redosier dogwood)
- SD - Salix discolor (pussy willow)
- VC - Vaccinium corymbosum (highbush blueberry)
- VD - Viburnum dentatum (arrowwood)

- Mh1 - Mixed herbaceous including Scirpus tabernaemontanii, Juncus effusus and Carex stricta
- Mh2 - Mixed herbaceous including Carex stricta, Carex crinita and Onoclea sensibilis
- Mh3 - Mixed herbaceous including Symplocarpus foetidus, Carex stricta and Onoclea sensibilis




Other shaded areas to be seeded using Wetland Diversity Mix or equivalent.

TL 59.20-2-1  
IPLC BETH TORAH, INC.



**Planting Plan**  
 On-site Wetland Mitigation Plan  
 prepared for  
**Courtyard at Upper Nyack**  
 Village of Upper Nyack, NY  
 Prepared by:  
 Tim Miller Associates, Inc.  
 12/13/04 Scale 1" = 30'

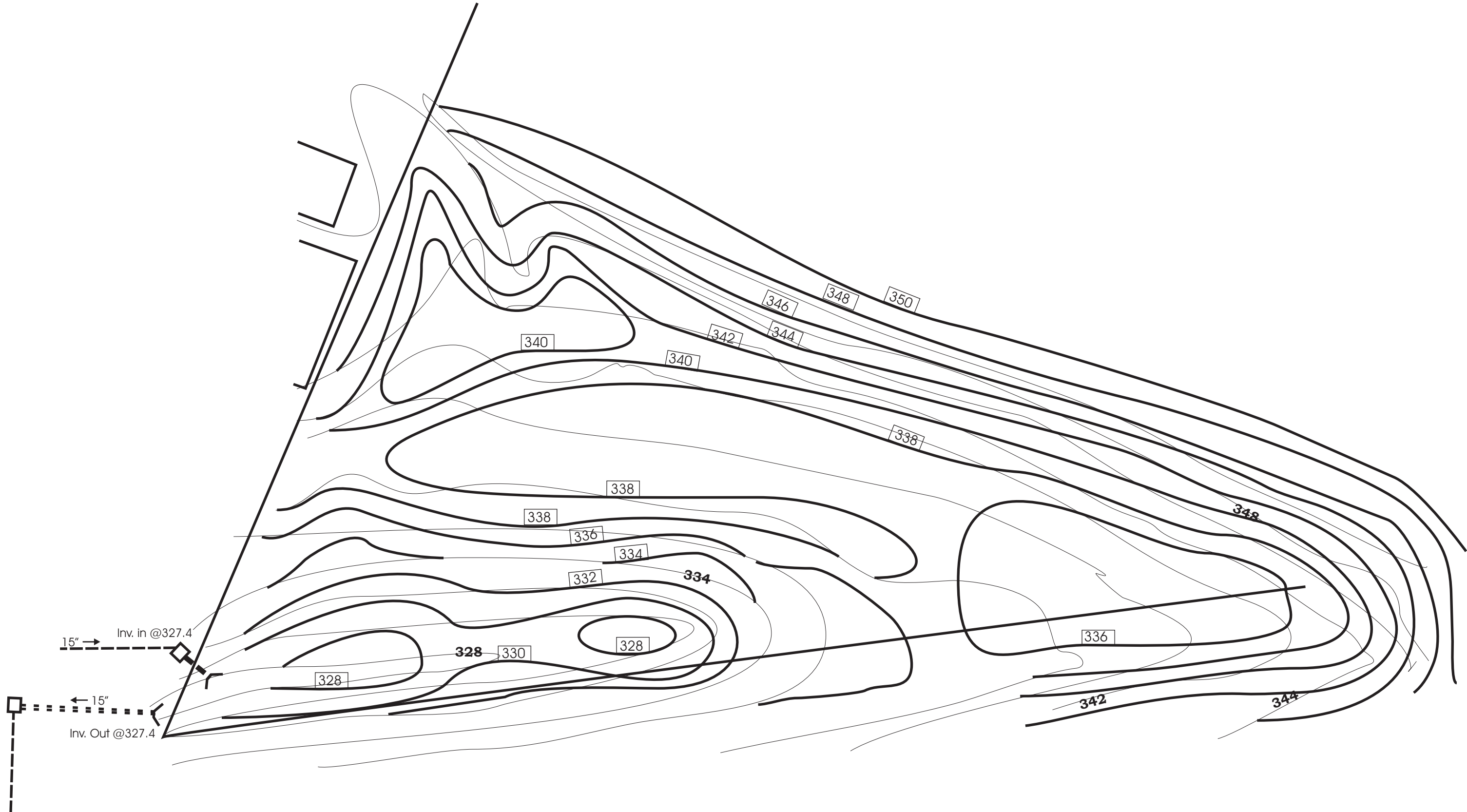


-  New Tree
-  Shrub Mass
-  Herbaceous plantings



Location of Wetland Mitigation Proposal  
 Courtyard at Upper Nyack  
 Village of Upper Nyack, Rockland County  
 N.T.S.





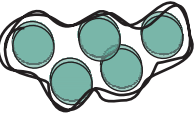



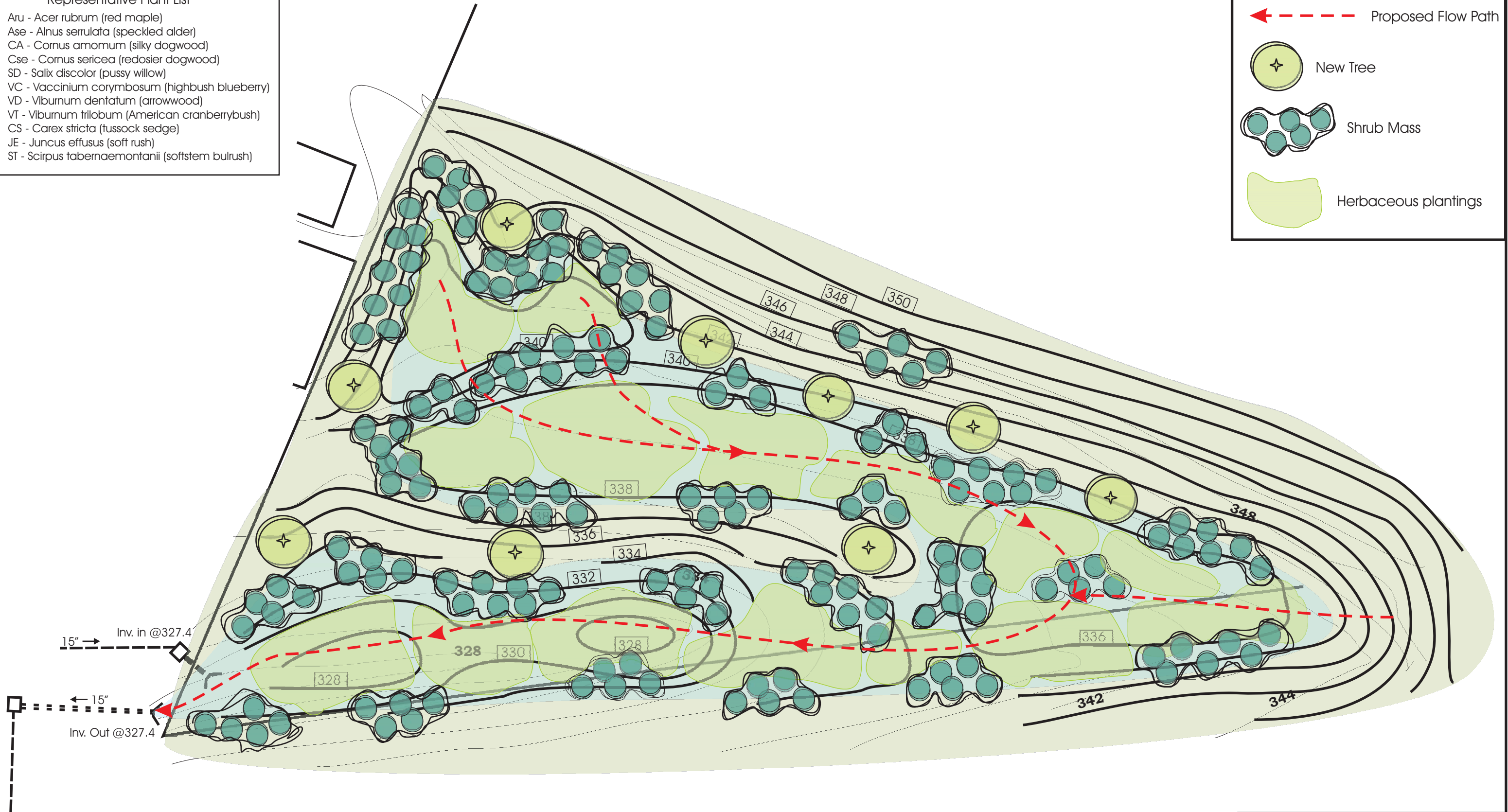
The Courtyard at Upper Nyack  
Wetland Mitigation Plan  
Proposed Grading  
Dated 2/18/04, rev. 8/24/04  
prepared by  
Tim Miller Associates, Inc.



Representative Plant List

- Aru - Acer rubrum (red maple)
- Ase - Alnus serrulata (speckled alder)
- CA - Cornus amomum (silky dogwood)
- Cse - Cornus sericea (redosier dogwood)
- SD - Salix discolor (pussy willow)
- VC - Vaccinium corymbosum (highbush blueberry)
- VD - Viburnum dentatum (arrowwood)
- VT - Viburnum trilobum (American cranberrybush)
- CS - Carex stricta (tussock sedge)
- JE - Juncus effusus (soft rush)
- ST - Scirpus tabernaemontanii (softstem bulrush)

-  Proposed Flow Path
-  New Tree
-  Shrub Mass
-  Herbaceous plantings



The Courtyard at Upper Nyack  
 Wetland Mitigation Plan  
 Proposed Planting Plan  
 Dated 2/18/04, rev. 8/24/04  
 prepared by  
 Tim Miller Associates, Inc.



APPENDIX E

Supplemental Traffic Analysis



## Appendix E: Supplemental Traffic Analysis

Some of the road grades used in the DEIS intersection analysis were not correct, and therefore, were reexamined for the FEIS to review the relative sensitivity of the grade corrections. Road grade is one of the less important variables in capacity analysis. The capacity analyses of intersections have numerous inputs to calculate volume to capacity ratios, delays, and levels of service at intersections. Some of these data requirements for unsignalized intersections analysis include:

- Number of lanes
- Grades (not an input for all way stop controlled intersections)
- Lane use (movements permitted by lane)
- Demand volume (traffic for each movement)
- Base saturation flow rate
- Peak hour factor (establishes 15 minute traffic flow)
- Percent of heavy vehicles of traffic

Signalized intersections have further requirements for example:

- Arrival type (degree of signal coordination)
- Cycle length (time before signal phases repeat)
- Green time (by lane group)
- Clearance interval (yellow plus all red)
- Phase operation type (pretimed, or actuated)
- Phase plan (what movements occur simultaneously)

Road grade primarily effects vehicle startup from stopped conditions. The more the grade slopes down toward the intersection, the faster a vehicle can accelerate from a stop or a queue can accelerate, hence the less the vehicle delay. Road grades do not change from Existing to Build Condition unless there is an improvement project being constructed, which is not the case herein. As such, the relative effect of altering the road grades in calculations is reduced because the analyses tends to alter delay in all conditions in the same direction. For example, if the No Build Condition delay is increased, then Build delay will remain the same or increase.

For a two way stop controlled intersection, road grades apply in the capacity analysis to the minor approach (the approach in which traffic stops) and lanes with left turning traffic, whose traffic stops to yield right of way to major street through traffic. Stopping is determined by the rules of the road in the absence of a stop sign. For example, the site driveway will be the minor approach as traffic from driveways must yield to traffic already on a state highway in the absence of traffic controls reassigning this priority.

Because the two way stopped control (unsignalized) intersections on Route 9W that were analyzed in the DEIS traffic analysis operate at levels of service A or B, re-analysis of these intersections utilizing field check grades was not done. The all way stop controlled intersections do not use road grades as a variable in the capacity analysis and, thus, these intersections were also not reanalyzed.

The Highmount Avenue/Route 9W intersection with levels of service D would have reduced delays as the minor approach grade is 3 percent lower than assumed in the DEIS. The 6th

## **Appendix E: Supplemental Traffic Analysis**

Avenue/Route 9W intersection with levels of service D and E has no grade change and thus the levels of service would remain unchanged. The state requires a low reverse grade at driveways to the state roads so the site driveway grade should remain nearly the same as shown in the DEIS. Thus for these intersections on Route 9W, no grade change was reanalyzed.

For signalized intersections all movements are affected by grade and were reanalyzed with grade changes. Below is an intersection by intersection review. Table E-1 summarizes the changes in level of service from the DEIS to the FEIS (with grade revisions). In two out of the three cases with a difference in level of service in the Build Condition, the revised level of service was better than previously indicated. In all cases the worst levels of service were already shown for at least two lane groups. Thus, the road grade change did not show levels of service previously unforeseen in the DEIS.

**Appendix E: Supplemental Traffic Analysis**

| Table E-1<br>All Condition Changes in Level of Service Summary<br>Signalized Intersections in the Village of Upper Nyack and Nyack |                                             |                    |          |                |          |                    |          |                |          |                 |          |                |          |
|------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------|--------------------|----------|----------------|----------|--------------------|----------|----------------|----------|-----------------|----------|----------------|----------|
| Intersection Roads                                                                                                                 | Lane Group<br>(Approach Direction-Movement) | Existing Condition |          |                |          | No Build Condition |          |                |          | Build Condition |          |                |          |
|                                                                                                                                    |                                             | A.M. Peak Hour     |          | P.M. Peak Hour |          | A.M. Peak Hour     |          | P.M. Peak Hour |          | A.M. Peak Hour  |          | P.M. Peak Hour |          |
|                                                                                                                                    |                                             | DEIS LOS           | FEIS LOS | DEIS LOS       | FEIS LOS | DEIS LOS           | FEIS LOS | DEIS LOS       | FEIS LOS | DEIS LOS        | FEIS LOS | DEIS LOS       | FEIS LOS |
| <b>US Route 9W and Christan Herald Rd.</b>                                                                                         |                                             |                    |          |                |          |                    |          |                |          |                 |          |                |          |
| Christan Herald Rd.                                                                                                                | EB-L,T,R                                    | C                  | C        | B              | B        | D*                 | D*       | C*             | B        | D               | D        | C              | C*       |
|                                                                                                                                    | WB-L,T,R                                    | B                  | B        | C              | C        | B                  | B        | C              | C        | B               | B        | C              | C        |
| US Route 9W                                                                                                                        | NB-L,T,R                                    | B                  | B        | B              | B        | B                  | C*       | C*             | C*       | C*              | C        | C              | C        |
|                                                                                                                                    | SB-L,T,R                                    | C                  | C        | B              | B        | C                  | C        | C*             | C*       | D*              | D*       | C              | C        |
|                                                                                                                                    | Overall                                     | C                  | C        | B              | B        | C                  | C        | C*             | C*       | D*              | C        | C              | C        |
| <b>US Route 9W and Birchwood Ave.</b>                                                                                              |                                             |                    |          |                |          |                    |          |                |          |                 |          |                |          |
| Birchwood Avenue<br>US Route 9W                                                                                                    | WB-L,R                                      | B                  | B        | B              | B        | B                  | B        | B              | B        | B               | B        | B              | B        |
|                                                                                                                                    | NB-T,R                                      | A                  | A        | B              | B        | A                  | A        | B              | B        | A               | A        | B              | B        |
|                                                                                                                                    | SB-L,T                                      | B                  | B        | B              | B        | B                  | B        | B              | B        | B               | B        | B              | B        |
|                                                                                                                                    | Overall                                     | B                  | B        | B              | B        | B                  | B        | B              | B        | B               | B        | B              | B        |
| <b>US Route 9W and High Avenue</b>                                                                                                 |                                             |                    |          |                |          |                    |          |                |          |                 |          |                |          |
| High Avenue                                                                                                                        | EB-L,T,R                                    | B                  | B        | B              | B        | C*                 | C*       | C*             | C*       | C               | C        | C              | C        |
|                                                                                                                                    | WB-L,T,R                                    | B                  | B        | B              | B        | B                  | B        | B              | B        | B               | B        | B              | B        |
| US Route 9W                                                                                                                        | NB-L                                        | B                  | B        | B              | B        | B                  | B        | B              | B        | B               | B        | B              | B        |
|                                                                                                                                    | NB-T,R                                      | B                  | B        | B              | B        | B                  | C*       | B              | C*       | C*              | C        | C*             | C        |
| US Route 9W                                                                                                                        | SB-L,T,R                                    | C                  | C        | B              | B        | C                  | C        | B              | B        | C               | C        | C*             | B        |
|                                                                                                                                    | Overall                                     | B                  | B        | B              | B        | C*                 | C*       | B              | B        | C               | C        | C*             | C*       |
| <b>US Route 9W and Main Street</b>                                                                                                 |                                             |                    |          |                |          |                    |          |                |          |                 |          |                |          |
| Main Street                                                                                                                        | EB-L                                        | D                  | D        | E              | E        | D                  | D        | F*             | F*       | E*              | E*       | F              | F        |
|                                                                                                                                    | EB-T,R                                      | D                  | D        | C              | C        | D                  | D        | C              | C        | D               | D        | C              | C        |
| Main Street                                                                                                                        | WB-L                                        | C                  | C        | D              | D        | D*                 | D*       | F*             | F*       | D               | D        | F              | F        |
|                                                                                                                                    | WB-T,R                                      | C                  | C        | E              | E        | C                  | C        | E              | F*       | C               | C        | E              | F        |
| US Route 9W                                                                                                                        | NB-L                                        | D                  | D        | D              | D        | D                  | D        | E*             | D        | D               | D        | E              | E*       |
|                                                                                                                                    | NB-T,R                                      | C                  | C        | D              | D        | C                  | C        | D              | D        | C               | C        | D              | D        |
| US Route 9W                                                                                                                        | SB-L                                        | C                  | C        | C              | C        | C                  | C        | C              | C        | C               | C        | C              | C        |
|                                                                                                                                    | SB-T,R                                      | D                  | D        | D              | D        | D                  | D        | D              | E*       | D               | D        | E*             | E        |
| Overall                                                                                                                            | D                                           | D                  | D        | D              | D        | D                  | D        | E*             | E*       | D               | D        | E              | E        |

LOS = Level of Service (see Table 3.7-8 for level-of-service criteria).  
 FEIS LOS is with grade revisions.  
 L = Left, T = Through, R = Right, (e.g. WB-L = Westbound left).  
 \*Decline in level of service from previous condition.

Levels of service shaded indicate a difference between the same conditions based on grade differences.

## Appendix E: Supplemental Traffic Analysis

### Christian Herald / Route 9W intersection

With the changes in grades, the existing levels of service remained unchanged. For the No Build Condition there were the same number of changes in level of service to C or D, however, the lane groups level of service changes were different in two instances. In these cases the delay differences between the two analyses was reduced by one second or less. Also in both cases upon reaching the Build Condition, the levels of service changed to C resulting in all the lane groups being the same levels of service under the Build Condition regardless of the grades used. Thus, for this intersection there is no difference in the Build levels of service and the change in level of service was for different lane groups.

### Birchwood Avenue / Route 9W intersection

Levels of service for all conditions remained unchanged with the grade corrections, remaining at levels of service A and B. The delays varied by less than one second for each lane group with the change in grades.

### High Avenue / Route 9W intersection

Levels of service for the existing conditions were unchanged with the grade revisions. In the revised No Build condition, the northbound through right lane declines from level of service B to C, however the difference in delay was less than one second. With the grade changes there are no lane groups decline in level of service between the No Build and Build Conditions. Without the grade revision the Build Conditions catch up with declines in level of service from B to C for the northbound through right lane. However, the southbound p.m. approach does not decline to level of service C as in the DEIS. Although, the southbound level of service C without the grade change is worse than the revised level of service B the difference in delay per vehicle is a half second.

### Main Street and US Route 9W

Levels of service for the existing conditions were the same regardless of grades used. Also the a.m. peak hour levels of service remained the same regardless of the grade changes. For the No Build Conditions both analyses had the westbound and eastbound lefts declining to level of service F. The differences were in the p.m. peak hour No Build Conditions. The original analysis had the northbound left declining to level of service E while the revised southbound through-right declined to E and westbound through right to F. The differences in the level of service E changes that occurred between the Existing and No Build conditions were equalized between the No Build and Build Conditions. Thus the difference in level of service was the revised analysis had a level of service F in the westbound through right verses a level of service E. Overall the difference in vehicle delay at the intersection in the p.m. peak hour was 1.3 seconds per vehicle higher with the grade changes.

Tables E-2 through E-4 show the delay, volume to capacity ratios, and level of service for all signalized intersections with the grade revisions.

**Appendix E: Supplemental Traffic Analysis**

| Table E-2<br>Revised Existing Condition Level of Service Summary<br>Signalized Intersections in the Villages of Upper Nyack and Nyack                                                                   |                                                    |                                |                                |                     |                                |                                |                     |
|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------|--------------------------------|--------------------------------|---------------------|--------------------------------|--------------------------------|---------------------|
| Intersection<br>Road                                                                                                                                                                                    | Lane Group<br>(Approach<br>Direction-<br>Movement) | AM Weekday Peak Hour           |                                |                     | PM Weekday Peak Hour           |                                |                     |
|                                                                                                                                                                                                         |                                                    | Volume to<br>Capacity<br>Ratio | Delay<br>(seconds/<br>vehicle) | Level of<br>Service | Volume to<br>Capacity<br>Ratio | Delay<br>(seconds/<br>vehicle) | Level of<br>Service |
| <b>US RT 9W and Christan Herald Rd.</b>                                                                                                                                                                 |                                                    |                                |                                |                     |                                |                                |                     |
| Christan Herald Rd.                                                                                                                                                                                     | EB-L,T,R                                           | 0.85                           | 28.4                           | C                   | 0.59                           | 18.4                           | B                   |
|                                                                                                                                                                                                         | WB-L,T,R                                           | 0.45                           | 14.8                           | B                   | 0.69                           | 20.8                           | C                   |
| US Route 9W                                                                                                                                                                                             | NB-L,T,R                                           | 0.53                           | 18.3                           | B                   | 0.77                           | 19.3                           | B                   |
|                                                                                                                                                                                                         | SB-L,T,R                                           | 0.83                           | 27.8                           | C                   | 0.71                           | 17.3                           | B                   |
|                                                                                                                                                                                                         | Overall                                            |                                | 24.6                           | C                   |                                | 18.9                           | B                   |
| <b>US Route 9W and Birchwood Ave.</b>                                                                                                                                                                   |                                                    |                                |                                |                     |                                |                                |                     |
| Birchwood Avenue                                                                                                                                                                                        | WB-L,R                                             | 0.07                           | 15.1                           | B                   | 0.04                           | 14.9                           | B                   |
| US Route 9W                                                                                                                                                                                             | NB-T,R                                             | 0.32                           | 8.7                            | A                   | 0.66                           | 13.7                           | B                   |
|                                                                                                                                                                                                         | SB-L,T                                             | 0.66                           | 13.7                           | B                   | 0.53                           | 11.3                           | B                   |
|                                                                                                                                                                                                         | Overall                                            |                                | 12.2                           | B                   |                                | 12.7                           | B                   |
| <b>US Route 9W and High Avenue</b>                                                                                                                                                                      |                                                    |                                |                                |                     |                                |                                |                     |
| High Avenue                                                                                                                                                                                             | EB-L,T,R                                           | 0.53                           | 18.5                           | B                   | 0.58                           | 19.2                           | B                   |
|                                                                                                                                                                                                         | WB-L,T,R                                           | 0.55                           | 18.2                           | B                   | 0.38                           | 16.3                           | B                   |
| US Route 9W                                                                                                                                                                                             | NB-L                                               | 0.27                           | 12.8                           | B                   | 0.17                           | 11.8                           | B                   |
|                                                                                                                                                                                                         | NB-T,R                                             | 0.69                           | 18.2                           | B                   | 0.71                           | 18.8                           | B                   |
| US Route 9W                                                                                                                                                                                             | SB-L,T,R                                           | 0.77                           | 20.9                           | C                   | 0.61                           | 16.2                           | B                   |
|                                                                                                                                                                                                         | Overall                                            |                                | 19.0                           | B                   |                                | 17.5                           | B                   |
| <b>US Route 9W and Main Street</b>                                                                                                                                                                      |                                                    |                                |                                |                     |                                |                                |                     |
| Main Street                                                                                                                                                                                             | EB-L                                               | 0.72                           | 37.8                           | D                   | 0.85                           | 58.4                           | E                   |
|                                                                                                                                                                                                         | EB-T,R                                             | 0.71                           | 36.4                           | D                   | 0.59                           | 23.5                           | C                   |
| Main Street                                                                                                                                                                                             | WB-L                                               | 0.10                           | 33.3                           | C                   | 0.64                           | 51.6                           | D                   |
|                                                                                                                                                                                                         | WB-T,R                                             | 0.49                           | 30.6                           | C                   | 0.95                           | 69.8                           | E                   |
| US Route 9W                                                                                                                                                                                             | NB-L                                               | 0.62                           | 43.0                           | D                   | 0.68                           | 45.0                           | D                   |
|                                                                                                                                                                                                         | NB-T,R                                             | 0.36                           | 31.4                           | C                   | 0.50                           | 38.1                           | D                   |
| US Route 9W                                                                                                                                                                                             | SB-L                                               | 0.09                           | 23.5                           | C                   | 0.08                           | 26.3                           | C                   |
|                                                                                                                                                                                                         | SB-T,R                                             | 0.72                           | 40.1                           | D                   | 0.81                           | 51.7                           | D                   |
|                                                                                                                                                                                                         | Overall                                            |                                | 36.5                           | D                   |                                | 47.0                           | D                   |
| Level-of-Service (see Table 3.7-8 for level-of-service criteria).<br>NB = Northbound, SB = Southbound, EB = Eastbound, WB = Westbound.<br>L = left, R= right, T= through, (e.g. WB-L = Westbound left). |                                                    |                                |                                |                     |                                |                                |                     |



APPENDIX F

Stormwater Drainage Report



August 22, 2006

Village of Upper Nyack Planning Board  
North Broadway  
Village of Upper Nyack, NY 10960

**To Whom It May Concern:**

**Re: Courtyard at Upper Nyack-Drainage Report  
Lja # 03118**

Dear Sir/Madam:

We have prepared a hydrologic analysis of the proposed subdivision at the 11.2 acre Courtyard at Upper Nyack site. Our analysis indicates that two detention basins are required to mitigate against increases in peak discharges for storms ranging from the 2-year to the 100-year design discharge. Basin #1 and Basin # 2 are controlled by two orifices (3.00" Ø and 12.00 "Ø ) and overflow weirs. See details in the Appendix.

Basin # 1 and Basin # 2 have been designed in accordance with N.Y.S.D.E.C. water quality guidelines for a Storm Water Pocket Pond (P-5), which requires a forebay and permanent pond area.

Our hydrologic analysis concludes that the proposed development will yield no increases in peak rate of runoff at the drainage points downstream (Study Point #A, Study Point #B and Study Point #C) from that which occurs under existing conditions. Our analysis includes storms ranging from the 2-year to the 100-year design. Refer to Summary Table below for a comparison of Existing and Developed Conditions Discharges from the site.

**Summary Table # 1 – Site Discharges for Existing and Developed Conditions to an existing 24" Ø RCP located at easterly corner of the site (Study Point # A)**

| Conditions                        | Storm Frequency (in years) |      |      |      |      |
|-----------------------------------|----------------------------|------|------|------|------|
|                                   | 2                          | 5    | 10   | 25   | 100  |
| Pre-Development Discharges (cfs)  | 9.0                        | 15.5 | 21.5 | 26.6 | 41.6 |
| Post-Development Discharges (cfs) | 8.3                        | 14.4 | 19.6 | 23.8 | 39.5 |
| Net Change:                       | -0.7                       | -1.1 | -1.9 | -2.8 | -2.1 |

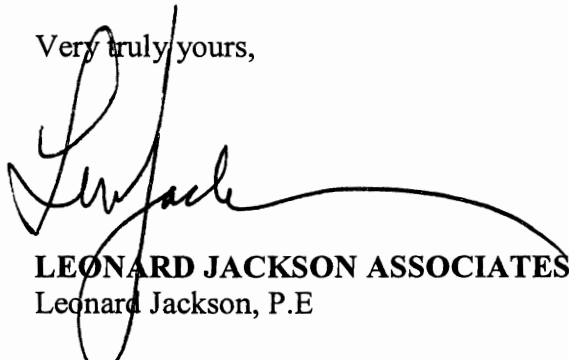
**Summary Table # 2 – Site Discharges for Existing and Developed Conditions to an existing 18" Ø RCP located at the northeasterly side of the site (Study Point # B)**

| Conditions                        | Storm Frequency (in years) |      |      |      |      |
|-----------------------------------|----------------------------|------|------|------|------|
|                                   | 2                          | 5    | 10   | 25   | 100  |
| Pre-Development Discharges (cfs)  | 0.3                        | 0.6  | 0.9  | 1.2  | 2.0  |
| Post-Development Discharges (cfs) | 0.3                        | 0.4  | 0.4  | 0.4  | 0.7  |
| Net Change:                       | 0.0                        | -0.2 | -0.5 | -0.8 | -1.3 |

**Summary Table # 3 – Site Discharges for Existing and Developed Conditions to a point located at the northeasterly corner of the site (Study Point # C)**

| Conditions                        | Storm Frequency (in years) |      |      |      |      |
|-----------------------------------|----------------------------|------|------|------|------|
|                                   | 2                          | 5    | 10   | 25   | 100  |
| Pre-Development Discharges (cfs)  | 0.7                        | 1.4  | 2.2  | 2.8  | 4.7  |
| Post-Development Discharges (cfs) | 0.3                        | 0.7  | 1.0  | 1.2  | 2.0  |
| Net Change:                       | -0.4                       | -0.7 | -1.2 | -1.6 | -2.5 |

Very truly yours,



**LEONARD JACKSON ASSOCIATES**  
Leonard Jackson, P.E

LJ:pd  
Attachment

P:\Word-Files\2003\03118\drainage report-8-22-06\Village of Upper Nyack 8-22-06.doc

# **TABLE OF CONTENTS:**

- 1.) *Hydrologic Narrative & Conclusions*
- 2.) *Table of Contents*
- 3.) *Pollutant Loading Summary Table*
- 4.) *Vicinity Map*

## **Appendix A – Methodology, Survey and Drainage Area Data:**

- 1.) *Methodology*
- 2.) *Existing Drainage Area Map*
- 3.) *Developed Conditions Drainage Area Map*
- 4.) *Water Quality Basin #1 – Plan View*
- 5.) *Water Quality Basin #2 – Plan View*
- 6.) *Outlet Structure #1 Detail*
- 7.) *Outlet Structure #2 Detail*
- 8.) *Diversion Manhole Detail*
- 9.) *Pocket Pond (P-5) Detail*
- 10.) *Pond Drain Detail*

## **Appendix B – Times of Concentration Calculations:**

- 1.) *Times of Concentration Calculations.*

## **Appendix C – Drainage Calculations:**

- 1.) *Rational Method Drainage Calculations*
- 2.) *Pollutant Loading Calculations*

## **Appendix D – Water Quality Calculations (Volume and Detention Time):**

- 1.) *Required and Provided Water Quality Volume Calculations in Basin 1*
- 2.) *Elevation versus Discharge Calculations for Basin 1*
- 3.) *Required and Provided Water Quality Volume Calculations in Basin 2*
- 4.) *Elevation versus Discharge Calculations for Basin 2*
- 5.) *Elevation versus Discharge Calculations for Diversion Manhole Design*

## **Appendix E –Downstream Pipe Analysis:**

- 1.) *Pipe Flow Calculations for Downstream Storm Drainage System*

## **Appendix F – Reference Materials:**

- 1.) *Urban Hydrology for Small Watersheds-Cover sheet*
- 2.) *TR-55 Figure 3-1: Average Velocities for estimating travel time.*
- 3.) *Rainfall intensity curves for Rockland County*
- 4.) *Newyork State Stormwater Management Design Manual-Cover sheet*
- 5.) *Unified Stormwater sizing Criteria*
- 6.) *Appendix A: The Simple Method to Calculate Urban Stormwater Load*
- 7.) *Table A.2 Pollutant Concentrations from Source Areas*
- 8.) *Table 1.1: Urban 'C' Values for use with the Simple Method (mg/l)*
- 9.) *Figure 15: Comparative Pollutant Removal of Urban BMP Designs*

## **Appendix G - Hec-1 Analyses:**

- 1.) *Existing Conditions (Hec-1 Model- "ex.h1out")*
- 2.) *Developed Conditions (Hec-1 Model- "dev.h1out")*





**LEONARD JACKSON ASSOCIATES CONSULTING ENGINEERS**

26 Firemens Memorial Drive. Suite 201. Pomona, NY 10970

845-354-4382 (phone) 845-354-4401 (fax)

**Summary Table #1  
Existing & Proposed Conditions  
Pollutant Loading Rates**

| <b>Phosphorous</b> | <b>Existing<br/>(lbs/yr)</b> | <b>Post-Development<br/>After BMP's<br/>(lbs/yr)</b> |
|--------------------|------------------------------|------------------------------------------------------|
|                    | 0.6                          | 2.0                                                  |

| <b>Nitrogen</b> | <b>Existing<br/>(lbs/yr)</b> | <b>Post-Development<br/>After BMP's<br/>(lbs/yr)</b> |
|-----------------|------------------------------|------------------------------------------------------|
|                 | 3.0                          | 28.2                                                 |

| <b>Suspended<br/>Solids</b> | <b>Existing<br/>(lbs/yr)</b> | <b>Post-Development<br/>After BMP's<br/>(lbs/yr)</b> |
|-----------------------------|------------------------------|------------------------------------------------------|
|                             | 268                          | 0                                                    |

| <b>BOD</b> | <b>Existing<br/>(lbs/yr)</b> | <b>Post-Development<br/>After BMP's<br/>(bil. colonies /yr)</b> |
|------------|------------------------------|-----------------------------------------------------------------|
|            | 13378                        | 294159                                                          |



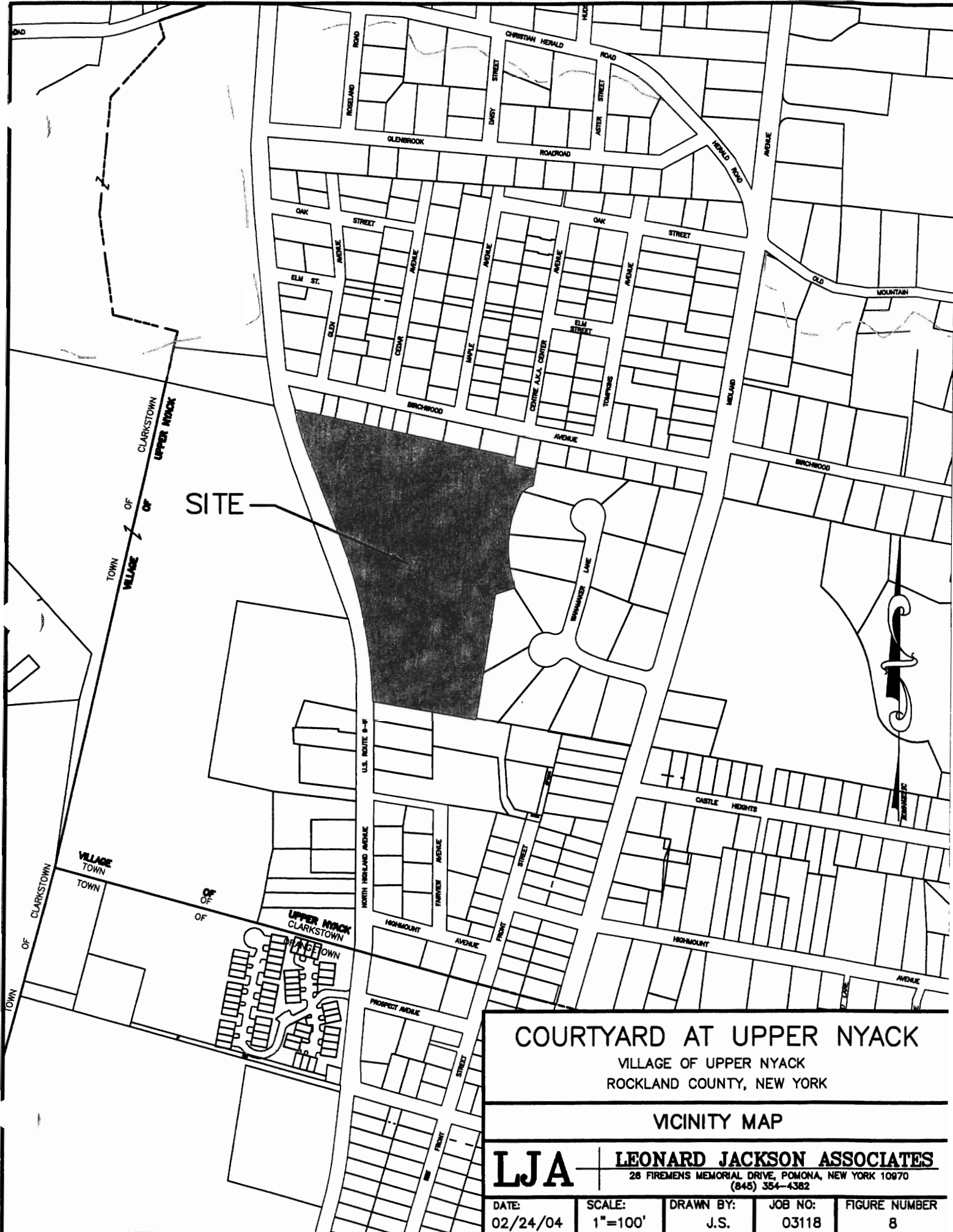
**LEONARD JACKSON ASSOCIATES CONSULTING ENGINEERS**

**26 Firemens Memorial Drive. Suite 201. Pomona, NY 10970**

**845-354-4382 (phone) 845-354-4401 (fax)**

**Summary Table #2  
Proposed Conditions  
Pollutant Loading Breakdown  
By Drainage Subbasin**

| <b>Subbasin</b> | <b>Phosphorous<br/>(lbs/yr)</b> | <b>Nitrogen<br/>(lbs/yr)</b> | <b>Suspended<br/>Solids<br/>(lbs/yr)</b> | <b>BOD<br/>(bil. colonies /yr)</b> |
|-----------------|---------------------------------|------------------------------|------------------------------------------|------------------------------------|
| area to basin 1 | 0.84                            | 15.28                        | 0                                        | 245998.3                           |
| area to basin 2 | 1.16                            | 12.88                        | 0                                        | 48160.68                           |
| <b>TOTALS</b>   | <b>2.00</b>                     | <b>28.16</b>                 | <b>0</b>                                 | <b>294159</b>                      |



SITE

**COURTYARD AT UPPER NYACK**  
 VILLAGE OF UPPER NYACK  
 ROCKLAND COUNTY, NEW YORK

VICINITY MAP

**LJA** | **LEONARD JACKSON ASSOCIATES**  
 26 FIREMENS MEMORIAL DRIVE, POMONA, NEW YORK 10970  
 (845) 354-4382

|                   |                   |                   |                  |                    |
|-------------------|-------------------|-------------------|------------------|--------------------|
| DATE:<br>02/24/04 | SCALE:<br>1"=100' | DRAWN BY:<br>J.S. | JOB NO:<br>03118 | FIGURE NUMBER<br>8 |
|-------------------|-------------------|-------------------|------------------|--------------------|



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- 10.) *Pond Drain Detail*



## **ENGINEERING METHODOLOGY:**

### Area Hydrology:

The 11.2-acre site runoff generally drains offsite in two existing storm drainage pipes. The majority draining to an existing 24"  $\Phi$  RCP located at the easterly side of the site (study point #A) and the rest draining to an existing 18"  $\Phi$  RCP located at the northeasterly side of the site (study point # B).

### Methodology:

Study Points #A and #B were evaluated for pre- and post-development conditions were used to evaluate pre- and post-developed peak discharges offsite.

All drainage area delineations and any changes from existing to proposed conditions are indicated graphically on Drainage Area Maps provided in the Appendix.

Flows were established for existing and developed conditions utilizing the Rational Method.

Time of concentration calculations were tabulated under existing and proposed conditions. Curve numbers were calibrated to match the flow for 25-year storm event. Supporting data is attached in the appendix.

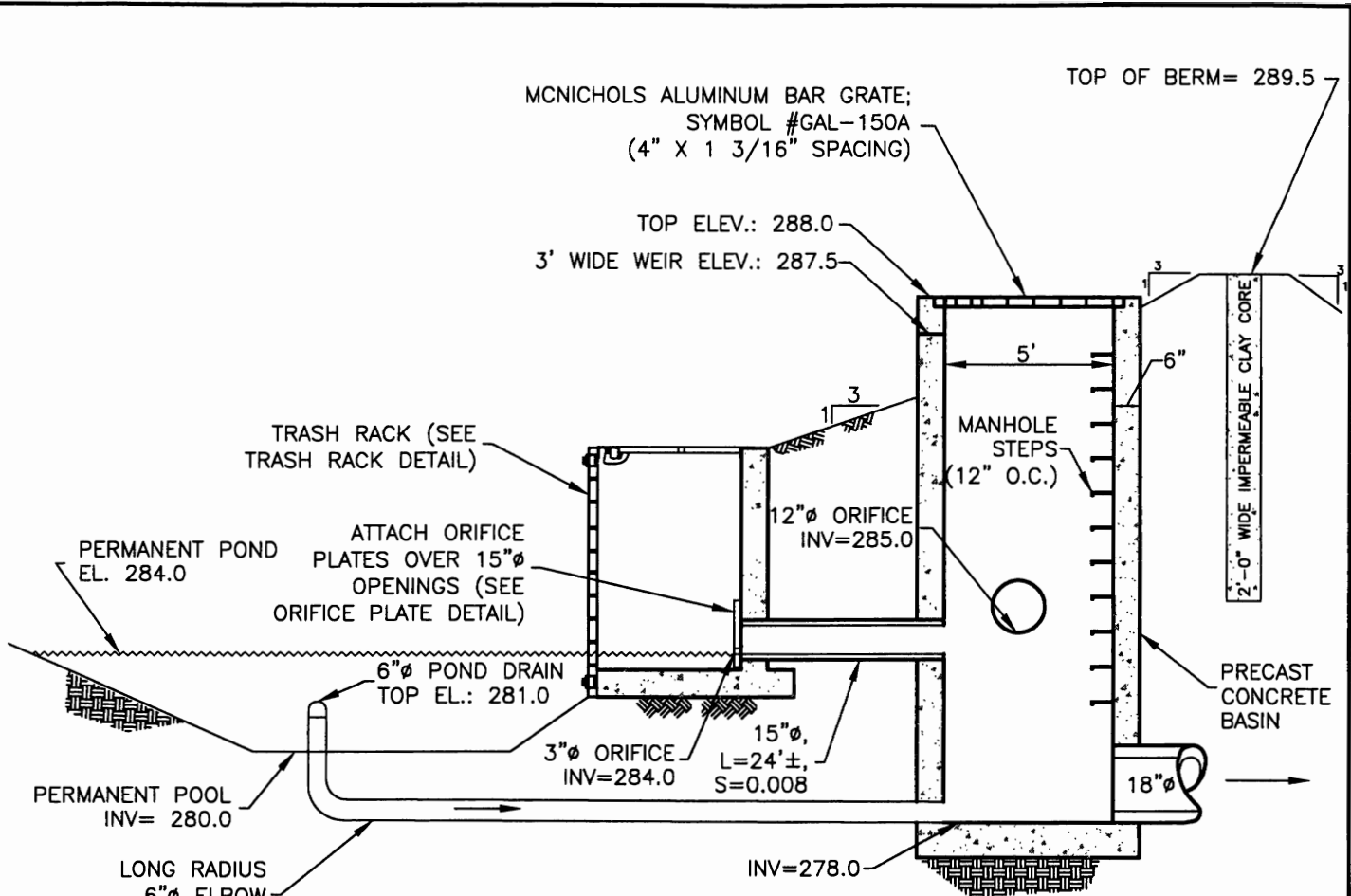
Hydrologic analyses were prepared for existing and proposed conditions and utilize SCS unit hydrographs utilizing the calibrated curve number for pre- and post-development conditions.

The hydrograph calculations and summations were prepared using the Corps of Engineers Hydrological Computer Program, HEC-1. To establish these flows the 2, 5, 10 and 100 year, 24-hour storm precipitation values were derived from available TP-40 information and incorporated in the HEC-1 models.

Our analysis indicates that two detention and water quality basins are required to mitigate against increases in peak discharge for storms ranging from the 2-year to the 100-year design discharge. Detention basin # 1 and # 2 will be controlled by a two orifices (3-inch diameter orifice and 12-inch diameter orifice) and over flow weirs. See details in the Appendix.

Detention Basin # 1 and # 2 are designed in accordance with N.Y.S.D.E.C. water quality guidelines for a *Storm water Pocket Pond (P-5)*, which requires a forebay and permanent pond area.

Refer to the Appendix for backup calculations, HEC-1 analyses and other supporting drainage data.



# OUTLET STRUCTURE DETAIL-BASIN-1

N.T.S.

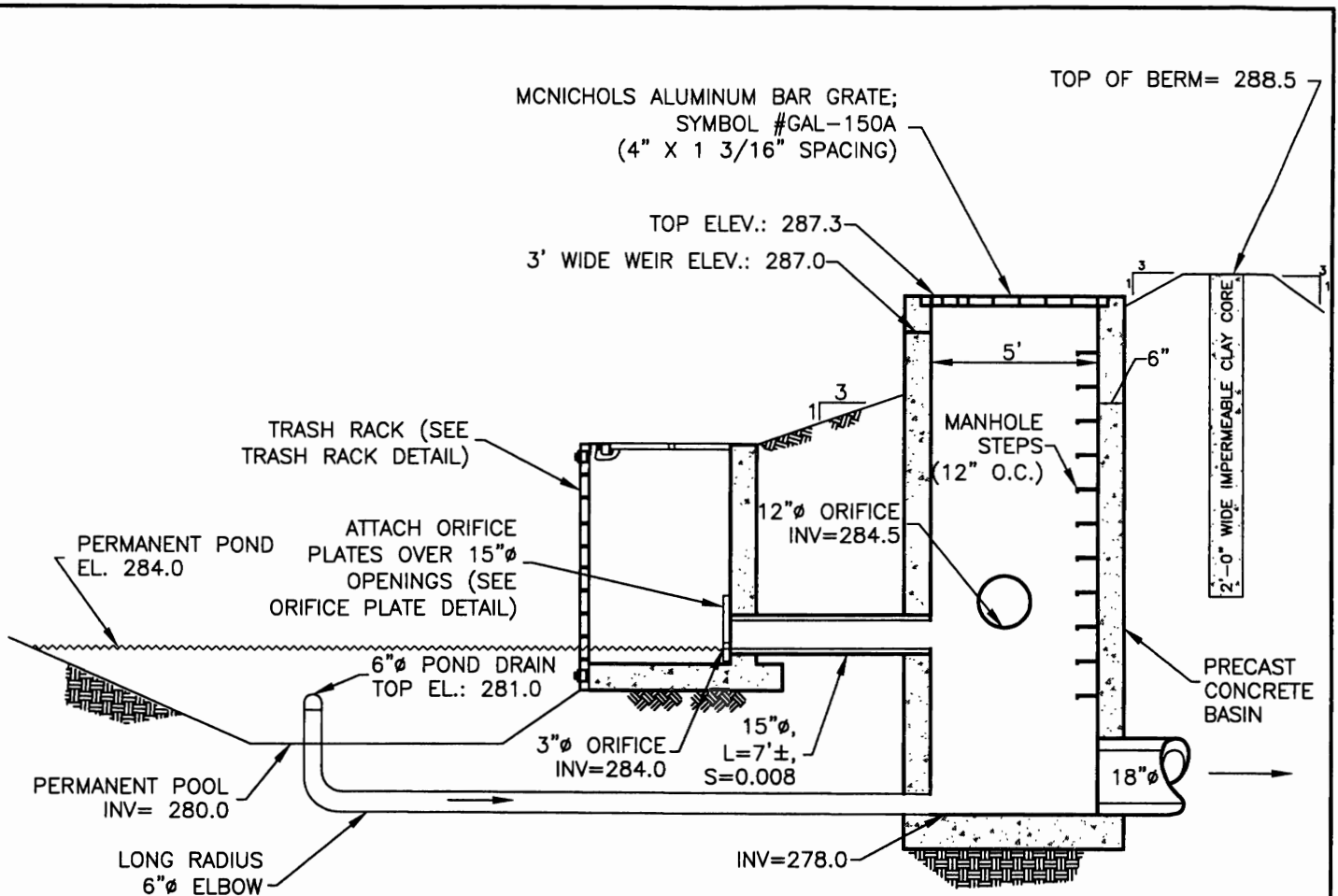
**BASIN NOTES:**

- A. ALL BERM FILL TO BE COMPACTED TO 95% MODIFIED PROCTOR MINIMUM DENSITY. LOW PERMEABILITY SOIL FREE OF ORGANIC MATERIALS TO BE UTILIZED IN BERM CONSTRUCTION.
- B. A LANDSCAPING PLAN FOR THE STORMWATER POND AND ITS BUFFER SHALL BE PREPARED TO INDICATE HOW AQUATIC AND TERRESTRIAL AREAS WILL BE VEGETATIVELY STABILIZED AND ESTABLISHED.
- C. SHOP DRAWINGS OF ALL STRUCTURES TO BE SUBMITTED TO THE DESIGN ENGINEER FOR APPROVAL PRIOR TO CONSTRUCTION.

**MAINTENANCE NOTES:**

- 1. A LEGALLY BINDING MAINTENANCE AGREEMENT TO BE PREPARED FOR THE TOWN OF CLARKSTOWN FOR FUTURE MAINTENANCE AND UPKEEP.
- 2. AN ACCESS AND MAINTENANCE EASEMENT TO BE PROVIDED TO THE TOWN OF CLARKSTOWN.
- 3. FOREBAY SEDIMENT REMOVAL TO BE PERFORMED EVERY FIVE YEARS OR WHEN THE FOREBAY IS 50% FULL.

|                                                                      |         |                                   |         |               |
|----------------------------------------------------------------------|---------|-----------------------------------|---------|---------------|
| <b>COURTYARD AT UPPER NYACK</b>                                      |         |                                   |         |               |
| VILLAGE OF UPPER NYACK<br>ROCKLAND COUNTY, NEW YORK                  |         |                                   |         |               |
| <b>OUTLET STRUCTURE DETAIL</b>                                       |         |                                   |         |               |
| <b>LJA</b>                                                           |         | <b>LEONARD JACKSON ASSOCIATES</b> |         |               |
| 26 FIREMENS MEMORIAL DRIVE, POMONA, NEW YORK 10970<br>(845) 354-4382 |         |                                   |         |               |
| DATE:                                                                | SCALE:  | DRAWN BY:                         | JOB NO: | FIGURE NUMBER |
| 08/24/06                                                             | 1"=100' | P.D.                              | 03118   | B9            |



# OUTLET STRUCTURE DETAIL-BASIN-2

N.T.S.

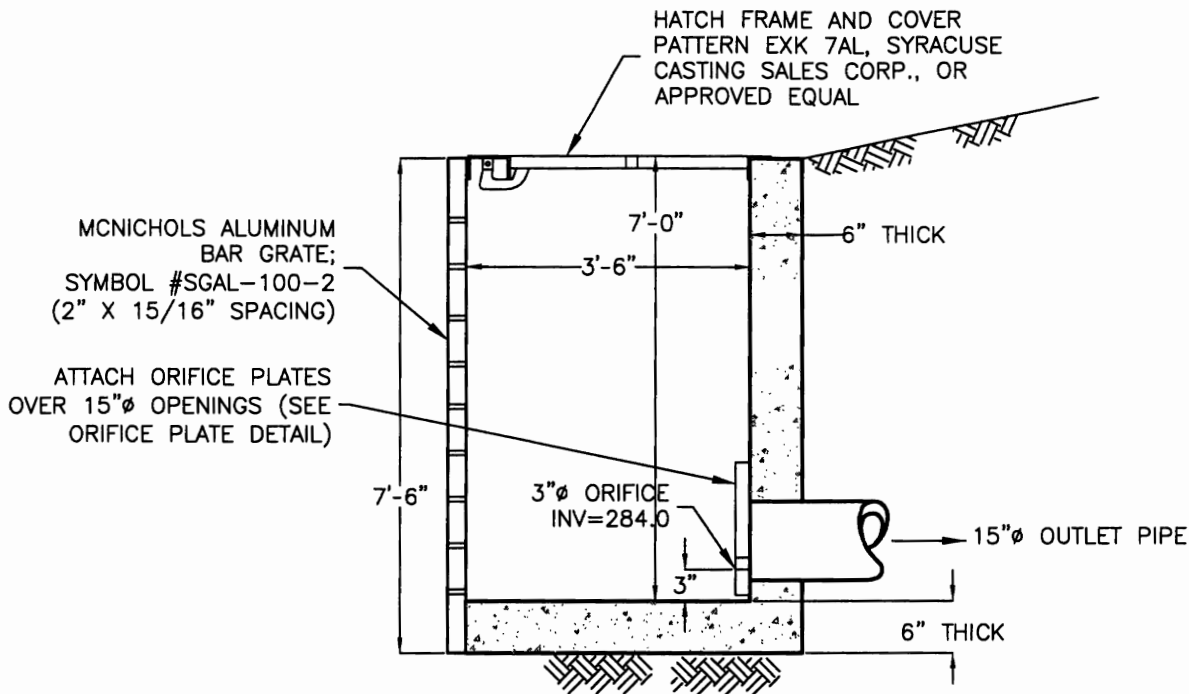
**BASIN NOTES:**

- A. ALL BERM FILL TO BE COMPACTED TO 95% MODIFIED PROCTOR MINIMUM DENSITY. LOW PERMEABILITY SOIL FREE OF ORGANIC MATERIALS TO BE UTILIZED IN BERM CONSTRUCTION.
- B. A LANDSCAPING PLAN FOR THE STORMWATER POND AND ITS BUFFER SHALL BE PREPARED TO INDICATE HOW AQUATIC AND TERRESTRIAL AREAS WILL BE VEGETATIVELY STABILIZED AND ESTABLISHED.
- C. SHOP DRAWINGS OF ALL STRUCTURES TO BE SUBMITTED TO THE DESIGN ENGINEER FOR APPROVAL PRIOR TO CONSTRUCTION.

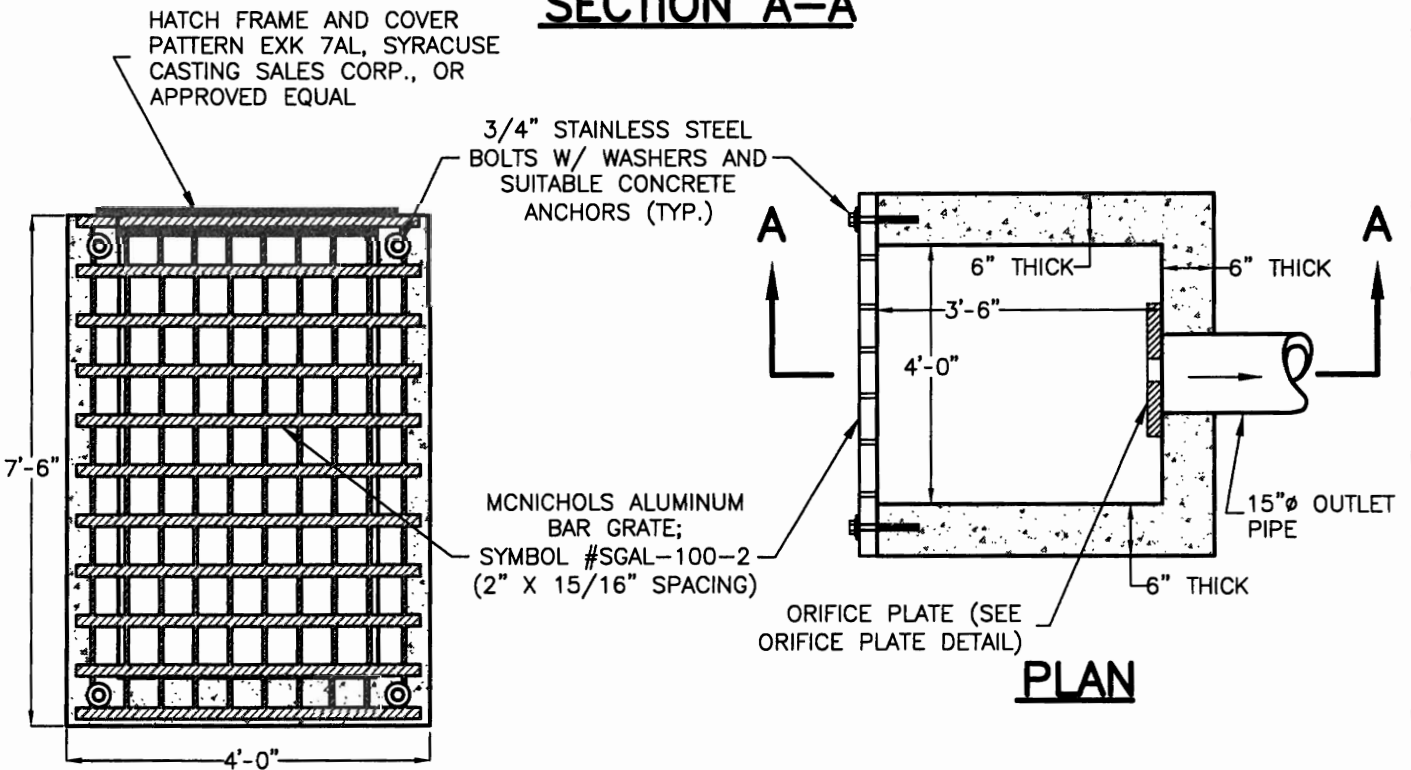
**MAINTENANCE NOTES:**

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- 2. AN ACCESS AND MAINTENANCE EASEMENT TO BE PROVIDED TO THE TOWN OF CLARKSTOWN.
- 3. FOREBAY SEDIMENT REMOVAL TO BE PERFORMED EVERY FIVE YEARS OR WHEN THE FOREBAY IS 50% FULL.

|                                                                                      |                   |                                   |                  |                     |
|--------------------------------------------------------------------------------------|-------------------|-----------------------------------|------------------|---------------------|
| <b>COURTYARD AT UPPER NYACK</b>                                                      |                   |                                   |                  |                     |
| VILLAGE OF UPPER NYACK<br>ROCKLAND COUNTY, NEW YORK                                  |                   |                                   |                  |                     |
| <b>OUTLET STRUCTURE DETAIL</b>                                                       |                   |                                   |                  |                     |
| <b>LJA</b>                                                                           |                   | <b>LEONARD JACKSON ASSOCIATES</b> |                  |                     |
| <small>28 FIREMENS MEMORIAL DRIVE, POMONA, NEW YORK 10970<br/>(845) 354-4382</small> |                   |                                   |                  |                     |
| DATE:<br>08/24/06                                                                    | SCALE:<br>1"=100' | DRAWN BY:<br>P.D.                 | JOB NO:<br>03118 | FIGURE NUMBER<br>B9 |



**SECTION A-A**

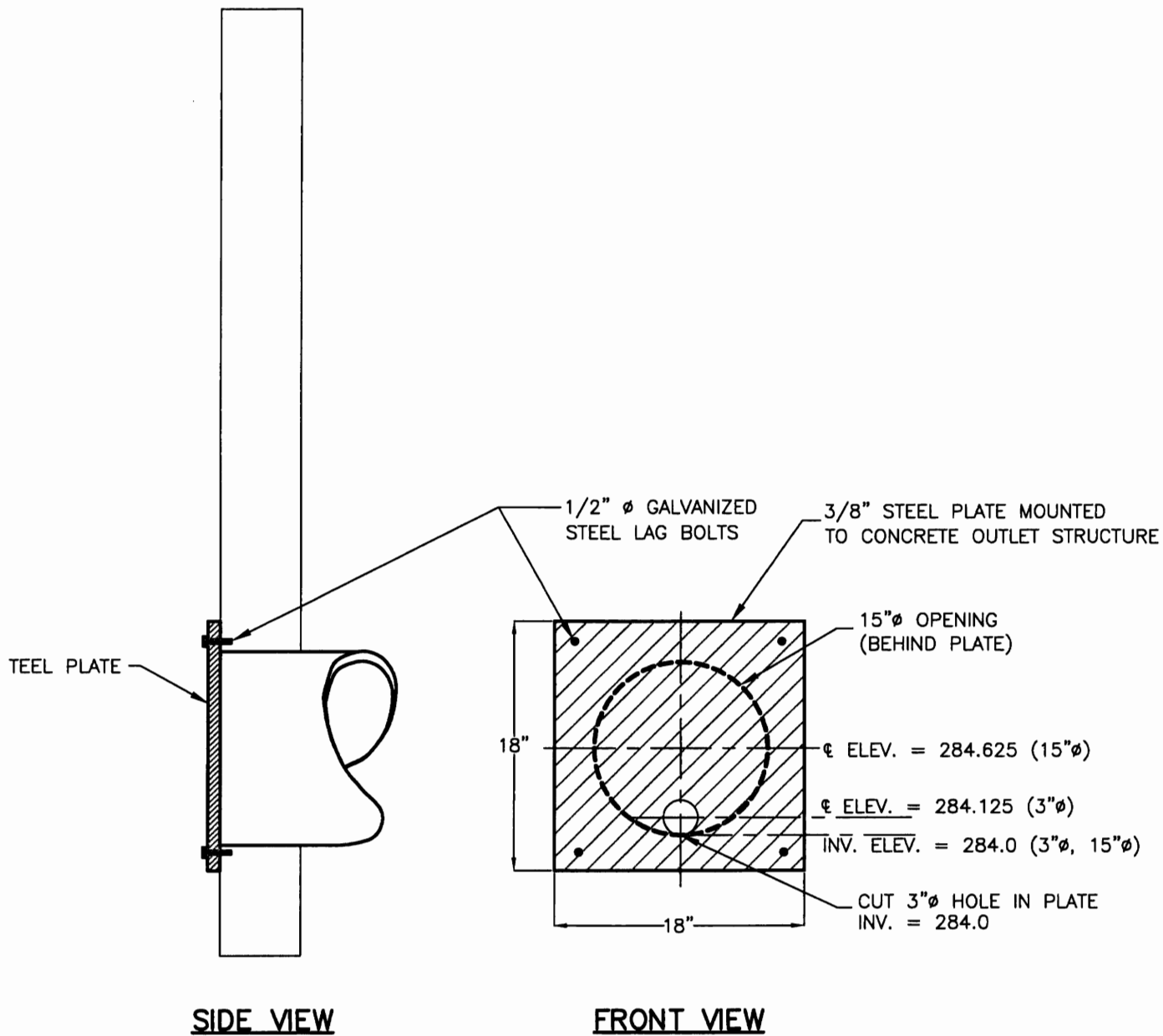


**FRONT ELEVATION**

**TRASH RACK DETAIL**

N.T.S.

|                                                                                        |                   |                                                                                                                           |                      |
|----------------------------------------------------------------------------------------|-------------------|---------------------------------------------------------------------------------------------------------------------------|----------------------|
| <b>COURTYARD AT UPPER NYACK</b><br>VILLAGE OF UPPER NYACK<br>ROCKLAND COUNTY, NEW YORK |                   |                                                                                                                           |                      |
| <b>TRASH RACK DETAIL</b>                                                               |                   |                                                                                                                           |                      |
| <b>LJA</b>                                                                             |                   | <b>LEONARD JACKSON ASSOCIATES</b><br><small>28 FIREMENS MEMORIAL DRIVE, POMONA, NEW YORK 10670<br/>(845) 354-4382</small> |                      |
| DATE:<br>08/24/06                                                                      | SCALE:<br>1"=100' | DRAWN BY:<br>P.D.                                                                                                         | JOB NO:<br>03118     |
|                                                                                        |                   |                                                                                                                           | FIGURE NUMBER<br>B10 |

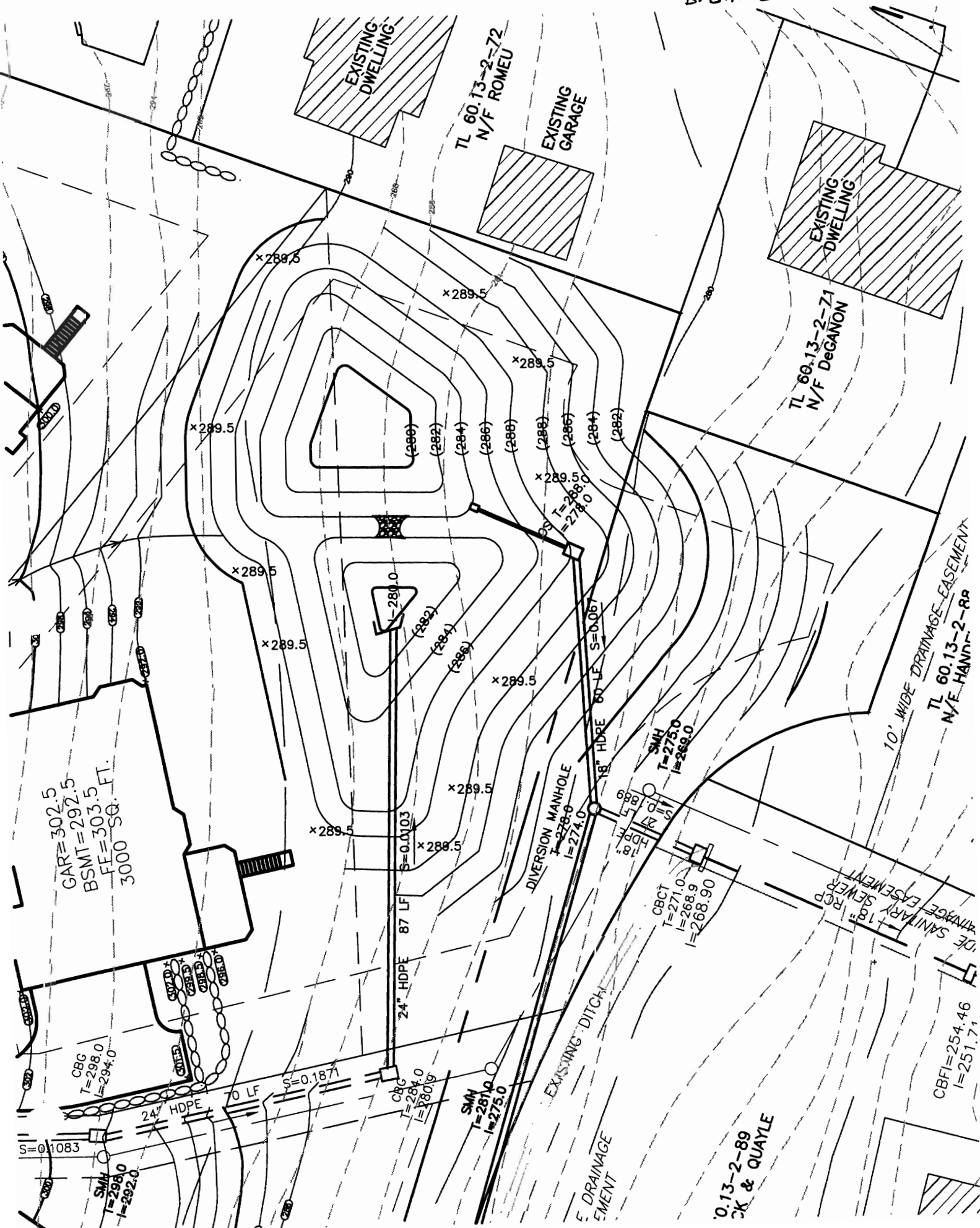


# ORIFICE PLATE DETAIL

N.T.S.

|                                                                                        |         |                                                                                                                           |         |               |
|----------------------------------------------------------------------------------------|---------|---------------------------------------------------------------------------------------------------------------------------|---------|---------------|
| <b>COURTYARD AT UPPER NYACK</b><br>VILLAGE OF UPPER NYACK<br>ROCKLAND COUNTY, NEW YORK |         |                                                                                                                           |         |               |
| <b>ORIFICE PLATE DETAIL</b>                                                            |         |                                                                                                                           |         |               |
| <b>LJA</b>                                                                             |         | <b>LEONARD JACKSON ASSOCIATES</b><br><small>26 FIREMENS MEMORIAL DRIVE, POMONA, NEW YORK 10970<br/>(845) 354-4382</small> |         |               |
| DATE:                                                                                  | SCALE:  | DRAWN BY:                                                                                                                 | JOB NO: | FIGURE NUMBER |
| 08/24/06                                                                               | 1"=100' | P.D.                                                                                                                      | 03118   | B11           |

BASIN 1



GAR=302.5  
 BSMT=292.5  
 FE=303.5  
 3000 SQ. FT.

SMH  
 T=298.0  
 I=294.0

24" HDPE 70 LF  
 S=0.1871

24" HDPE 87 LF  
 S=0.0103

SMH  
 T=281.0  
 I=275.0

EXISTING DITCH  
 EXISTING DRAINAGE EASEMENT

DIVERSION MANHOLE  
 T=274.0  
 I=274.0

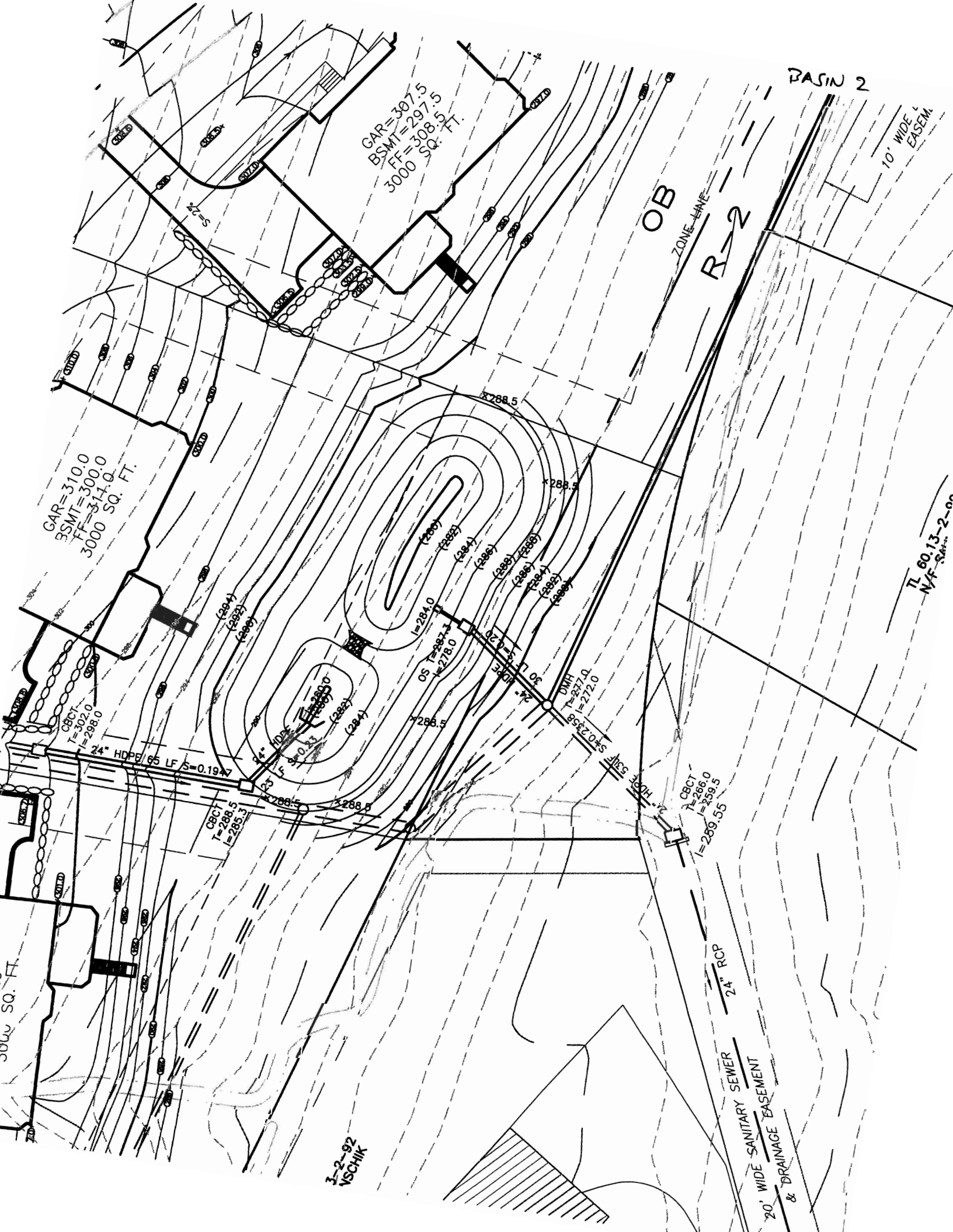
CBCF  
 T=271.0  
 I=268.90

SMH  
 T=275.0  
 I=268.0

0.13-2-89  
 CK & QUAYLE

CBEI=254.46  
 I=251.71

10' WIDE DRAINAGE EASEMENT  
 TL 60.13-2-RP  
 N/E HAND



BASIN 2

10' WIDE EASEMENT

OB ZONE-LANE  
R-2

T. 60.13-2-00  
N/F 8-4-00

GAR=307.5  
BSMT=297.5  
FF=308.5  
3000 SQ. FT.

GAR=310.0  
BSMT=300.0  
FF=314.0  
3000 SQ. FT.

3-2-92  
VSC/IK

20' WIDE SANITARY SEWER & DRAINAGE EASEMENT

POB 24"

CBCT  
T=266.0  
I=269.5

DMH  
T=277.0  
I=272.0

OS  
T=287.3  
I=278.0

CBCT  
T=286.5  
I=285.3

24" HDPE/95 LF/S=0.1947

5000 SQ. FT.

CBCT  
T=302.0  
I=298.0

(284)  
(283)  
(289)

(284)  
(283)  
(289)

288.5

288.5

(280)  
(282)  
(284)

(288)  
(286)  
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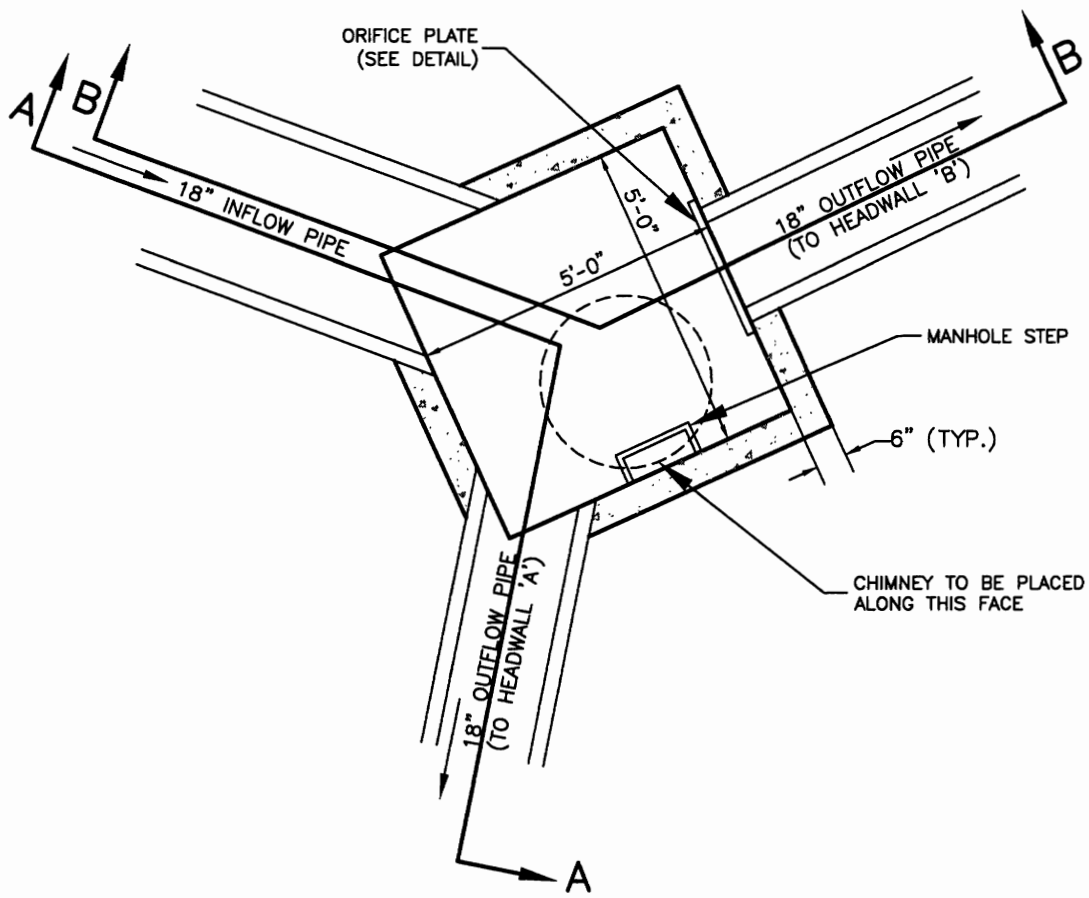
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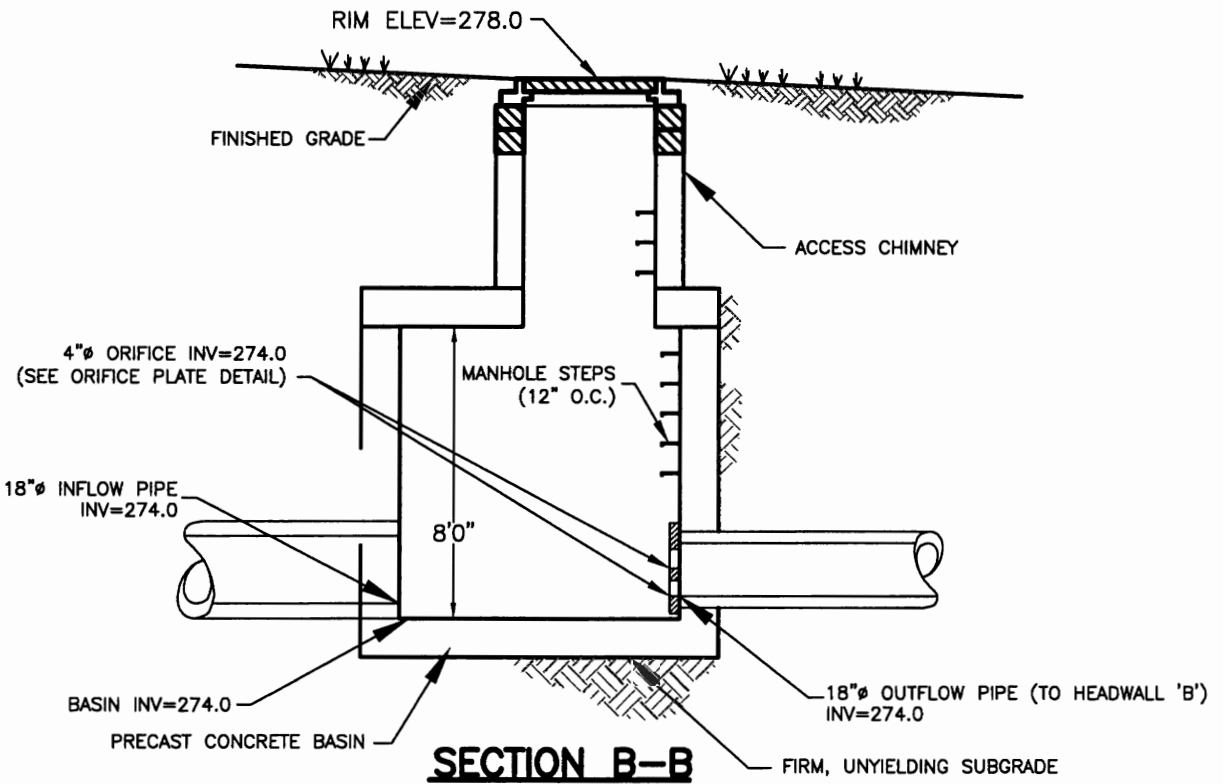
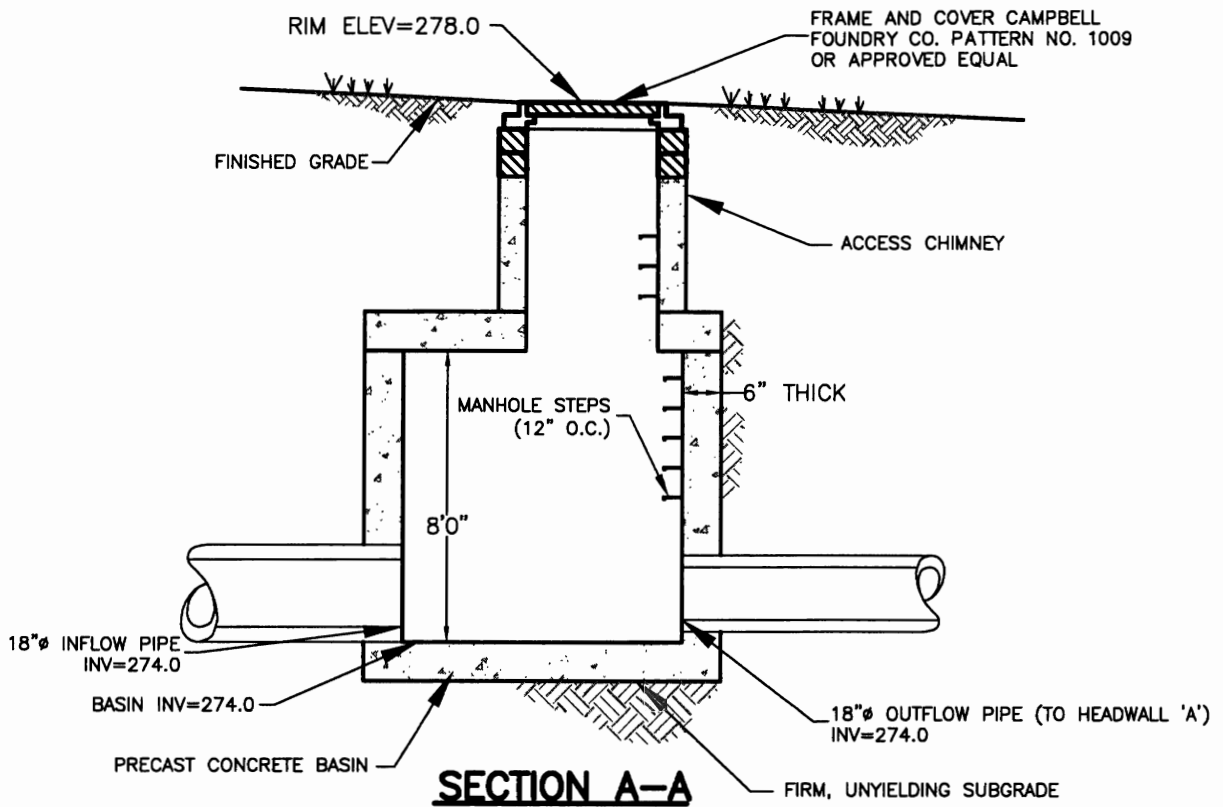
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**PLAN**

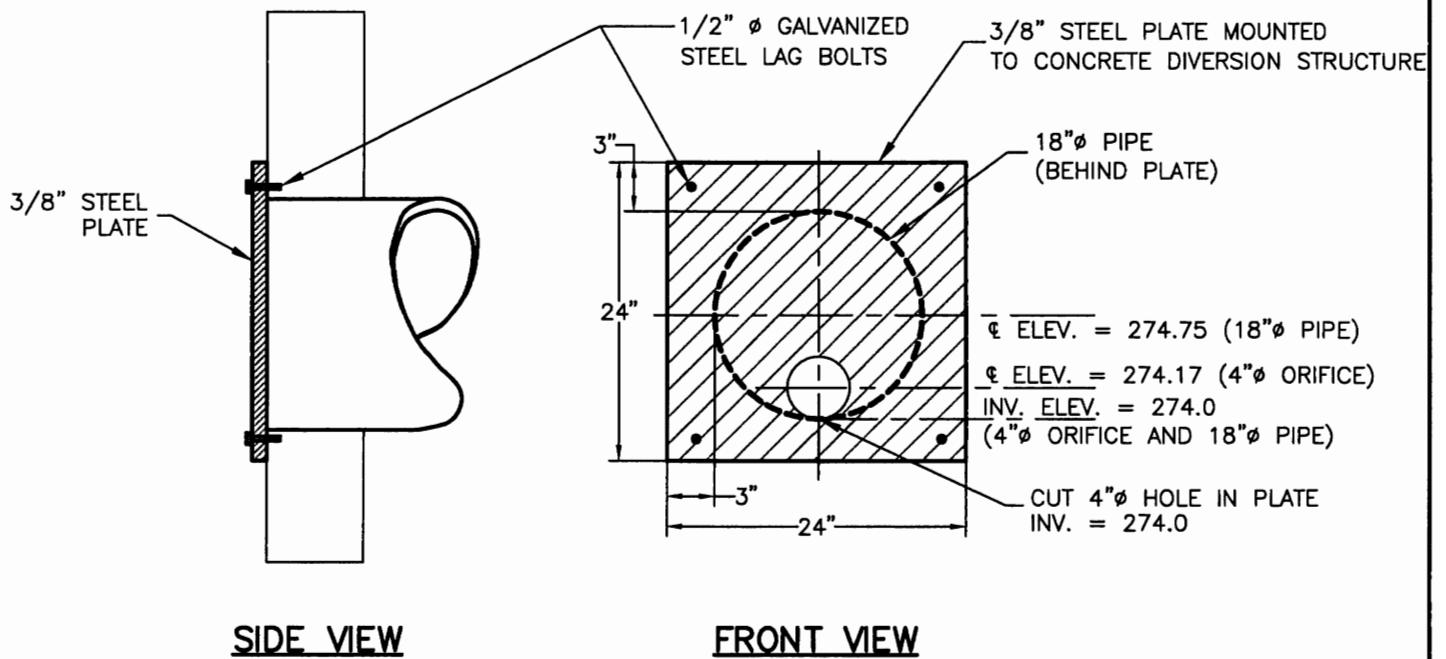
**DIVERSION STRUCTURE DETAIL**

N.T.S.



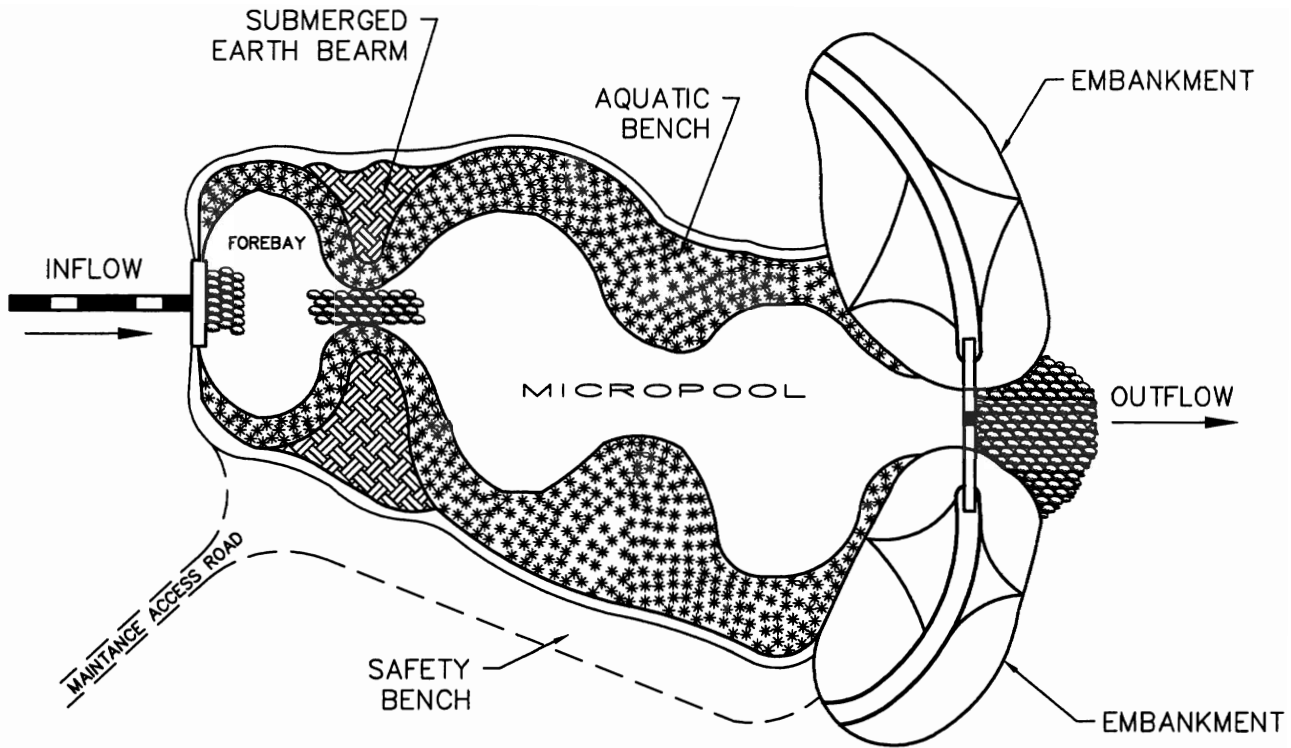
# DIVERSION STRUCTURE SECTIONS

N.T.S.

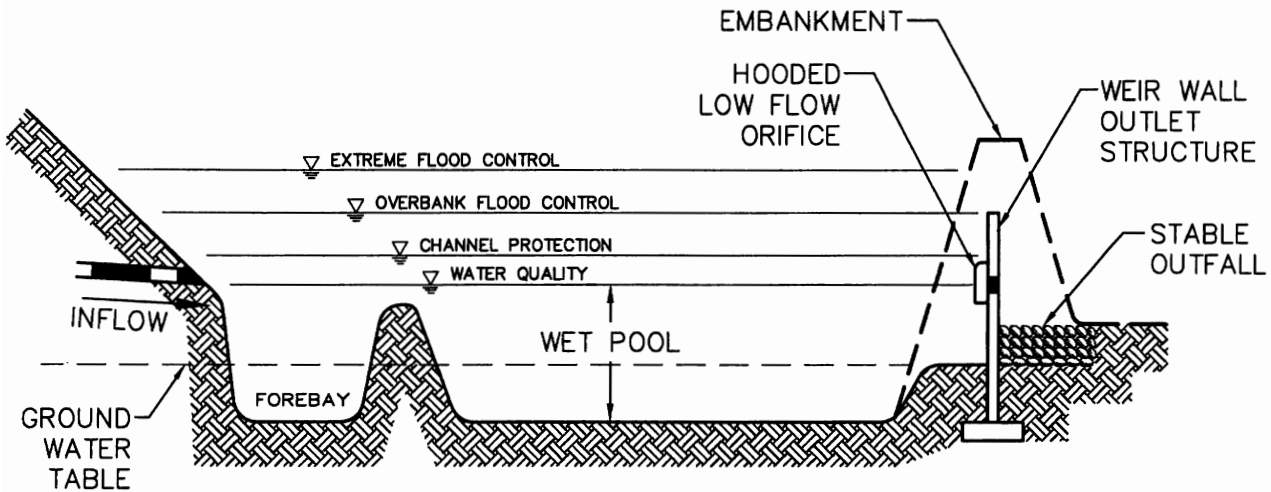


**DIVERSION STRUCTURE ORIFICE PLATE DETAIL  
 (FOR PIPE TO HEADWALL 'B')**

N.T.S.



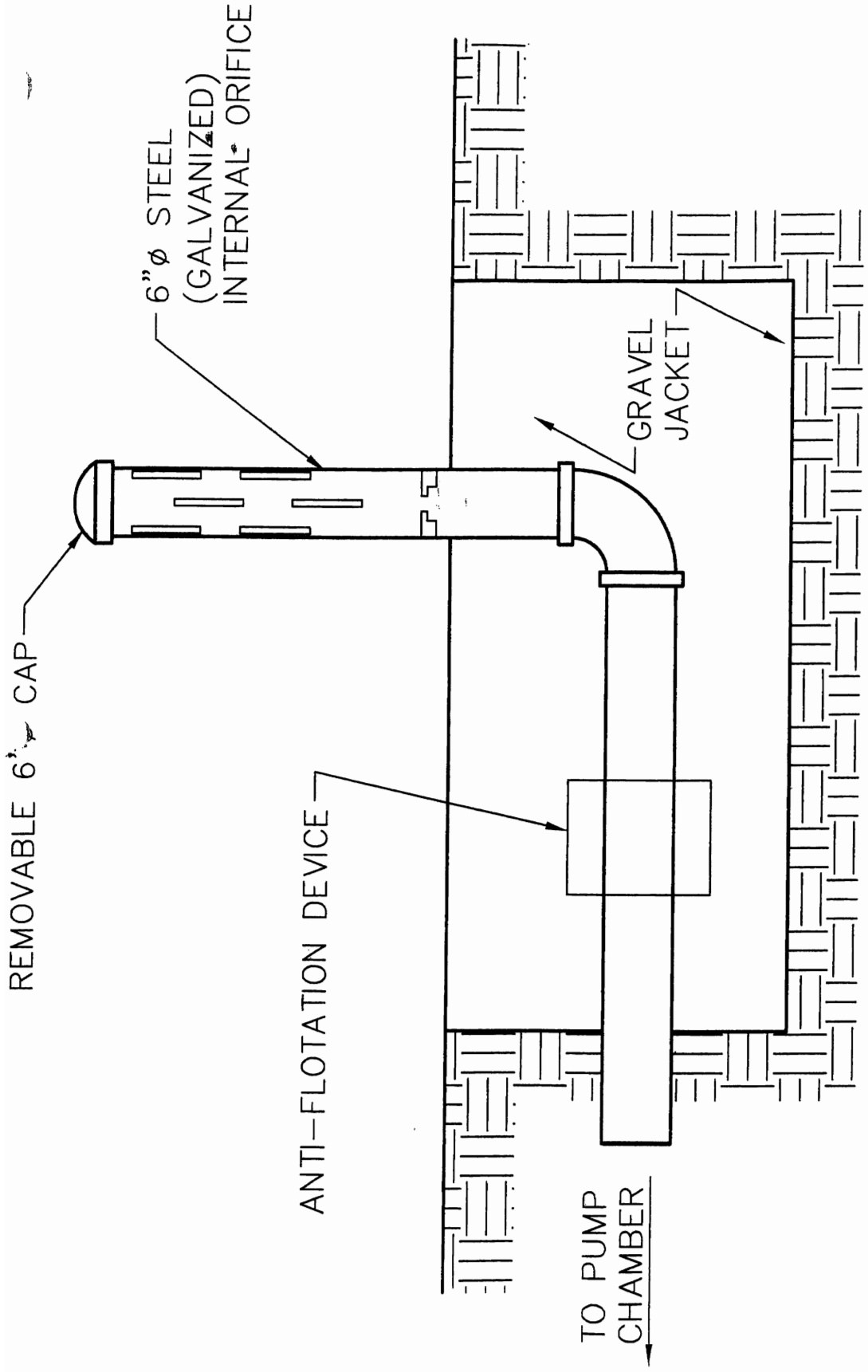
PLAN VIEW



PROFILE

POCKET POND (P-5) DETAIL

N.T.S.



# POND DRAIN DETAIL

N.T.S.



Appendix B – Times of Concentration Calculations:

1.) *Times of Concentration Calculations.*



# LEONARD JACKSON ASSOCIATES

26 Firemens Memorial Drive  
Pomona, NY 10970  
845-354-4382

## Worksheet 3: Time of Concentration (Tc) Calculations

PROJECT: Courtyard at Upper Nyack  
LOCATION: Village of Upper Nyack, NY

JOB #: 03118  
DATE: 02/24/04

BY: JS

Mark One:      Existing                  Developed

Subarea Description:      Subarea 1, Offsite area contributing to stream flowing through the site, to Point of Interest 'A'  
Subarea conditions do not vary between Existing and Developed Conditions

Sheet Flow:

1. Surface description (table 3-1).....
2. Manning's Roughness Coeff., n (table 3-1).....
3. Flow Length, L (total < or = to 300 ft.).....(ft.)
4. Two year, 24 hr rainfall, P<sub>2</sub>.....(in.)
5. Land Slope, S.....(ft./ft.)

Segment ID:

|         |  |
|---------|--|
| 575-526 |  |
| Unpaved |  |
| 0.4     |  |
| 200     |  |
| 3.33    |  |
| 0.245   |  |
| 0.22    |  |

6.  $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} S^{0.4}}$       Compute  $T_t = \dots\dots\dots$ (hr.)

= **0.22** (hrs.)

Shallow Concentrated Flow:

1. Surface description (paved or unpaved).....
2. Flow Length, L ..... (ft.)
3. Watercourse Slope, s.....(ft./ft.)
4. Average Velocity, V (figure 3-1)..... (ft./s)

Segment ID:

|           |  |
|-----------|--|
| 526-327.2 |  |
| unpaved   |  |
| 1015      |  |
| 0.196     |  |
| 7.1       |  |
| 0.04      |  |

6.  $T_t = \frac{L}{3600 V}$       Compute  $T_t = \dots\dots\dots$ (hr.)

= **0.04** (hrs.)

Open Channel Flow (California Method):

|                   |                             |                       |                               |
|-------------------|-----------------------------|-----------------------|-------------------------------|
| Flow Length, L:   | (ft.)<br>0                  | (mi.)<br><u>0.000</u> |                               |
| Elevation Change: | (Start )<br>0.0             | (End)<br>0.0          | (Change in ft.)<br><u>0.0</u> |
|                   | $T_t = (11.9L^3/H)^{0.385}$ |                       |                               |
|                   | $T_t = 0.00$                |                       |                               |

= **0.00** (hrs.)

**Total Tc = 0.26 (hrs.)**  
**15.8 (min.)**

# LEONARD JACKSON ASSOCIATES

26 Firemens Memorial Drive  
Pomona, NY 10970  
845-354-4382

## Worksheet 3: Time of Concentration (Tc) Calculations

PROJECT: Courtyard at Upper Nyack  
LOCATION: Village of Upper Nyack, NY

JOB #: 03118  
DATE: 02/24/04

BY: JS

Mark One:      Existing              Developed

Subarea Description:      Subarea 2, Offsite area draining through site to Point of Interest 'C'

Sheet Flow:

1. Surface description (table 3-1).....
2. Manning's Roughness Coeff., n (table 3-1).....
3. Flow Length, L (total < or = to 300 ft.).....(ft.)
4. Two year, 24 hr rainfall, P<sub>2</sub>.....(in.)
5. Land Slope, S.....(ft./ft.)
6.  $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} S^{0.4}}$               Compute T<sub>t</sub> = .....(hr.)

|             |           |  |
|-------------|-----------|--|
| Segment ID: | 347.7-.43 |  |
|             | PAVED     |  |
|             | 0.02      |  |
|             | 75        |  |
|             | 3.33      |  |
|             | 0.063     |  |
|             | 0.02      |  |

= 0.02 (hrs.)

Shallow Concentrated Flow:

1. Surface description (paved or unpaved).....
2. Flow Length, L ..... (ft.)
3. Watercourse Slope, s.....(ft./ft.)
4. Average Velocity, V (figure 3-1)..... (ft./s)
6.  $T_t = \frac{L}{3600 V}$               Compute T<sub>t</sub> = .....(hr.)

|             |  |  |
|-------------|--|--|
| Segment ID: |  |  |
|             |  |  |
|             |  |  |
|             |  |  |
|             |  |  |
|             |  |  |

= 0.00 (hrs.)

Open Channel Flow (California Method):

|                             |                  |              |                 |
|-----------------------------|------------------|--------------|-----------------|
|                             | (ft.)            | (mi.)        |                 |
| Flow Length, L:             | 0                | <u>0.000</u> |                 |
|                             | (Start)          | (End)        | (Change in ft.) |
| Elevation Change:           | 0.0              | 0.0          | <u>0.0</u>      |
| $T_t = (11.9L^3/H)^{0.385}$ |                  |              |                 |
|                             | T <sub>t</sub> = | 0.00         |                 |

= 0.00 (hrs.)

**Total Tc =** 0.02 (hrs.)  
1.0 (min.)

# LEONARD JACKSON ASSOCIATES

26 Firemens Memorial Drive  
Pomona, NY 10970  
845-354-4382

## Worksheet 3: Time of Concentration (Tc) Calculations

PROJECT: Courtyard at Upper Nyack  
LOCATION: Village of Upper Nyack, NY

JOB #: 03118  
DATE: 02/24/04

BY: JS

Mark One:      Existing              Developed

Subarea Description:              Subarea 3, Offsite area draining through site to Point of Interest 'B'

Sheet Flow:

1. Surface description (table 3-1).....
2. Manning's Roughness Coeff., n (table 3-1).....
3. Flow Length, L (total < or = to 300 ft.).....(ft.)
4. Two year, 24 hr rainfall, P<sub>2</sub>.....(in.)
5. Land Slope, S.....(ft./ft.)
6.  $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} S^{0.4}}$               Compute T<sub>t</sub> = .....(hr.)

|             |         |  |
|-------------|---------|--|
| Segment ID: | 347-342 |  |
|             | PAVED   |  |
|             | 0.02    |  |
|             | 60      |  |
|             | 3.33    |  |
|             | 0.083   |  |
|             | 0.01    |  |

= 0.01 (hrs.)

Shallow Concentrated Flow:

1. Surface description (paved or unpaved).....
2. Flow Length, L ..... (ft.)
3. Watercourse Slope, s.....(ft./ft.)
4. Average Velocity, V (figure 3-1)..... (ft./s)
6.  $T_t = \frac{L}{3600 V}$               Compute T<sub>t</sub> = .....(hr.)

|             |  |  |
|-------------|--|--|
| Segment ID: |  |  |
|             |  |  |
|             |  |  |
|             |  |  |
|             |  |  |
|             |  |  |

= 0.00 (hrs.)

Open Channel Flow (California Method):

|                   |                              |                       |                               |
|-------------------|------------------------------|-----------------------|-------------------------------|
| Flow Length, L:   | (ft.)<br>0                   | (mi.)<br><u>0.000</u> |                               |
| Elevation Change: | (Start)<br>0.0               | (End)<br>0.0          | (Change in ft.)<br><u>0.0</u> |
|                   | $T_t = (11.9L^3/H)^{0.385}$  |                       |                               |
|                   | T <sub>t</sub> = <b>0.00</b> |                       |                               |

= 0.00 (hrs.)

**Total Tc = 0.01 (hrs.)  
0.7 (min.)**



# LEONARD JACKSON ASSOCIATES

26 Firemens Memorial Drive  
Pomona, NY 10970  
845-354-4382

## Worksheet 3: Time of Concentration (Tc) Calculations

PROJECT: Courtyard at Upper Nyack  
LOCATION: Village of Upper Nyack, NY

JOB #: 03118  
DATE: 02/24/04

BY: JS

Mark One:      Existing                  Developed

Subarea Description:                  Subarea 5, Onsite area draining to Point of Interest 'C'

Sheet Flow:

1. Surface description (table 3-1).....
2. Manning's Roughness Coeff., n (table 3-1).....
3. Flow Length, L (total < or = to 300 ft.).....(ft.)
4. Two year, 24 hr rainfall, P<sub>2</sub>.....(in.)
5. Land Slope, S.....(ft./ft.)
6.  $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} S^{0.4}}$                   Compute T<sub>t</sub> = .....(hr.)

Segment ID:

|             |  |
|-------------|--|
| 343-324     |  |
| Light Brush |  |
| 0.4         |  |
| 200         |  |
| 3.33        |  |
| 0.095       |  |
| 0.33        |  |

= **0.33** (hrs.)

Shallow Concentrated Flow:

1. Surface description (paved or unpaved).....
2. Flow Length, L ..... (ft.)
3. Watercourse Slope, s.....(ft./ft.)
4. Average Velocity, V (figure 3-1)..... (ft./s)
6.  $T_t = \frac{L}{3600 V}$                   Compute T<sub>t</sub> = .....(hr.)

Segment ID:

|         |  |
|---------|--|
| 324-267 |  |
| unpaved |  |
| 540     |  |
| 0.106   |  |
| 5.2     |  |
| 0.03    |  |

= **0.03** (hrs.)

Open Channel Flow (California Method):

|                   |                              |                |                        |
|-------------------|------------------------------|----------------|------------------------|
| Flow Length, L:   | (ft.)<br>0                   | (mi.)<br>0.000 |                        |
| Elevation Change: | (Start)<br>0.0               | (End)<br>0.0   | (Change in ft.)<br>0.0 |
|                   | $T_t = (11.9L^3/H)^{0.385}$  |                |                        |
|                   | T <sub>t</sub> = <b>0.00</b> |                |                        |

= **0.00** (hrs.)

**Total Tc = 0.36 (hrs.)**  
**21.4 (min.)**

# LEONARD JACKSON ASSOCIATES

26 Firemens Memorial Drive  
Pomona, NY 10970  
845-354-4382

## Worksheet 3: Time of Concentration (Tc) Calculations

PROJECT: Courtyard at Upper Nyack  
LOCATION: Village of Upper Nyack, NY

JOB #: 03118  
DATE: 02/24/04

BY: JS

Mark One:      Existing      Developed

Subarea Description:      Subarea 6, Onsite area draining to Point of Interest 'B'

Sheet Flow:

|                                                                                                                                                                                                                                                                                                                                                |             |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |           |  |             |  |     |  |     |  |      |  |       |  |      |  |   |                    |
|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------|--|-------------|--|-----|--|-----|--|------|--|-------|--|------|--|---|--------------------|
| 1. Surface description (table 3-1).....<br>2. Manning's Roughness Coeff., n (table 3-1).....<br>3. Flow Length, L (total < or = to 300 ft.).....(ft.)<br>4. Two year, 24 hr rainfall, P <sub>2</sub> .....(in.)<br>5. Land Slope, S.....(ft./ft.)<br>6. $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} S^{0.4}}$ Compute T <sub>t</sub> = .....(hr.) | Segment ID: | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr><td style="text-align: center;">342-322.5</td><td style="width: 20px;"></td></tr> <tr><td style="text-align: center;">Light Brush</td><td></td></tr> <tr><td style="text-align: center;">0.4</td><td></td></tr> <tr><td style="text-align: center;">200</td><td></td></tr> <tr><td style="text-align: center;">3.33</td><td></td></tr> <tr><td style="text-align: center;">0.098</td><td></td></tr> <tr><td style="text-align: center;">0.32</td><td></td></tr> </table> | 342-322.5 |  | Light Brush |  | 0.4 |  | 200 |  | 3.33 |  | 0.098 |  | 0.32 |  | = | <b>0.32</b> (hrs.) |
| 342-322.5                                                                                                                                                                                                                                                                                                                                      |             |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |           |  |             |  |     |  |     |  |      |  |       |  |      |  |   |                    |
| Light Brush                                                                                                                                                                                                                                                                                                                                    |             |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |           |  |             |  |     |  |     |  |      |  |       |  |      |  |   |                    |
| 0.4                                                                                                                                                                                                                                                                                                                                            |             |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |           |  |             |  |     |  |     |  |      |  |       |  |      |  |   |                    |
| 200                                                                                                                                                                                                                                                                                                                                            |             |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |           |  |             |  |     |  |     |  |      |  |       |  |      |  |   |                    |
| 3.33                                                                                                                                                                                                                                                                                                                                           |             |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |           |  |             |  |     |  |     |  |      |  |       |  |      |  |   |                    |
| 0.098                                                                                                                                                                                                                                                                                                                                          |             |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |           |  |             |  |     |  |     |  |      |  |       |  |      |  |   |                    |
| 0.32                                                                                                                                                                                                                                                                                                                                           |             |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |           |  |             |  |     |  |     |  |      |  |       |  |      |  |   |                    |

Shallow Concentrated Flow:

|                                                                                                                                                                                                                                                 |             |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |             |  |         |  |     |  |       |  |     |  |      |  |   |                    |
|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------|--|---------|--|-----|--|-------|--|-----|--|------|--|---|--------------------|
| 1. Surface description (paved or unpaved).....<br>2. Flow Length, L ..... (ft.)<br>3. Watercourse Slope, s.....(ft./ft.)<br>4. Average Velocity, V (figure 3-1)..... (ft./s)<br>6. $T_t = \frac{L}{3600 V}$ Compute T <sub>t</sub> = .....(hr.) | Segment ID: | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr><td style="text-align: center;">322.5-274.5</td><td style="width: 20px;"></td></tr> <tr><td style="text-align: center;">unpaved</td><td></td></tr> <tr><td style="text-align: center;">400</td><td></td></tr> <tr><td style="text-align: center;">0.120</td><td></td></tr> <tr><td style="text-align: center;">5.5</td><td></td></tr> <tr><td style="text-align: center;">0.02</td><td></td></tr> </table> | 322.5-274.5 |  | unpaved |  | 400 |  | 0.120 |  | 5.5 |  | 0.02 |  | = | <b>0.02</b> (hrs.) |
| 322.5-274.5                                                                                                                                                                                                                                     |             |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |             |  |         |  |     |  |       |  |     |  |      |  |   |                    |
| unpaved                                                                                                                                                                                                                                         |             |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |             |  |         |  |     |  |       |  |     |  |      |  |   |                    |
| 400                                                                                                                                                                                                                                             |             |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |             |  |         |  |     |  |       |  |     |  |      |  |   |                    |
| 0.120                                                                                                                                                                                                                                           |             |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |             |  |         |  |     |  |       |  |     |  |      |  |   |                    |
| 5.5                                                                                                                                                                                                                                             |             |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |             |  |         |  |     |  |       |  |     |  |      |  |   |                    |
| 0.02                                                                                                                                                                                                                                            |             |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |             |  |         |  |     |  |       |  |     |  |      |  |   |                    |

Open Channel Flow (California Method):

|                             |          |              |                 |   |                    |
|-----------------------------|----------|--------------|-----------------|---|--------------------|
|                             | (ft.)    | (mi.)        |                 |   |                    |
| Flow Length, L:             | 0        | <u>0.000</u> |                 |   |                    |
|                             | (Start ) | (End)        | (Change in ft.) |   |                    |
| Elevation Change:           | 0.0      | 0.0          | <u>0.0</u>      |   |                    |
| $T_t = (11.9L^3/H)^{0.385}$ |          |              |                 |   |                    |
| T <sub>t</sub> =            | 0.00     |              |                 | = | <b>0.00</b> (hrs.) |

Total Tc = **0.34** (hrs.)  
**20.7** (min.)

# LEONARD JACKSON ASSOCIATES

26 Firemens Memorial Drive  
Pomona, NY 10970  
845-354-4382

## Worksheet 3: Time of Concentration (Tc) Calculations

PROJECT: Courtyard at Upper Nyack  
LOCATION: Village of Upper Nyack, NY

JOB #: 03118  
DATE: 02/24/04

BY: JS

Mark One:      Existing                  Developed

Subarea Description:                  Subarea 7, Onsite area draining to Point of Interest 'A'

Sheet Flow:

1. Surface description (table 3-1).....
2. Manning's Roughness Coeff., n (table 3-1).....
3. Flow Length, L (total < or = to 300 ft.).....(ft.)
4. Two year, 24 hr rainfall, P<sub>2</sub>.....(in.)
5. Land Slope, S.....(ft./ft.)

Segment ID:

|             |  |
|-------------|--|
| 342-322     |  |
| Light Brush |  |
| 0.4         |  |
| 200         |  |
| 3.33        |  |
| 0.100       |  |
| 0.32        |  |

6.  $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} S^{0.4}}$                   Compute T<sub>t</sub> = .....(hr.)

= **0.32** (hrs.)

Shallow Concentrated Flow:

1. Surface description (paved or unpaved).....
2. Flow Length, L ..... (ft.)
3. Watercourse Slope, s.....(ft./ft.)
4. Average Velocity, V (figure 3-1)..... (ft./s)

Segment ID:

|         |  |
|---------|--|
| 322-278 |  |
| unpaved |  |
| 350     |  |
| 0.126   |  |
| 5.7     |  |
| 0.02    |  |

6.  $T_t = \frac{L}{3600 V}$                   Compute T<sub>t</sub> = .....(hr.)

= **0.02** (hrs.)

Open Channel Flow (California Method):

|                   |                              |                       |                               |
|-------------------|------------------------------|-----------------------|-------------------------------|
| Flow Length, L:   | (ft.)<br>0                   | (mi.)<br><u>0.000</u> |                               |
| Elevation Change: | (Start )<br>0.0              | (End)<br>0.0          | (Change in ft.)<br><u>0.0</u> |
|                   | $T_t = (11.9L^3/H)^{0.385}$  |                       |                               |
|                   | T <sub>t</sub> = <b>0.00</b> |                       |                               |

= **0.00** (hrs.)

**Total Tc =** **0.34** (hrs.)  
**20.3** (min.)

# LEONARD JACKSON ASSOCIATES

26 Firemens Memorial Drive  
Pomona, NY 10970  
845-354-4382

## Worksheet 3: Time of Concentration (Tc) Calculations

PROJECT: Courtyard at Upper Nyack  
LOCATION: Village of Upper Nyack, NY

JOB #: 03118  
DATE: 02/24/04

BY: JS

Mark One:      Existing              Developed

Subarea Description:              Subarea 8, Onsite area draining to Point of Interest 'D'

Sheet Flow:

1. Surface description (table 3-1).....
2. Manning's Roughness Coeff., n (table 3-1).....
3. Flow Length, L (total < or = to 300 ft.).....(ft.)
4. Two year, 24 hr rainfall, P<sub>2</sub>.....(in.)
5. Land Slope, S.....(ft./ft.)

|             |             |  |
|-------------|-------------|--|
| Segment ID: | 333-328.5   |  |
|             | Light Brush |  |
|             | 0.4         |  |
|             | 60          |  |
|             | 3.33        |  |
|             | 0.075       |  |
|             | 0.14        |  |

6.  $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} S^{0.4}}$               Compute T<sub>t</sub> = .....(hr.)              =      **0.14** (hrs.)

Shallow Concentrated Flow:

1. Surface description (paved or unpaved).....
2. Flow Length, L ..... (ft.)
3. Watercourse Slope, s.....(ft./ft.)
4. Average Velocity, V (figure 3-1)..... (ft./s)

|             |  |  |
|-------------|--|--|
| Segment ID: |  |  |
|             |  |  |
|             |  |  |
|             |  |  |
|             |  |  |
|             |  |  |

6.  $T_t = \frac{L}{3600 V}$               Compute T<sub>t</sub> = .....(hr.)              =      **0.00** (hrs.)

Open Channel Flow (California Method):

|                   |                              |                       |                               |
|-------------------|------------------------------|-----------------------|-------------------------------|
| Flow Length, L:   | (ft.)<br>0                   | (mi.)<br><u>0.000</u> |                               |
| Elevation Change: | (Start)<br>0.0               | (End)<br>0.0          | (Change in ft.)<br><u>0.0</u> |
|                   | $T_t = (11.9L^3/H)^{0.385}$  |                       |                               |
|                   | T <sub>t</sub> = <b>0.00</b> |                       |                               |

=      **0.00** (hrs.)

**Total Tc** =      **0.14** (hrs.)  
                                 **8.2** (min.)

# LEONARD JACKSON ASSOCIATES

26 Firemens Memorial Drive  
Pomona, NY 10970  
845-354-4382

## Worksheet 3: Time of Concentration (Tc) Calculations

PROJECT: Courtyard at Upper Nyack  
LOCATION: Village of Upper Nyack, NY

JOB #: 03118  
DATE: 02/24/04

BY: JS

Mark One:      Existing              Developed

Subarea Description:              Subarea 9, Offsite area draining to Point of Interest 'B'

Sheet Flow:

|                                                                                           |             |           |                                                                           |
|-------------------------------------------------------------------------------------------|-------------|-----------|---------------------------------------------------------------------------|
|                                                                                           | Segment ID: | 276-268.9 |                                                                           |
| 1. Surface description (table 3-1).....                                                   |             | grass     |                                                                           |
| 2. Manning's Roughness Coeff., n (table 3-1).....                                         |             | 0.2       |                                                                           |
| 3. Flow Length, L (total < or = to 300 ft.).....(ft.)                                     |             | 105       |                                                                           |
| 4. Two year, 24 hr rainfall, P <sub>2</sub> .....(in.)                                    |             | 3.33      |                                                                           |
| 5. Land Slope, S.....(ft./ft.)                                                            |             | 0.068     |                                                                           |
| 6. $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} S^{0.4}}$ Compute T <sub>t</sub> = .....(hr.) |             | 0.13      | = <span style="border: 1px solid black; padding: 2px;">0.13 (hrs.)</span> |

Shallow Concentrated Flow:

|                                                                 |             |  |                                                                           |
|-----------------------------------------------------------------|-------------|--|---------------------------------------------------------------------------|
|                                                                 | Segment ID: |  |                                                                           |
| 1. Surface description (paved or unpaved).....                  |             |  |                                                                           |
| 2. Flow Length, L ..... (ft.)                                   |             |  |                                                                           |
| 3. Watercourse Slope, s.....(ft./ft.)                           |             |  |                                                                           |
| 4. Average Velocity, V (figure 3-1)..... (ft./s)                |             |  |                                                                           |
| 6. $T_t = \frac{L}{3600 V}$ Compute T <sub>t</sub> = .....(hr.) |             |  | = <span style="border: 1px solid black; padding: 2px;">0.00 (hrs.)</span> |

Open Channel Flow (California Method):

|                             |                  |       |                                                                           |
|-----------------------------|------------------|-------|---------------------------------------------------------------------------|
|                             | (ft.)            | (mi.) |                                                                           |
| Flow Length, L:             | 0                | 0.000 |                                                                           |
|                             | (Start )         | (End) | (Change in ft.)                                                           |
| Elevation Change:           | 0.0              | 0.0   | 0.0                                                                       |
| $T_t = (11.9L^3/H)^{0.385}$ |                  |       |                                                                           |
|                             | T <sub>t</sub> = | 0.00  | = <span style="border: 1px solid black; padding: 2px;">0.00 (hrs.)</span> |

**Total Tc = 0.13 (hrs.)  
7.7 (min.)**

# LEONARD JACKSON ASSOCIATES

26 Firemens Memorial Drive  
Pomona, NY 10970  
845-354-4382

## Worksheet 3: Time of Concentration (Tc) Calculations

PROJECT: Courtyard at Upper Nyack  
LOCATION: Village of Upper Nyack, NY

JOB #: 03118  
DATE: 02/24/04

BY: JS

Mark One:      Existing              Developed

Subarea Description:              Subarea 10, Offsite area draining to Point of Interest 'A'

Sheet Flow:

|                                                                                           |             |         |  |                      |
|-------------------------------------------------------------------------------------------|-------------|---------|--|----------------------|
|                                                                                           | Segment ID: | 288-282 |  |                      |
| 1. Surface description (table 3-1).....                                                   |             | grass   |  |                      |
| 2. Manning's Roughness Coeff., n (table 3-1).....                                         |             | 0.2     |  |                      |
| 3. Flow Length, L (total < or = to 300 ft.).....(ft.)                                     |             | 100     |  |                      |
| 4. Two year, 24 hr rainfall, P <sub>2</sub> .....(in.)                                    |             | 3.33    |  |                      |
| 5. Land Slope, S.....(ft./ft.)                                                            |             | 0.060   |  |                      |
| 6. $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} S^{0.4}}$ Compute T <sub>t</sub> = .....(hr.) |             | 0.13    |  | = <b>0.13</b> (hrs.) |

Shallow Concentrated Flow:

|                                                                 |             |  |  |                      |
|-----------------------------------------------------------------|-------------|--|--|----------------------|
|                                                                 | Segment ID: |  |  |                      |
| 1. Surface description (paved or unpaved).....                  |             |  |  |                      |
| 2. Flow Length, L ..... (ft.)                                   |             |  |  |                      |
| 3. Watercourse Slope, s.....(ft./ft.)                           |             |  |  |                      |
| 4. Average Velocity, V (figure 3-1)..... (ft./s)                |             |  |  |                      |
| 6. $T_t = \frac{L}{3600 V}$ Compute T <sub>t</sub> = .....(hr.) |             |  |  | = <b>0.00</b> (hrs.) |

Open Channel Flow (California Method):

|                   |                              |              |                 |  |                      |
|-------------------|------------------------------|--------------|-----------------|--|----------------------|
|                   | (ft.)                        | (mi.)        |                 |  |                      |
| Flow Length, L:   | 340                          | <u>0.064</u> |                 |  |                      |
|                   | (Start)                      | (End)        | (Change in ft.) |  |                      |
| Elevation Change: | 282.0                        | 276.0        | <u>6.0</u>      |  |                      |
|                   | $T_t = (11.9L^3/H)^{0.385}$  |              |                 |  |                      |
|                   | T <sub>t</sub> = <b>0.05</b> |              |                 |  | = <b>0.05</b> (hrs.) |

**Total Tc = 0.18 (hrs.)**  
**11.1 (min.)**

# LEONARD JACKSON ASSOCIATES

26 Firemens Memorial Drive  
Pomona, NY 10970  
845-354-4382

## Worksheet 3: Time of Concentration (Tc) Calculations

PROJECT: Courtyard at Upper Nyack  
LOCATION: Village of Upper Nyack, NY

JOB #: 03118  
DATE: 02/24/04

BY: JS

Mark One:      Existing       Developed

Subarea Description:      Subarea 1, Offsite area contributing to stream flowing through the site, to Point of Interest 'A'  
Subarea conditions do not vary between Existing and Developed Conditions

Sheet Flow:

1. Surface description (table 3-1).....
2. Manning's Roughness Coeff., n (table 3-1).....
3. Flow Length, L (total < or = to 300 ft.).....(ft.)
4. Two year, 24 hr rainfall, P<sub>2</sub>.....(in.)
5. Land Slope, S.....(ft./ft.)
6.  $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} S^{0.4}}$       Compute T<sub>t</sub> = .....(hr.)

|             |         |  |
|-------------|---------|--|
| Segment ID: | 575-526 |  |
|             | Unpaved |  |
|             | 0.4     |  |
|             | 200     |  |
|             | 3.33    |  |
|             | 0.245   |  |
|             | 0.22    |  |

= 0.22 (hrs.)

Shallow Concentrated Flow:

1. Surface description (paved or unpaved).....
2. Flow Length, L ..... (ft.)
3. Watercourse Slope, s.....(ft./ft.)
4. Average Velocity, V (figure 3-1)..... (ft./s)
6.  $T_t = \frac{L}{3600 V}$       Compute T<sub>t</sub> = .....(hr.)

|             |           |  |
|-------------|-----------|--|
| Segment ID: | 526-327.2 |  |
|             | unpaved   |  |
|             | 1015      |  |
|             | 0.196     |  |
|             | 7.1       |  |
|             | 0.04      |  |

= 0.04 (hrs.)

Open Channel Flow (California Method):

|                             |             |              |                 |
|-----------------------------|-------------|--------------|-----------------|
|                             | (ft.)       | (mi.)        |                 |
| Flow Length, L:             | 0           | <u>0.000</u> |                 |
|                             | (Start)     | (End)        | (Change in ft.) |
| Elevation Change:           | 0.0         | 0.0          | <u>0.0</u>      |
| $T_t = (11.9L^3/H)^{0.385}$ |             |              |                 |
| T <sub>t</sub> =            | <b>0.00</b> |              |                 |

= 0.00 (hrs.)

**Total Tc =** **0.26 (hrs.)**  
**15.8 (min.)**

# LEONARD JACKSON ASSOCIATES

26 Firemens Memorial Drive  
Pomona, NY 10970  
845-354-4382

## Worksheet 3: Time of Concentration (Tc) Calculations

PROJECT: Courtyard at Upper Nyack  
LOCATION: Village of Upper Nyack, NY

JOB #: 03118  
DATE: 02/24/04

BY: JS

Mark One:      Existing       Developed

Description: Lag Subarea 1 to Point of Interest 'A'

Sheet Flow:

- Segment ID: \_\_\_\_\_
1. Surface description (table 3-1).....
  2. Manning's Roughness Coeff, n (table 3-1).....
  3. Flow Length, L (total < or = to 300 ft.).....(ft.)
  4. Two year, 24 hr rainfall, P<sub>2</sub>.....(in.)
  5. Land Slope, S.....(ft./ft.)
  6.  $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} S^{0.4}}$       Compute T<sub>t</sub> = .....(hr.)

|  |                                                                    |
|--|--------------------------------------------------------------------|
|  |                                                                    |
|  |                                                                    |
|  |                                                                    |
|  |                                                                    |
|  |                                                                    |
|  |                                                                    |
|  | = <span style="border: 1px solid black; padding: 2px;">0.00</span> |

Shallow Concentrated Flow:

- Segment ID: \_\_\_\_\_
1. Surface description (paved or unpaved).....
  2. Flow Length, L ..... (ft.)
  3. Watercourse Slope, s.....(ft./ft.)
  4. Average Velocity, V (figure 3-1)..... (ft./s)
  6.  $T_t = \frac{L}{3600 V}$       Compute T<sub>t</sub> = .....(hr.)

|  |                                                                    |
|--|--------------------------------------------------------------------|
|  |                                                                    |
|  |                                                                    |
|  |                                                                    |
|  |                                                                    |
|  |                                                                    |
|  | = <span style="border: 1px solid black; padding: 2px;">0.00</span> |

Open Channel Flow (California Method):

|                   |                              |              |                 |
|-------------------|------------------------------|--------------|-----------------|
|                   | (ft.)                        | (mi.)        |                 |
| Flow Length, L:   | 650                          | <u>0.123</u> |                 |
|                   | (Start)                      | (End)        | (Change in ft.) |
| Elevation Change: | 327.2                        | 259.6        | <u>67.7</u>     |
|                   | $T_t = (11.9L^3/H)^{0.385}$  |              |                 |
|                   | T <sub>t</sub> = <b>0.05</b> |              |                 |

= 0.05

# LEONARD JACKSON ASSOCIATES

26 Firemens Memorial Drive  
Pomona, NY 10970  
845-354-4382

## Worksheet 3: Time of Concentration (Tc) Calculations

PROJECT: Courtyard at Upper Nyack  
LOCATION: Village of Upper Nyack, NY

JOB #: 03118  
DATE: 08/21/06

BY: PD

Mark One:      Existing       Developed

Subarea Description:      Subarea 2, Offsite area draining through site to Point of Interest 'C'

Sheet Flow:

|                                                                                           |             |           |                      |
|-------------------------------------------------------------------------------------------|-------------|-----------|----------------------|
|                                                                                           | Segment ID: | 347.7-.43 |                      |
| 1. Surface description (table 3-1).....                                                   |             | PAVED     |                      |
| 2. Manning's Roughness Coeff., n (table 3-1).....                                         |             | 0.02      |                      |
| 3. Flow Length, L (total < or = to 300 ft.).....(ft.)                                     |             | 75        |                      |
| 4. Two year, 24 hr rainfall, P <sub>2</sub> .....(in.)                                    |             | 3.33      |                      |
| 5. Land Slope, S.....(ft./ft.)                                                            |             | 0.063     |                      |
| 6. $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} S^{0.4}}$ Compute T <sub>t</sub> = .....(hr.) |             | 0.02      | = <b>0.02 (hrs.)</b> |

Shallow Concentrated Flow:

|                                                                 |             |  |                      |
|-----------------------------------------------------------------|-------------|--|----------------------|
|                                                                 | Segment ID: |  |                      |
| 1. Surface description (paved or unpaved).....                  |             |  |                      |
| 2. Flow Length, L ..... (ft.)                                   |             |  |                      |
| 3. Watercourse Slope, s.....(ft./ft.)                           |             |  |                      |
| 4. Average Velocity, V (figure 3-1)..... (ft./s)                |             |  |                      |
| 6. $T_t = \frac{L}{3600 V}$ Compute T <sub>t</sub> = .....(hr.) |             |  | = <b>0.00 (hrs.)</b> |

Open Channel Flow (California Method):

|                             |             |              |                      |
|-----------------------------|-------------|--------------|----------------------|
|                             | (ft.)       | (mi.)        |                      |
| Flow Length, L:             | 0           | <u>0.000</u> |                      |
|                             | (Start)     | (End)        | (Change in ft.)      |
| Elevation Change:           | 0.0         | 0.0          | <u>0.0</u>           |
| $T_t = (11.9L^3/H)^{0.385}$ |             |              |                      |
| $T_t =$                     | <b>0.00</b> |              | = <b>0.00 (hrs.)</b> |

**Total Tc = 0.02 (hrs.)**  
**1.0 (min.)**

# LEONARD JACKSON ASSOCIATES

26 Firemens Memorial Drive  
Pomona, NY 10970  
845-354-4382

## Worksheet 3: Time of Concentration (Tc) Calculations

PROJECT: Courtyard at Upper Nyack  
LOCATION: Village of Upper Nyack, NY

JOB #: 03118  
DATE: 08/21/06

BY: PD

Mark One:      Existing       Developed

Subarea Description:      Subarea 3, Offsite area draining through site to Point of Interest 'B'

Sheet Flow:

|                                                                                           |             |         |               |
|-------------------------------------------------------------------------------------------|-------------|---------|---------------|
|                                                                                           | Segment ID: | 347-342 |               |
| 1. Surface description (table 3-1).....                                                   |             | PAVED   |               |
| 2. Manning's Roughness Coeff., n (table 3-1).....                                         |             | 0.02    |               |
| 3. Flow Length, L (total < or = to 300 ft.).....(ft.)                                     |             | 60      |               |
| 4. Two year, 24 hr rainfall, P <sub>2</sub> .....(in.)                                    |             | 3.33    |               |
| 5. Land Slope, S.....(ft./ft.)                                                            |             | 0.083   |               |
| 6. $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} S^{0.4}}$ Compute T <sub>t</sub> = .....(hr.) |             | 0.01    | = 0.01 (hrs.) |

Shallow Concentrated Flow:

|                                                                 |             |  |               |
|-----------------------------------------------------------------|-------------|--|---------------|
|                                                                 | Segment ID: |  |               |
| 1. Surface description (paved or unpaved).....                  |             |  |               |
| 2. Flow Length, L ..... (ft.)                                   |             |  |               |
| 3. Watercourse Slope, s.....(ft./ft.)                           |             |  |               |
| 4. Average Velocity, V (figure 3-1)..... (ft/s)                 |             |  |               |
| 6. $T_t = \frac{L}{3600 V}$ Compute T <sub>t</sub> = .....(hr.) |             |  | = 0.00 (hrs.) |

Open Channel Flow (California Method):

|                              |         |              |                 |  |
|------------------------------|---------|--------------|-----------------|--|
|                              | (ft.)   | (mi.)        |                 |  |
| Flow Length, L:              | 0       | <u>0.000</u> |                 |  |
|                              | (Start) | (End)        | (Change in ft.) |  |
| Elevation Change:            | 0.0     | 0.0          | <u>0.0</u>      |  |
| $T_t = (11.9L^3/H)^{0.385}$  |         |              |                 |  |
| T <sub>t</sub> = <b>0.00</b> |         |              |                 |  |

= 0.00 (hrs.)

Total Tc = 0.01 (hrs.)  
0.7 (min.)

# LEONARD JACKSON ASSOCIATES

26 Firemens Memorial Drive  
Pomona, NY 10970  
845-354-4382

## Worksheet 3: Time of Concentration (Tc) Calculations

PROJECT: Courtyard at Upper Nyack  
LOCATION: Village of Upper Nyack, NY

JOB #: 03118  
DATE: 08/21/06

BY: PD

Mark One:      Existing       Developed

Subarea Description:      Subarea 4, Offsite area draining through the site to point of interest 'A'

Sheet Flow:

1. Surface description (table 3-1).....
2. Manning's Roughness Coeff., n (table 3-1).....
3. Flow Length, L (total < or = to 300 ft.).....(ft.)
4. Two year, 24 hr rainfall, P<sub>2</sub>.....(in.)
5. Land Slope, S.....(ft./ft.)

Segment ID:

|         |  |
|---------|--|
| 341-333 |  |
| grass   |  |
| 0.2     |  |
| 20      |  |
| 3.33    |  |
| 0.400   |  |
| 0.02    |  |

6.  $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} S^{0.4}}$

Compute T<sub>t</sub> = .....(hr.)

= **0.02** (hrs.)

Shallow Concentrated Flow:

1. Surface description (paved or unpaved).....
2. Flow Length, L ..... (ft.)
3. Watercourse Slope, s.....(ft./ft.)
4. Average Velocity, V (figure 3-1)..... (ft./s)

Segment ID:

|  |  |
|--|--|
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |

6.  $T_t = \frac{L}{3600 V}$

Compute T<sub>t</sub> = .....(hr.)

= **0.00** (hrs.)

Open Channel Flow (California Method):

|                   |                              |                       |                               |
|-------------------|------------------------------|-----------------------|-------------------------------|
| Flow Length, L:   | (ft.)<br>0                   | (mi.)<br><u>0.000</u> |                               |
| Elevation Change: | (Start)<br>0.0               | (End)<br>0.0          | (Change in ft.)<br><u>0.0</u> |
|                   | $T_t = (11.9L^3/H)^{0.385}$  |                       |                               |
|                   | T <sub>t</sub> = <b>0.00</b> |                       |                               |

= **0.00** (hrs.)

**Total Tc** = **0.02** (hrs.)  
**1.0** (min.)

# LEONARD JACKSON ASSOCIATES

26 Firemens Memorial Drive  
 Pomona, NY 10970  
 845-354-4382

## Worksheet 3: Time of Concentration (Tc) Calculations

PROJECT: Courtyard at Upper Nyack  
 LOCATION: Village of Upper Nyack, NY

JOB #: 03118  
 DATE: 08/21/06

BY: PD

Mark One: Existing  Developed

Subarea Description: Subarea 5

Sheet Flow:

1. Surface description (table 3-1).....
2. Manning's Roughness Coeff., n (table 3-1).....
3. Flow Length, L (total < or = to 300 ft.).....(ft.)
4. Two year, 24 hr rainfall, P<sub>2</sub>.....(in.)
5. Land Slope, S.....(ft./ft.)
6.  $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} S^{0.4}}$  Compute T<sub>t</sub> = .....(hr.)

|             |         |  |
|-------------|---------|--|
| Segment ID: | 341-333 |  |
|             | grass   |  |
|             | 0.2     |  |
|             | 20      |  |
|             | 3.33    |  |
|             | 0.400   |  |
|             | 0.02    |  |

= **0.02** (hrs.)

Shallow Concentrated Flow:

1. Surface description (paved or unpaved).....
2. Flow Length, L ..... (ft.)
3. Watercourse Slope, s.....(ft./ft.)
4. Average Velocity, V (figure 3-1)..... (ft./s)
6.  $T_t = \frac{L}{3600 V}$  Compute T<sub>t</sub> = .....(hr.)

|             |  |  |
|-------------|--|--|
| Segment ID: |  |  |
|             |  |  |
|             |  |  |
|             |  |  |
|             |  |  |
|             |  |  |

= **0.00** (hrs.)

Open Channel Flow (California Method):

|                   |                              |              |                 |
|-------------------|------------------------------|--------------|-----------------|
| Flow Length, L:   | (ft.)                        | (mi.)        |                 |
|                   | 0                            | <u>0.000</u> |                 |
| Elevation Change: | (Start)                      | (End)        | (Change in ft.) |
|                   | 0.0                          | 0.0          | <u>0.0</u>      |
|                   | $T_t = (11.9L^3/H)^{0.385}$  |              |                 |
|                   | T <sub>t</sub> = <b>0.00</b> |              |                 |

= **0.00** (hrs.)

**Total Tc = 0.02 (hrs.)**  
**1.0 (min.)**

# LEONARD JACKSON ASSOCIATES

26 Firemens Memorial Drive  
Pomona, NY 10970  
845-354-4382

## Worksheet 3: Time of Concentration (Tc) Calculations

PROJECT: Courtyard at Upper Nyack  
LOCATION: Village of Upper Nyack, NY

JOB #: 03118  
DATE: 08/21/06

BY: PD

Mark One:      Existing       Developed

Subarea Description:      Subarea 10, Offsite area draining to Point of Interest 'A'

Sheet Flow:

|                                                                                           |             |         |                                                                           |
|-------------------------------------------------------------------------------------------|-------------|---------|---------------------------------------------------------------------------|
|                                                                                           | Segment ID: | 288-282 |                                                                           |
| 1. Surface description (table 3-1).....                                                   |             | grass   |                                                                           |
| 2. Manning's Roughness Coeff., n (table 3-1).....                                         |             | 0.2     |                                                                           |
| 3. Flow Length, L (total < or = to 300 ft.).....(ft.)                                     |             | 100     |                                                                           |
| 4. Two year, 24 hr rainfall, P <sub>2</sub> .....(in.)                                    |             | 3.33    |                                                                           |
| 5. Land Slope, S.....(ft./ft.)                                                            |             | 0.060   |                                                                           |
| 6. $T_t = \frac{0.007 (nL)^{0.8}}{P_2^{0.5} S^{0.4}}$ Compute T <sub>t</sub> = .....(hr.) |             | 0.13    | = <span style="border: 1px solid black; padding: 2px;">0.13 (hrs.)</span> |

Shallow Concentrated Flow:

|                                                                 |             |  |                                                                           |
|-----------------------------------------------------------------|-------------|--|---------------------------------------------------------------------------|
|                                                                 | Segment ID: |  |                                                                           |
| 1. Surface description (paved or unpaved).....                  |             |  |                                                                           |
| 2. Flow Length, L ..... (ft.)                                   |             |  |                                                                           |
| 3. Watercourse Slope, s.....(ft./ft.)                           |             |  |                                                                           |
| 4. Average Velocity, V (figure 3-1)..... (ft./s)                |             |  |                                                                           |
| 6. $T_t = \frac{L}{3600 V}$ Compute T <sub>t</sub> = .....(hr.) |             |  | = <span style="border: 1px solid black; padding: 2px;">0.00 (hrs.)</span> |

Open Channel Flow (California Method):

|                   |                             |       |                 |
|-------------------|-----------------------------|-------|-----------------|
|                   | (ft.)                       | (mi.) |                 |
| Flow Length, L:   | 340                         | 0.064 |                 |
|                   | (Start)                     | (End) | (Change in ft.) |
| Elevation Change: | 282.0                       | 276.0 | 6.0             |
|                   | $T_t = (11.9L^3/H)^{0.385}$ |       |                 |
|                   | T <sub>t</sub> = 0.05       |       |                 |

= 0.05 (hrs.)

**Total Tc** = 0.18 (hrs.)  
11.1 (min.)



Appendix C – Drainage Calculations:

- 1.) *Rational Method Drainage Calculations*
- 2.) *Pollutant Loading Calculations*





PROJECT: Courtyard at Upper Nyack  
 DATE: Aug-06 PD

**Rational Method  
 25 Year Discharge Calculations:**

| Sub-basin Name | Time of Concentration (min.) |           | 25 year Intensity (U.C.) |           | Total Contributing Drainage Area (ac.) |           | C Values |       |      | Breakdown of Existing Drainage Area (ac.) |            |            | Breakdown of Developed Drainage Area (ac.) |            |            | Sum of Area x C |           | 25 year Discharge (cfs) |           |
|----------------|------------------------------|-----------|--------------------------|-----------|----------------------------------------|-----------|----------|-------|------|-------------------------------------------|------------|------------|--------------------------------------------|------------|------------|-----------------|-----------|-------------------------|-----------|
|                | Existing                     | Developed | Existing                 | Developed | Existing                               | Developed | Woods    | Grass | Imp. | Woods                                     | Grass/Lawn | Impervious | Woods                                      | Grass/Lawn | Impervious | Existing        | Developed | Existing                | Developed |
| sub1           | 14.8                         | 14.8      | 5.3                      | 5.3       | 7.75                                   | 7.75      | 0.2      | 0.3   | 0.9  | 4.73                                      | 2.37       | 0.65       | 4.73                                       | 2.37       | 0.65       | 2.24            | 2.24      | 11.87                   | 11.87     |
| sub2           | 1.0                          | 1.0       | 5.5                      | 5.5       | 0.24                                   | 0.10      | 0.2      | 0.3   | 0.9  | 0.00                                      | 0.13       | 0.12       | 0.00                                       | 0.05       | 0.05       | 0.14            | 0.06      | 0.78                    | 0.32      |
| sub3           | 0.7                          | 0.7       | 5.5                      | 5.5       | 0.08                                   | 0.14      | 0.2      | 0.3   | 0.9  | 0.00                                      | 0.06       | 0.03       | 0.01                                       | 0.07       | 0.07       | 0.04            | 0.08      | 0.22                    | 0.45      |
| sub4           | 1.0                          | 1.0       | 5.5                      | 5.5       | 0.19                                   | 0.15      | 0.2      | 0.3   | 0.9  | 0.00                                      | 0.19       | 0.00       | 0.01                                       | 0.07       | 0.07       | 0.06            | 0.09      | 0.32                    | 0.48      |
| sub5           | 21.4                         | 1.0       | 4.6                      | 5.5       | 3.60                                   | 0.12      | 0.2      | 0.3   | 0.9  | 3.60                                      | 0.00       | 0.00       | 0.01                                       | 0.06       | 0.06       | 0.72            | 0.07      | 3.31                    | 0.38      |
| sub6           | 20.7                         | 21.4      | 4.7                      | 4.6       | 1.50                                   | 0.95      | 0.2      | 0.3   | 0.9  | 1.50                                      | 0.00       | 0.00       | 0.55                                       | 0.40       | 0.00       | 0.30            | 0.23      | 1.41                    | 1.06      |
| sub7           | 20.3                         | 12.8      | 4.8                      | 5.5       | 5.93                                   | 5.43      | 0.2      | 0.3   | 0.9  | 5.93                                      | 0.00       | 0.00       | 2.77                                       | 1.33       | 1.33       | 1.19            | 2.15      | 5.63                    | 11.83     |
| sub8           | 8.2                          | 9.6       | 5.5                      | 5.5       | 0.15                                   | 1.90      | 0.2      | 0.3   | 0.9  | 0.15                                      | 0.00       | 0.00       | 1.10                                       | 0.80       | 0.00       | 0.03            | 0.46      | 0.17                    | 2.53      |
| sub9           | 7.7                          | 3.2       | 5.5                      | 5.5       | 0.03                                   | 2.90      | 0.2      | 0.3   | 0.9  | 0.00                                      | 0.03       | 0.00       | 1.03                                       | 0.90       | 0.97       | 0.01            | 1.35      | 0.05                    | 7.42      |
| sub10          | 11.1                         | 11.2      | 5.5                      | 5.5       | 0.16                                   | 0.19      | 0.2      | 0.3   | 0.9  | 0.00                                      | 0.16       | 0.00       | 0.00                                       | 0.19       | 0.00       | 0.05            | 0.06      | 0.26                    | 0.31      |

\*Note: For Rational Equation 25 year Intensity, a minimum Time of Concentration of 1.5 minutes is used.



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Location: **Village of Upper Nyack, NY**  
Job # 03118

By: PD  
Date: 23-Aug-06  
AREA TO BASIN -1

**Pre Development Loadings**

**1) Existing Conditions**

Total Area = 5.43 Ac.  
Impervious Area = 0.000 Ac.  
Pervious Area = 5.43 Ac.

**(a) Calculate Runoff Coefficient  $R_v$**

$$\% \text{ Impervious} = \frac{0}{5.43} \times 100\% = 0.00\%$$

$$\begin{aligned} R_v &= 0.05 & + & 0.009 & \times & \% \text{ Impervious} \\ R_v &= 0.05 & + & 0.009 & \times & 0.00 & = & 0.050 \end{aligned}$$

**(b) Calculate Phosphorous Load**

$$L_{TP} = P \times P_J \times R_v \times C_P \times A \times 0.2267$$

Where;

P = 45 in.  
P<sub>J</sub> = 0.9  
R<sub>v</sub> = 0.050  
C<sub>P</sub> = 0.15 mg/L  
A = 5.43 Ac.

**Existing  $L_{TP}$  = 0.4 lbs./yr.**

**(c) Calculate Nitrogen Load**

$$L_{TN} = P \times P_J \times R_v \times C_P \times A \times 0.2267$$

Where;

P = 45 in.  
P<sub>J</sub> = 0.9  
R<sub>v</sub> = 0.050  
C<sub>P</sub> = 0.78 mg/L  
A = 5.43 Ac.

**Existing  $L_{TN}$  = 1.9 lbs./yr.**

1) Existing Conditions (continued)

(d) Calculate Suspended Solids Load

$$L_{TSS} = P \times P_J \times R_V \times C_P \times A \times 0.2267$$

Where;

$$\begin{aligned} P &= 45 \text{ in.} \\ P_J &= 0.9 \\ R_V &= 0.050 \\ C_P &= 70 \text{ mg/L} \\ A &= 5.43 \text{ Ac.} \end{aligned}$$

|                                                             |
|-------------------------------------------------------------|
| <b>Existing <math>L_{TSS} = 174 \text{ lbs./yr.}</math></b> |
|-------------------------------------------------------------|

---

(e) Calculate BOD Load

$$L_{BOD} = P \times P_J \times R_V \times C_P \times A \times 103$$

Where;

$$\begin{aligned} P &= 45 \text{ in.} \\ P_J &= 0.9 \\ R_V &= 0.050 \\ C_P &= 7.7 \text{ 1,000 col/ml} \\ A &= 5.43 \text{ Ac.} \end{aligned}$$

|                                                                           |
|---------------------------------------------------------------------------|
| <b>Existing <math>L_{BOD} = 8721 \text{ billion colonies /yr.}</math></b> |
|---------------------------------------------------------------------------|

---



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Location: **Village of Upper Nyack, NY**  
Job # 03118

By: PD  
Date: 23-Aug-06

**Post Development Loadings**

**2) Proposed Conditions - Area to Basin 1**

|                 |   |       |     |
|-----------------|---|-------|-----|
| Total Area      | = | 5.43  | Ac. |
| Impervious Area | = | 1.330 | Ac. |
| Pervious Area   | = | 4.100 | Ac. |

**(a) Calculate Runoff Coefficient  $R_v$**

$$\% \text{ Impervious} = \frac{1.33}{5.43} \times 100\% = \mathbf{24.49\%}$$

$$R_v = 0.05 + 0.009 \times \% \text{ Impervious}$$

$$R_v = 0.05 + 0.009 \times 24.49 = \mathbf{0.270}$$

**(b) Proposed Coverage Breakdown**

| Coverage    | Area (sf) | Phos. Loading Conc. | Nit. Loading Conc. | S.S. Loading Conc. | B.O.D. Loading Conc. |
|-------------|-----------|---------------------|--------------------|--------------------|----------------------|
| roof        | 28967     | 0.11                | 1.5                | 19                 | 0.26                 |
| C/R Parking | 28967     | 0.15                | 1.9                | 27                 | 1.8                  |
| landscaping | 120661    | 0                   | 0                  | 37                 | 94                   |
| Lawn        | 57934     | 2.1                 | 9.1                | 602                | 24                   |

**(c) Calculate Pretreatment Phosphorous**

$$L_{TP} = P \times P_J \times R_v \times \text{Weighted Average } C_p \times A \times 0.2267$$

Where;

|                        |   |       |      |
|------------------------|---|-------|------|
| P                      | = | 45    | in.  |
| $P_J$                  | = | 0.9   |      |
| $R_v$                  | = | 0.270 |      |
| Weighted Average $C_p$ | = | 0.5   | mg/L |
| A                      | = | 5.43  | Ac.  |

$$\text{Pretreatment } L_{TP} = \mathbf{7.4 \text{ lbs./yr.}}$$

## 2) Area to Basin 1 (continued)

### (d) Calculate Phosphorous Load

BMP Removal Method: Extended Detention Basin

Removal Rate: 80%

Phosphorous Load:  $7.4 \times (1 - 0.8) = 0.84$  lbs./yr.

---

### (e) Calculate Pretreatment Nitrogen

$$L_{TN} = P \times P_J \times R_V \times \text{Weighted Average } C_P \times A \times 0.2267$$

Where;

$$P = 45 \text{ in.}$$

$$P_J = 0.9$$

$$R_V = 0.270$$

$$\text{Weighted Average } C_P = 2.6 \text{ mg/L}$$

$$A = 5.43 \text{ Ac.}$$

$$\text{Pretreatment } L_{TP} = 35.7 \text{ lbs./yr.}$$

### (f) Calculate Nitrogen Load

BMP Removal Method: Extended Detention Basin

Removal Rate: 60%

Nitrogen Load:  $35.7 \times (1 - 0.6) = 15.28$  lbs./yr.

---

### (g) Calculate Pretreatment Suspended Solids

$$L_{SS} = P \times P_J \times R_V \times \text{Weighted Average } C_P \times A \times 0.2267$$

Where;

$$P = 45 \text{ in.}$$

$$P_J = 0.9$$

$$R_V = 0.270$$

$$\text{Weighted Average } C_P = 172.0 \text{ mg/L}$$

$$A = 5.43 \text{ Ac.}$$

$$\text{Pretreatment } L_{SS} = 2318 \text{ lbs./yr.}$$

### (h) Calculate Suspended Solids Load

BMP Removal Method: Infiltration followed by Filter Strip

Removal Rate: 100%

Suspended Solids Load: 0 lbs./yr.

## 2) Area to Basin 1 (continued)

---

### (i) Calculate Pretreatment BOD

$$L_{BOD} = P \times P_J \times R_V \times \text{Weighted Average } C_p \times A \times 103$$

Where;

$$P = 45 \text{ in.}$$

$$P_J = 0.9$$

$$R_V = 0.270$$

$$\text{Weighted Average } C_p = 54.1 \text{ mg/L}$$

$$A = 5.43 \text{ Ac.}$$

$$\text{Pretreatment } L_{BOD} = 331302$$

### (j) Calculate BOD Load

BMP Removal Method: Infiltration followed by Filter Strip

Removal Rate: 60%

|           |                               |                                     |
|-----------|-------------------------------|-------------------------------------|
| BOD Load: | $331302.3 \times (1 - 0.6) =$ | <b>245998 billion colonies /yr.</b> |
|-----------|-------------------------------|-------------------------------------|



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Project: **Courtyard at Upper Nyack**  
Location: **Village of Upper Nyack, NY**  
Job # 03118

By: PD  
Date: 23-Aug-06  
AREA TO BASIN -2

**Pre Development Loadings**

**1) Existing Conditions**

Total Area = 2.90 Ac.  
Impervious Area = 0.000 Ac.  
Pervious Area = 2.90 Ac.

**(a) Calculate Runoff Coefficient  $R_v$**

$$\% \text{ Impervious} = \frac{0}{2.9} \times 100\% = 0.00\%$$

$$\begin{aligned} R_v &= 0.05 & + & 0.009 & \times & \% \text{ Impervious} \\ R_v &= 0.05 & + & 0.009 & \times & 0.00 & = & 0.050 \end{aligned}$$

**(b) Calculate Phosphorous Load**

$$L_{TP} = P \times P_j \times R_v \times C_p \times A \times 0.2267$$

Where;

P = 45 in.  
P<sub>j</sub> = 0.9  
R<sub>v</sub> = 0.050  
C<sub>p</sub> = 0.15 mg/L  
A = 2.90 Ac.

**Existing  $L_{TP} = 0.2 \text{ lbs./yr.}$**

**(c) Calculate Nitrogen Load**

$$L_{TN} = P \times P_j \times R_v \times C_p \times A \times 0.2267$$

Where;

P = 45 in.  
P<sub>j</sub> = 0.9  
R<sub>v</sub> = 0.050  
C<sub>p</sub> = 0.78 mg/L  
A = 2.90 Ac.

**Existing  $L_{TN} = 1.0 \text{ lbs./yr.}$**

### 1) Existing Conditions (continued)

#### (d) Calculate Suspended Solids Load

$$L_{TSS} = P \times P_J \times R_V \times C_P \times A \times 0.2267$$

Where;

$$\begin{aligned} P &= 45 \text{ in.} \\ P_J &= 0.9 \\ R_V &= 0.050 \\ C_P &= 70 \text{ mg/L} \\ A &= 2.90 \text{ Ac.} \end{aligned}$$

$$\text{Existing } L_{TSS} = 93 \text{ lbs./yr.}$$

---

#### (e) Calculate BOD Load

$$L_{BOD} = P \times P_J \times R_V \times C_P \times A \times 103$$

Where;

$$\begin{aligned} P &= 45 \text{ in.} \\ P_J &= 0.9 \\ R_V &= 0.050 \\ C_P &= 7.7 \text{ 1,000 col/ml} \\ A &= 2.90 \text{ Ac.} \end{aligned}$$

$$\text{Existing } L_{BOD} = 4657 \text{ billion colonies /yr.}$$

---



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Location: **Village of Upper Nyack, NY**  
Job # 03118

By: PD  
Date: 23-Aug-06

**Post Development Loadings**

**2) Proposed Conditions - Area to Basin 2**

|                 |   |       |     |
|-----------------|---|-------|-----|
| Total Area      | = | 2.90  | Ac. |
| Impervious Area | = | 0.970 | Ac. |
| Pervious Area   | = | 1.930 | Ac. |

**(a) Calculate Runoff Coefficient  $R_v$**

$$\% \text{ Impervious} = \frac{0.97}{2.9} \times 100\% = 33.45\%$$

$$R_v = 0.05 + 0.009 \times \% \text{ Impervious}$$

$$R_v = 0.05 + 0.009 \times 33.45 = 0.351$$

**(b) Proposed Coverage Breakdown**

| Coverage    | Area (sf) | Phos. Loading Conc. | Nit. Loading Conc. | S.S. Loading Conc. | B.O.D. Loading Conc. |
|-------------|-----------|---------------------|--------------------|--------------------|----------------------|
| roof        | 21126     | 0.11                | 1.5                | 19                 | 0.26                 |
| C/R Parking | 21126     | 0.15                | 1.9                | 27                 | 1.8                  |
| landscaping | 44866     | 0                   | 0                  | 37                 | 94                   |
| Lawn        | 39204     | 2.1                 | 9.1                | 602                | 24                   |

**(c) Calculate Pretreatment Phosphorous**

$$L_{TP} = P \times P_J \times R_v \times \text{Weighted Average } C_p \times A \times 0.2267$$

Where;

|                        |   |       |      |
|------------------------|---|-------|------|
| P                      | = | 45    | in.  |
| $P_J$                  | = | 0.9   |      |
| $R_v$                  | = | 0.351 |      |
| Weighted Average $C_p$ | = | 0.7   | mg/L |
| A                      | = | 2.90  | Ac.  |

$$\text{Pretreatment } L_{TP} = 6.5 \text{ lbs./yr.}$$

## 2) Area to Basin 2 (continued)

### (d) Calculate Phosphorous Load

BMP Removal Method: Extended Detention Basin

Removal Rate: 80%

Phosphorous Load:  $6.5 \times (1 - 0.8) = 1.16$  lbs./yr.

---

### (e) Calculate Pretreatment Nitrogen

$$L_{TN} = P \times P_J \times R_V \times \text{Weighted Average } C_P \times A \times 0.2267$$

Where;

$$P = 45 \text{ in.}$$

$$P_J = 0.9$$

$$R_V = 0.351$$

$$\text{Weighted Average } C_P = 3.4 \text{ mg/L}$$

$$A = 2.90 \text{ Ac.}$$

$$\text{Pretreatment } L_{TP} = 31.7 \text{ lbs./yr.}$$

### (f) Calculate Nitrogen Load

BMP Removal Method: Extended Detention Basin

Removal Rate: 60%

Nitrogen Load:  $31.7 \times (1 - 0.6) = 12.88$  lbs./yr.

---

### (g) Calculate Pretreatment Suspended Solids

$$L_{SS} = P \times P_J \times R_V \times \text{Weighted Average } C_P \times A \times 0.2267$$

Where;

$$P = 45 \text{ in.}$$

$$P_J = 0.9$$

$$R_V = 0.351$$

$$\text{Weighted Average } C_P = 207.7 \text{ mg/L}$$

$$A = 2.90 \text{ Ac.}$$

$$\text{Pretreatment } L_{SS} = 1941 \text{ lbs./yr.}$$

### (h) Calculate Suspended Solids Load

BMP Removal Method: Infiltration followed by Filter Strip

Removal Rate: 100%

Suspended Solids Load: 0 lbs./yr.

## 2) Area to Basin 2 (continued)

---

### (i) Calculate Pretreatment BOD

$$L_{BOD} = P \times P_J \times R_V \times \text{Weighted Average } C_P \times A \times 103$$

Where;

$$P = 45 \text{ in.}$$

$$P_J = 0.9$$

$$R_V = 0.351$$

$$\text{Weighted Average } C_P = 41.2 \text{ mg/L}$$

$$A = 2.90 \text{ Ac.}$$

$$\text{Pretreatment } L_{BOD} = 174868$$

### (j) Calculate BOD Load

BMP Removal Method: Infiltration followed by Filter Strip

Removal Rate: 60%

|           |                               |                                      |
|-----------|-------------------------------|--------------------------------------|
| BOD Load: | $174867.6 \times (1 - 0.6) =$ | <b>48160.7 billion colonies /yr.</b> |
|-----------|-------------------------------|--------------------------------------|

Appendix D – Water Quality Calculations (Volume and Detention Time):

- 1.) *Required and Provided Water Quality Volume Calculations in Basin 1*
- 2.) *Elevation versus Discharge Calculations for Basin 1*
- 3.) *Required and Provided Water Quality Volume Calculations in Basin 2*
- 4.) *Elevation versus Discharge Calculations for Basin 2*
- 5.) *Elevation versus Discharge Calculations for Diversion Manhole Design*

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**Summary Table #WQ-3:Water Quality Volume Calculations**

Project: **Courtyard at Upper Nyack**  
 Location: **Village of Upper Nyack, NY**  
 JOB # 03118

By: PD  
 Date: 23-Aug-06

**Water Quality Calculations - New Developed Area - Provide 100% WQv**

NYSDEC Required Storage Volume: Sub-Area: Basin 1

Data:

P: 1.3 = 90th Percentile Rainfall Event  
 Rv: 0.2704 = 0.05 + 0.009(I) (Min. Rv =0.2) Use Rv = 0.27041  
 I: 24.49 = Impervious coverage percentage  
 A: 5.43 = Site Area to Basin (in acres)

WQv: 0.159 = Req'd Water Quality Volume (in ac-ft)  
 =  $\frac{(P)(Rv)(A)}{12}$

Total WQv = 0.159 ac-ft

Forebay Requirements:

Minimum Size: 10% of WQv = 0.0159 ac-ft  
 Minimum Depth: 4 ft.

Pond P-5 -Permanent Pool Requirements:

Minimum Size: 50% of WQv = 0.0795 ac-ft  
 Minimum Depth: 4 ft.

**Chart : Forebay Storage Volume:**

| Contour Elev. (ft) | Contour Area                |                            |               |              | Depth (ft) | Total Volume (ft <sup>3</sup> ) | A                    | 1                               | 2                               | 1-2=3                       |
|--------------------|-----------------------------|----------------------------|---------------|--------------|------------|---------------------------------|----------------------|---------------------------------|---------------------------------|-----------------------------|
|                    | Proposed (ft <sup>2</sup> ) | Average (ft <sup>2</sup> ) | Proposed (ac) | Average (ac) |            |                                 | Total Volume (ac-ft) | Cumulative Total Volume (ac-ft) | Required Forebay Volume (ac-ft) | Net Volume Provided (ac-ft) |
| 280                | 68                          | 134                        | 0.0016        | 0.0031       | 1          | 134                             | 0.0031               | 0.0031                          | 0.0159                          | -0.0128                     |
| 281                | 200                         | 340                        | 0.0046        | 0.0078       | 1          | 340                             | 0.0078               | 0.0109                          | 0.0159                          | -0.0050                     |
| 282                | 479                         | 629                        | 0.0110        | 0.0144       | 1          | 629                             | 0.0144               | 0.0253                          | 0.0159                          | 0.0094                      |
| 283                | 779                         | 1021                       | 0.0179        | 0.0234       | 1          | 1021                            | 0.0234               | 0.0487                          | 0.0159                          | 0.0328                      |
| 284                | 1263                        |                            | 0.0290        |              |            |                                 |                      |                                 |                                 |                             |

**Chart : Permanent Pool Storage Volume (Including Forebay Volumes)**

| Contour Elev. (ft) | Contour Area                |                            |               |              | Depth (ft) | Total Volume (ft <sup>3</sup> ) | Total Volume (ac-ft) | 1                                     | 2                               | 1-2=3                               |
|--------------------|-----------------------------|----------------------------|---------------|--------------|------------|---------------------------------|----------------------|---------------------------------------|---------------------------------|-------------------------------------|
|                    | Proposed (ft <sup>2</sup> ) | Average (ft <sup>2</sup> ) | Proposed (ac) | Average (ac) |            |                                 |                      | Total Forebay Volume Provided (ac-ft) | Cumulative Total Volume (ac-ft) | Req'd Permanent Pool Volume (ac-ft) |
| 280                | 68                          | 134                        | 0.0016        | 0.0031       | 1          | 134                             | 0.0031               | 0.0031                                | 0.0159                          | -0.0128                             |
| 281                | 200                         | 340                        | 0.0046        | 0.0078       | 1          | 340                             | 0.0078               | 0.0109                                | 0.0159                          | -0.0050                             |
| 282                | 479                         | 629                        | 0.0110        | 0.0144       | 1          | 629                             | 0.0144               | 0.0253                                | 0.0159                          | 0.0094                              |
| 283                | 779                         | 1021                       | 0.0179        | 0.0234       | 1          | 1021                            | 0.0234               | 0.0487                                | 0.0159                          | 0.0328                              |
| 284                | 1263                        |                            | 0.0290        |              |            |                                 |                      |                                       |                                 |                                     |

|     |      |      |        |        |   |      |        |        |        |        |         |
|-----|------|------|--------|--------|---|------|--------|--------|--------|--------|---------|
| 280 | 449  | 588  | 0.0103 | 0.0135 | 1 | 588  | 0.0135 | 0.0031 | 0.0166 | 0.0795 | -0.0630 |
| 281 | 726  | 920  | 0.0167 | 0.0211 | 1 | 920  | 0.0211 | 0.0078 | 0.0455 | 0.0795 | -0.0341 |
| 282 | 1114 | 1325 | 0.0256 | 0.0304 | 1 | 1325 | 0.0304 | 0.0144 | 0.0903 | 0.0795 | 0.0108  |
| 283 | 1535 | 1802 | 0.0352 | 0.0414 | 1 | 1802 | 0.0414 | 0.0234 | 0.1551 | 0.0795 | 0.0756  |
| 284 | 2068 |      | 0.0475 |        |   |      |        |        |        |        |         |

0.1064 (Sum of individual Perm. Pool Volume)

**Balance of Water Quality Volume:**

|                                             |                      |                                |        |                 |
|---------------------------------------------|----------------------|--------------------------------|--------|-----------------|
|                                             | (Total Req'd Volume) | (Perm. Pool Cumulative Volume) |        |                 |
| *Balance of Required Water Quality Volume = | 0.1591               | -                              | 0.1551 | = 0.0039 ac-ft. |

(100% water quality in permanent pool)

**Chart : Basin Volume (excluding Permanent Pool Volume)**

| Contour Elev. (ft) | Contour Area                |                            |               |              | Depth (ft) | Total Volume (ft <sup>3</sup> ) | Total Volume (ac-ft) | 1                               | 2                                   | 1-2=3                                |
|--------------------|-----------------------------|----------------------------|---------------|--------------|------------|---------------------------------|----------------------|---------------------------------|-------------------------------------|--------------------------------------|
|                    | Proposed (ft <sup>2</sup> ) | Average (ft <sup>2</sup> ) | Proposed (ac) | Average (ac) |            |                                 |                      | Cumulative Total Volume (ac-ft) | *Req'd Water Quality Volume (ac-ft) | Net Volume for Cp, treatment (ac-ft) |
| 284                | 3331                        |                            | 0.0765        |              |            |                                 |                      |                                 |                                     |                                      |
| 286                | 5583                        | 4457                       | 0.1282        | 0.1023       | 2          | 8914                            | 0.2046               | 0.2046                          | 0.004                               | 0.2007                               |
|                    |                             |                            |               |              |            |                                 |                      |                                 |                                     |                                      |
|                    |                             |                            |               |              |            |                                 |                      |                                 |                                     |                                      |

Perm. Pool Elevation = 284.00 ft.

**Set required WQv Elev:**

Elevation: 284.00 ft.

|                                                                     |             |                           |
|---------------------------------------------------------------------|-------------|---------------------------|
| Water Quality Basin Permanent Pool Elevation (WQ <sub>PPE</sub> ) = | Elev. (ft.) | Cumulative Volume (ac-ft) |
|                                                                     | 284.0       |                           |
| Water Quality Storage Elevation Range: High:                        | 286.00      | 0.2046                    |
| Low:                                                                | 284.00      | 0.0000                    |
|                                                                     | Diff. =     | 0.2046                    |

Minimum WQ Volume required above permanent pool = 0.0039 ac-ft

Interpolated Volume Change = ( Higher Cumulative Volume - Req'd WQ Volume over Perm. Pool)/Diff. In Volume in Range

Interpolated Volume Change = ( 0.2046 - 0.0039 ) / 0.2046

Interpolated Volume Ratio = 0.9807

Interpolated Elevation Change = 286.00 - ( 0.9807 x 2.00 )

Interpolated Elevation Change = 284.04 ft.

Minimum Water Quality Volume High Elevation = 284.04 ft.

Set Water Quality Volume Elevation = 284.05 ft.

\*Note: Total Storage at elevation: 284.05 is 0.0051 ac-ft, which is greater than req. WQ<sub>v</sub> of: 0.0039 ac-ft. ok

**Compute the required WQ<sub>v</sub>-ED orifice:**

(Note: ED means extended detention.)

Required WQ<sub>v</sub> = 0.0039 ac-ft.  
 Average ED release rate = 0.0039 x 43560 ft<sup>2</sup>/ac / (24 hr x 3600 sec/hr)  
 Average ED release rate = 0.00 cfs

\*Size WQv-ED orifice  
to release average of : 0.00 - 0.00 cfs

Qavg = 0.00 cfs

Average WQv-ED orifice rate is:  
Average head (h) = (WQ<sub>VE</sub> - WQ<sub>PE</sub>)/2

Average h =  $\frac{284.05 - 284.00}{2}$

Average h = 0.03 ft.

**\*\*Use the orifice flow equation to calculate the required cross-sectional area and diameter for the WQ<sub>v</sub>-ED orifice:**

[Q=ca(sq. rt. (2gh))]

where:

c = 0.61

g = 32.2

Average h = 0.03

sqrt(2gh) = 1.269

a = 0.003 sq. ft.

Based upon: [a=Q/c (sq. rt. (2gh))]

Calculate diameter of pipe based upon area = D = 0.057 ft.

D = 0.687 in.

Based upon: [D = sq. rt. (4a/3.15159)]

For Design, Use a 3.0 in. diameter hole or equivalent area.

Orifice centerline elevation = Orifice invert + (Orifice size in feet/2)

Orifice centerline elevation = 284.00 + 0.13

Orifice centerline elevation = 284.13 ft.

# LEONARD JACKSON ASSOCIATES

Project: Courtyard at Upper Nyack  
 Location: Village of Upper Nyack, NY  
 JOB # 03118

By: PD  
 Date: 23-Aug-06  
 Sub-Area: Basin 1

## Outlet Structure - Elevation vs. Discharge Calculations

Known Data:

|                    |                       |                    |                       |                    |                       |                    |                       |
|--------------------|-----------------------|--------------------|-----------------------|--------------------|-----------------------|--------------------|-----------------------|
| <b>Orifice #1:</b> |                       | <b>Orifice #2:</b> |                       | <b>Orifice #3:</b> |                       | <b>Orifice #4:</b> |                       |
| Orifice Dia.:      | 3.00 in.              | Orifice Dia.:      | 12.00 in.             | Orifice Dia.:      | 0.00 in.              | Orifice Dia.:      | 0.00 in.              |
| Invert El.:        | 284.00 ft.            | Invert El.:        | 285.00 ft.            | Invert El.:        | 532.85 ft.            | Invert El.:        | 532.85 ft.            |
| Centerline El.:    | 284.13 ft.            | Centerline El.:    | 285.50 ft.            | Centerline El.:    | 532.85 ft.            | Centerline El.:    | 532.85 ft.            |
| A=                 | 0.049 ft <sup>2</sup> | A=                 | 0.785 ft <sup>2</sup> | A=                 | 0.000 ft <sup>2</sup> | A=                 | 0.000 ft <sup>2</sup> |

**Spillway #1 (Weir):**

|                      |           |
|----------------------|-----------|
| Spillway Inv. Elev.: | 287.5 ft. |
| Spillway Top Elev.:  | n/a ft.   |
| Spillway Length:     | 3.0 ft.   |

**Spillway #2 (Top Struct.):**

|                      |           |
|----------------------|-----------|
| Spillway Inv. Elev.: | 288.0 ft. |
| Spillway Top Elev.:  | n/a ft.   |
| Spillway Length:     | 12.0 ft.  |

In Orifice Flow Eq. ;  
 $Q=cA[\text{sq. rt. } (2gH)]$

c= 0.61 (orifice #1)  
 c= 0.61 (orifice #2)  
 c= 0.61 (orifice #3)  
 c= 0.61 (orifice #4)  
 c= 0.61 (orifice #5)  
 g= 32.2  
 H= (See Below)

In Weir Flow Eq. ;  
 $Q=cLH^{3/2}$

c= 3.0  
 use L= 3.0 > than el. 287.50 ft.  
 H<sub>4</sub>= (See Below)

H<sub>1</sub>= Height over orifice centerline  
 H<sub>2</sub>= Height over orifice #2 centerline  
 H<sub>3</sub>= Height over orifice #3 centerline  
 H<sub>4</sub>= Height over orifice #4 centerline  
 H<sub>10</sub>= Height over spillway #1 elevation  
 H<sub>11</sub>= Height over spillway #2 elevation

\* c=0.61 for square-edged orifice  
 \*\* c=0.98 for orifice with well-rounded entry  
 (Oct., 1959 Seelye Data Book for Civil Engineers)

## Elevation vs. Discharge

| Elev.<br>(ft.) | Orifice Flows<br>to Orifice #1 |               | Orifice Flows<br>to Orifice #2 |               | Orifice Flows<br>to Orifice #3 |               | Orifice Flows<br>to Orifice #4 |               | Weir Flows<br>over Spillway #1 |               | Weir Flows<br>over Spillway #2 |               | Totals                      |
|----------------|--------------------------------|---------------|--------------------------------|---------------|--------------------------------|---------------|--------------------------------|---------------|--------------------------------|---------------|--------------------------------|---------------|-----------------------------|
|                | H <sub>1</sub><br>(ft.)        | Flow<br>(cfs) | H <sub>2</sub><br>(ft.)        | Flow<br>(cfs) | H <sub>3</sub><br>(ft.)        | Flow<br>(cfs) | H <sub>4</sub><br>(ft.)        | Flow<br>(cfs) | H <sub>10</sub><br>(ft.)       | Flow<br>(cfs) | H <sub>11</sub><br>(ft.)       | Flow<br>(cfs) | Cumulative<br>Flow<br>(cfs) |
| 284.00         | 0.0                            | 0.00          |                                |               |                                |               |                                |               |                                |               |                                |               | 0.00                        |
| 284.20         | 0.1                            | 0.07          |                                |               |                                |               |                                |               |                                |               |                                |               | 0.07                        |
| 284.40         | 0.3                            | 0.13          |                                |               |                                |               |                                |               |                                |               |                                |               | 0.13                        |
| 284.60         | 0.5                            | 0.17          |                                |               |                                |               |                                |               |                                |               |                                |               | 0.17                        |
| 284.80         | 0.7                            | 0.20          |                                |               |                                |               |                                |               |                                |               |                                |               | 0.20                        |
| 285.00         | 0.9                            | 0.22          |                                |               |                                |               |                                |               |                                |               |                                |               | 0.22                        |
| 285.20         | 1.1                            | 0.25          |                                |               |                                |               |                                |               |                                |               |                                |               | 0.25                        |
| 285.40         | 1.3                            | 0.27          |                                |               |                                |               |                                |               |                                |               |                                |               | 0.27                        |
| 285.60         | 1.5                            | 0.29          | 0.1                            | 1.22          |                                |               |                                |               |                                |               |                                |               | 1.51                        |
| 285.80         | 1.7                            | 0.31          | 0.3                            | 2.11          |                                |               |                                |               |                                |               |                                |               | 2.42                        |
| 286.00         | 1.9                            | 0.33          | 0.5                            | 2.72          |                                |               |                                |               |                                |               |                                |               | 3.05                        |
| 286.20         | 2.1                            | 0.35          | 0.7                            | 3.22          |                                |               |                                |               |                                |               |                                |               | 3.56                        |
| 286.40         | 2.3                            | 0.36          | 0.9                            | 3.65          |                                |               |                                |               |                                |               |                                |               | 4.01                        |
| 286.60         | 2.5                            | 0.38          | 1.1                            | 4.03          |                                |               |                                |               |                                |               |                                |               | 4.41                        |
| 286.80         | 2.7                            | 0.39          | 1.3                            | 4.38          |                                |               |                                |               |                                |               |                                |               | 4.78                        |
| 287.00         | 2.9                            | 0.41          | 1.5                            | 4.71          |                                |               |                                |               |                                |               |                                |               | 5.12                        |
| 287.20         | 3.1                            | 0.42          | 1.7                            | 5.01          |                                |               |                                |               |                                |               |                                |               | 5.43                        |
| 287.40         | 3.3                            | 0.43          | 1.9                            | 5.30          |                                |               |                                |               |                                |               |                                |               | 5.73                        |
| 287.60         | 3.5                            | 0.45          | 2.1                            | 5.57          |                                |               |                                |               | 0.1                            | 0.28          |                                |               | 6.30                        |
| 287.80         | 3.7                            | 0.46          | 2.3                            | 5.83          |                                |               |                                |               | 0.3                            | 1.48          |                                |               | 7.77                        |
| 288.00         | 3.9                            | 0.47          | 2.5                            | 6.08          |                                |               |                                |               | 0.5                            | 3.18          | 0.0                            | 0.00          | 9.73                        |
| 288.20         | 4.1                            | 0.49          | 2.7                            | 6.32          |                                |               |                                |               | 0.7                            | 5.27          | 0.2                            | 3.22          | 15.29                       |



|     |      |      |        |        |   |      |        |        |        |        |         |
|-----|------|------|--------|--------|---|------|--------|--------|--------|--------|---------|
| 280 | 147  |      | 0.0034 |        |   |      |        |        |        |        |         |
|     |      | 299  |        | 0.0069 | 1 | 299  | 0.0069 | 0.0016 | 0.0084 | 0.0551 | -0.0467 |
| 281 | 451  |      | 0.0104 |        |   |      |        |        |        |        |         |
|     |      | 631  |        | 0.0145 | 1 | 631  | 0.0145 | 0.0047 | 0.0276 | 0.0551 | -0.0275 |
| 282 | 811  |      | 0.0186 |        |   |      |        |        |        |        |         |
|     |      | 1020 |        | 0.0234 | 1 | 1020 | 0.0234 | 0.0090 | 0.0600 | 0.0551 | 0.0049  |
| 283 | 1228 |      | 0.0282 |        |   |      |        |        |        |        |         |
|     |      | 1465 |        | 0.0336 | 1 | 1465 | 0.0336 | 0.0147 | 0.1083 | 0.0551 | 0.0532  |
| 284 | 1702 |      | 0.0391 |        |   |      |        |        |        |        |         |

0.0784 (Sum of individual Perm. Pool Volume)

**Balance of Water Quality Volume:**

|                                             |                      |                                |        |                 |
|---------------------------------------------|----------------------|--------------------------------|--------|-----------------|
|                                             | (Total Req'd Volume) | (Perm. Pool Cumulative Volume) |        |                 |
| *Balance of Required Water Quality Volume = | 0.1103               | -                              | 0.1083 | = 0.0020 ac-ft. |

(100% water quality in permanent pool)

**Chart : Basin Volume (excluding Permanent Pool Volume)**

| Contour Elev. (ft) | Contour Area                |                            |               |              | Depth (ft) | Total Volume (ft <sup>3</sup> ) | Total Volume (ac-ft) | 1                               | 2                                   | 1-2=3                                           |
|--------------------|-----------------------------|----------------------------|---------------|--------------|------------|---------------------------------|----------------------|---------------------------------|-------------------------------------|-------------------------------------------------|
|                    | Proposed (ft <sup>2</sup> ) | Average (ft <sup>2</sup> ) | Proposed (ac) | Average (ac) |            |                                 |                      | Cumulative Total Volume (ac-ft) | *Req'd Water Quality Volume (ac-ft) | Net Volume for C <sub>p</sub> treatment (ac-ft) |
| 284                | 2479                        | 3470                       | 0.0569        | 0.0796       | 2          | 6939                            | 0.1593               | 0.1593                          | 0.002                               | 0.1573                                          |
| 286                | 4460                        |                            | 0.1024        |              |            |                                 |                      |                                 |                                     |                                                 |
|                    |                             |                            |               |              |            |                                 |                      |                                 |                                     |                                                 |
|                    |                             |                            |               |              |            |                                 |                      |                                 |                                     |                                                 |

Perm. Pool Elevation = 284.00 ft.

**Set required WQv Elev:**

Elevation: 284.00 ft.

|                                                                     |             |                           |
|---------------------------------------------------------------------|-------------|---------------------------|
| Water Quality Basin Permanent Pool Elevation (WQ <sub>PPC</sub> ) = | Elev. (ft.) | Cumulative Volume (ac-ft) |
|                                                                     | 284.0       |                           |
| Water Quality Storage Elevation Range: High:                        | 286.00      | 0.1593                    |
| Low:                                                                | 284.00      | 0.0000                    |
|                                                                     | Diff. =     | 0.1593                    |

Minimum WQ Volume required above permanent pool = 0.0020 ac-ft

Interpolated Volume Change = ( Higher Cumulative Volume - Req'd WQ Volume over Perm. Pool)/Diff. In Volume in Range

Interpolated Volume Change = ( 0.1593 - 0.0020 )/ 0.1593

Interpolated Volume Ratio = 0.9877

Interpolated Elevation Change = 286.00 - ( 0.9877 x 2.00 )

Interpolated Elevation Change = 284.02 ft.

Minimum Water Quality Volume High Elevation = 284.02 ft.

Set Water Quality Volume Elevation = 284.05 ft.

\*Note: Total Storage at elevation: 284.05 is 0.0040 ac-ft, which is greater than req. WQ<sub>v</sub> of: 0.0020 ac-ft. ok

**Compute the required WQ<sub>v</sub>-ED orifice:**

(Note: ED means extended detention.)

Required WQ<sub>v</sub> = 0.0020 ac-ft.  
Average ED release rate = 0.0020 x 43560 ft<sup>2</sup>/ac / (24 hr x 3600 sec/hr)  
Average ED release rate = 0.00 cfs

\*Size WQv-ED orifice  
to release average of : 0.00 - 0.00 cfs

$$Q_{avg} = \underline{0.00} \text{ cfs}$$

Average WQv-ED orifice rate is:  
Average head (h) =  $(WQ_{VE} - WQ_{PE})/2$

$$\text{Average h} = \frac{284.05 - 284.00}{2}$$

$$\text{Average h} = \underline{0.03} \text{ ft.}$$

**\*\*Use the orifice flow equation to calculate the required cross-sectional area and diameter for the WQ<sub>v</sub>-ED orifice:**

$$[Q = ca(\text{sq. ft.} \cdot (2gh))]$$

where:

$$c = 0.61$$

$$g = 32.2$$

$$\text{Average h} = 0.03$$

$$\text{sqrt}(2gh) = 1.269$$

$$a = \underline{0.001} \text{ sq. ft.}$$

Based upon:  $[a = Q/c (\text{sq. ft.} \cdot (2gh))]$

$$\text{Calculate diameter of pipe based upon area} = D = \underline{0.040} \text{ ft.}$$

$$D = \underline{0.483} \text{ in.}$$

Based upon:  $[D = \text{sq. rt.} (4a/3.15159)]$

**For Design, Use a 3.0 in. diameter hole or equivalent area.**

Orifice centerline elevation = Orifice invert + (Orifice size in feet/2)

$$\text{Orifice centerline elevation} = 284.00 + 0.13$$

$$\text{Orifice centerline elevation} = \underline{284.13} \text{ ft.}$$

# LEONARD JACKSON ASSOCIATES

Project: Courtyard at Upper Nyack  
 Location: Village of Upper Nyack, NY  
 JOB # 03118

By: PD  
 Date: 23-Aug-06  
 Sub-Area: Basin 2

## Outlet Structure - Elevation vs. Discharge Calculations

Known Data:

**Orifice #1:**

Orifice Dia.: 3.00 in.  
 Invert El.: 284.00 ft.  
 Centerline El.: 284.13 ft.  
 A= 0.049 ft<sup>2</sup>

**Orifice #2:**

Orifice Dia.: 12.00 in.  
 Invert El.: 284.50 ft.  
 Centerline El.: 285.00 ft.  
 A= 0.785 ft<sup>2</sup>

**Orifice #3:**

Orifice Dia.: 0.00 in.  
 Invert El.: 532.85 ft.  
 Centerline El.: 532.85 ft.  
 A= 0.000 ft<sup>2</sup>

**Orifice #4:**

Orifice Dia.: 0.00 in.  
 Invert El.: 532.85 ft.  
 Centerline El.: 532.85 ft.  
 A= 0.000 ft<sup>2</sup>

**Spillway #1 (Weir):**

Spillway Inv. Elev.: 287.0 ft.  
 Spillway Top Elev.: n/a ft.  
 Spillway Length: 3.0 ft.

**Spillway #2 (Top Struct.):**

Spillway Inv. Elev.: 287.3 ft.  
 Spillway Top Elev.: n/a ft.  
 Spillway Length: 12.0 ft.

In Orifice Flow Eq. ;  
 $Q=cA[\text{sq. ft.} \cdot (2gH)]$

c= 0.61 (orifice #1)  
 c= 0.61 (orifice #2)  
 c= 0.61 (orifice #3)  
 c= 0.61 (orifice #4)  
 c= 0.61 (orifice #5)  
 g= 32.2  
 H= (See Below)

In Weir Flow Eq. ;  
 $Q=cLH^{3/2}$

c= 3.0  
 use L= 3.0 > than el. 287.00 ft.  
 H<sub>4</sub>= (See Below)

\* c=0.61 for square-edged orifice  
 \*\* c=0.98 for orifice with well-rounded entry  
 (Oct., 1959 Seelye Data Book for Civil Engineers)

H<sub>1</sub>= Height over orifice centerline  
 H<sub>2</sub>= Height over orifice #2 centerline  
 H<sub>3</sub>= Height over orifice #3 centerline  
 H<sub>4</sub>= Height over orifice #4 centerline  
 H<sub>10</sub>= Height over spillway #1 elevation  
 H<sub>11</sub>= Height over spillway #2 elevation

## Elevation vs. Discharge

| Elev.<br>(ft.) | Orifice Flows<br>to Orifice #1 |               | Orifice Flows<br>to Orifice #2 |               | Orifice Flows<br>to Orifice #3 |               | Orifice Flows<br>to Orifice #4 |               | Weir Flows<br>over Spillway #1 |               | Weir Flows<br>over Spillway #2 |               | Totals<br>Cumulative<br>Flow<br>(cfs) |
|----------------|--------------------------------|---------------|--------------------------------|---------------|--------------------------------|---------------|--------------------------------|---------------|--------------------------------|---------------|--------------------------------|---------------|---------------------------------------|
|                | H <sub>1</sub><br>(ft.)        | Flow<br>(cfs) | H <sub>2</sub><br>(ft.)        | Flow<br>(cfs) | H <sub>3</sub><br>(ft.)        | Flow<br>(cfs) | H <sub>4</sub><br>(ft.)        | Flow<br>(cfs) | H <sub>10</sub><br>(ft.)       | Flow<br>(cfs) | H <sub>11</sub><br>(ft.)       | Flow<br>(cfs) |                                       |
| 284.00         | 0.0                            | 0.00          |                                |               |                                |               |                                |               |                                |               |                                |               | 0.00                                  |
| 284.20         | 0.1                            | 0.07          |                                |               |                                |               |                                |               |                                |               |                                |               | 0.07                                  |
| 284.40         | 0.3                            | 0.13          |                                |               |                                |               |                                |               |                                |               |                                |               | 0.13                                  |
| 284.60         | 0.5                            | 0.17          |                                |               |                                |               |                                |               |                                |               |                                |               | 0.17                                  |
| 284.80         | 0.7                            | 0.20          |                                |               |                                |               |                                |               |                                |               |                                |               | 0.20                                  |
| 285.00         | 0.9                            | 0.22          | 0.0                            | 0.00          |                                |               |                                |               |                                |               |                                |               | 0.22                                  |
| 285.20         | 1.1                            | 0.25          | 0.2                            | 1.72          |                                |               |                                |               |                                |               |                                |               | 1.97                                  |
| 285.40         | 1.3                            | 0.27          | 0.4                            | 2.43          |                                |               |                                |               |                                |               |                                |               | 2.70                                  |
| 285.60         | 1.5                            | 0.29          | 0.6                            | 2.98          |                                |               |                                |               |                                |               |                                |               | 3.27                                  |
| 285.80         | 1.7                            | 0.31          | 0.8                            | 3.44          |                                |               |                                |               |                                |               |                                |               | 3.75                                  |
| 286.00         | 1.9                            | 0.33          | 1.0                            | 3.84          |                                |               |                                |               |                                |               |                                |               | 4.17                                  |
| 286.20         | 2.1                            | 0.35          | 1.2                            | 4.21          |                                |               |                                |               |                                |               |                                |               | 4.56                                  |
| 286.40         | 2.3                            | 0.36          | 1.4                            | 4.55          |                                |               |                                |               |                                |               |                                |               | 4.91                                  |
| 286.60         | 2.5                            | 0.38          | 1.6                            | 4.86          |                                |               |                                |               |                                |               |                                |               | 5.24                                  |
| 286.80         | 2.7                            | 0.39          | 1.8                            | 5.16          |                                |               |                                |               |                                |               |                                |               | 5.55                                  |
| 287.00         | 2.9                            | 0.41          | 2.0                            | 5.44          |                                |               |                                |               | 0.0                            | 0.00          |                                |               | 5.84                                  |
| 287.20         | 3.1                            | 0.42          | 2.2                            | 5.70          |                                |               |                                |               | 0.2                            | 0.80          |                                |               | 6.93                                  |
| 287.40         | 3.3                            | 0.43          | 2.4                            | 5.96          |                                |               |                                |               | 0.4                            | 2.28          | 0.1                            | 2.09          | 10.76                                 |
| 287.60         | 3.5                            | 0.45          | 2.6                            | 6.20          |                                |               |                                |               | 0.6                            | 4.18          | 0.3                            | 7.45          | 18.28                                 |

# LEONARD JACKSON ASSOCIATES

Project: Courtyard at Upper Nyack  
 Location: Village of Upper Nyack  
 JOB # 03118

By: PD  
 Date: 23-Aug-06

## Diversion Manhole - Elevation vs. Discharge Calculations

Known Data:

**Orifice #1:**

Orifice Dia.: 18.00 in.  
 Invert El.: 274.00 ft.  
 Centerline El.: 274.75 ft.  
 A= 1.767 ft<sup>2</sup>

**Orifice #2:**

Orifice Dia.: 4.00 in.  
 Invert El.: 274.00 ft.  
 Centerline El.: 274.17 ft.  
 A= 0.087 ft<sup>2</sup>

In Orifice Flow Eq. ;

$$Q=cA(\text{sq. rt. } (2gH))$$

c= 0.61 (orifice #1)  
 c= 0.61 (orifice #2)  
 c= 0.61 (orifice #3)  
 c= 0.61 (orifice #4)  
 c= 0.61 (orifice #5)  
 g= 32.2  
 H= (See Below)

c= 0.61 (orifice #6)  
 c= 0.61 (orifice #7)  
 c= 0.61 (orifice #8)  
 c= 0.61 (orifice #9)

H<sub>1</sub>= Head water for 18"Ø pipe - To Point 'A'  
 H<sub>2</sub>= Head water for 4"Ø orifice - To Point 'B'

\* c=0.61 for square-edged orifice  
 \*\* c=0.98 for orifice with well-rounded entry  
 (Oct., 1959 Seelye Data Book for Civil Engineers)

## Elevation vs. Discharge

| Elev.<br>(ft.) | Flows<br>to Point A     |               | Flows<br>to Point B     |               | Total                       |
|----------------|-------------------------|---------------|-------------------------|---------------|-----------------------------|
|                | H <sub>1</sub><br>(ft.) | Flow<br>(cfs) | H <sub>2</sub><br>(ft.) | Flow<br>(cfs) | Cumulative<br>Flow<br>(cfs) |
| 274.00         |                         |               |                         |               | 0.00                        |
| 274.20         |                         |               |                         |               | 0.00                        |
| 274.40         | 0.0                     | 1.09          | 0.2                     | 0.21          | 1.30                        |
| 274.60         | 0.0                     | 1.58          | 0.4                     | 0.28          | 1.86                        |
| 274.80         | 0.0                     | 1.93          | 0.6                     | 0.34          | 2.27                        |
| 275.00         | 0.2                     | 4.33          | 0.8                     | 0.39          | 4.72                        |
| 275.20         | 0.4                     | 5.80          | 1.0                     | 0.43          | 6.24                        |
| 275.40         | 0.6                     | 6.97          | 1.2                     | 0.47          | 7.45                        |
| 275.60         | 0.8                     | 7.98          | 1.4                     | 0.51          | 8.49                        |
| 275.80         | 1.0                     | 8.86          | 1.6                     | 0.55          | 9.41                        |
| 276.00         | 1.2                     | 9.67          | 1.8                     | 0.58          | 10.25                       |
| 276.20         | 1.4                     | 10.42         | 2.0                     | 0.61          | 11.03                       |
| 276.40         | 1.6                     | 11.11         | 2.2                     | 0.64          | 11.75                       |
| 276.60         | 1.8                     | 11.77         | 2.4                     | 0.67          | 12.43                       |
| 276.80         | 2.0                     | 12.39         | 2.6                     | 0.69          | 13.08                       |
| 277.00         | 2.2                     | 12.98         | 2.8                     | 0.72          | 13.69                       |



*Appendix E –Downstream Pipe Analysis:*

*1.) Pipe Flow Calculations for Downstream Storm Drainage System*



## Pipe Flow Calculations For Downstream Storm Drainage System - Existing Conditions

| Point of Interest*                                   | Point A                 | Point C                | Point D                 | Point B                 | Point E                  | Point F                 | Point G                  |
|------------------------------------------------------|-------------------------|------------------------|-------------------------|-------------------------|--------------------------|-------------------------|--------------------------|
| Description                                          | Area draining to HW 'A' | Area draining to CB #8 | Area draining to CB #10 | Area draining to HW 'B' | Area draining to FI #11A | Area draining to CB #12 | Area draining to DMH #19 |
| Drainage Area (acres)                                | **                      | 1.6                    | 8.7                     | **                      | 3.2                      | 1.6                     | 13.8                     |
| 'C' Value                                            | **                      | 0.45                   | 0.45                    | **                      | 0.45                     | 0.45                    | 0.45                     |
| 25-Year Rainfall Intensity <sup>†</sup> (i)          | **                      | 4.3                    | 4.3                     | **                      | 4.3                      | 4.3                     | 4.3                      |
| 100-Year Rainfall Intensity <sup>†</sup> (I)         | **                      | 5.4                    | 5.4                     | **                      | 5.4                      | 5.4                     | 5.4                      |
| 25-Year Discharge for Subarea                        | 23.8                    | 3.0                    | 16.6                    | 0.4                     | 6.2                      | 3.1                     | 26.4                     |
| 100-Year Discharge for Subarea                       | 39.5                    | 3.8                    | 20.8                    | 0.7                     | 7.8                      | 3.9                     | 33.2                     |
| 25-Year Discharge at Point of Interest               | 23.8                    | 26.8                   | 43.4                    | 0.4                     | 6.6                      | 53.0                    | 79.4                     |
| 100-Year Discharge at Point of Interest              | 39.5                    | 43.3                   | 64.2                    | 0.7                     | 8.5                      | 76.5                    | 109.7                    |
| Description of Pipe Leaving Point                    | 24" diameter @ 8.5%     | 30" diameter @ 0.2%    | 30" diameter @ 1%       | 18" diameter @ 24%      | 18" diameter @ 12%       | 36" diameter @ 0.2%     | 36" diameter @ 1.6%      |
| Existing Pipe Capacity <sup>‡</sup>                  | 27 cfs                  | 17 cfs                 | 38 cfs                  | 14 cfs                  | 14 cfs                   | 28 cfs                  | 80 cfs                   |
| Does Pipe Have Capacity for 25-Year / 100-Year Storm | Yes / No                | No / No                | No / No                 | Yes / Yes               | Yes / Yes                | No / No                 | Yes / No                 |

\* Refer to 'Downstream Pipe Analysis Drainage Area Map' for Point of Interest designations

\*\* Flow data for areas draining to HW 'A' and HW 'B' were taken from Hec-1 model output used for Site Drainage Analysis

<sup>†</sup> Rainfall Intensity from 'Rainfall Intensity Curves for Rockland county, NY' based on 25 minute Time of Concentration

<sup>‡</sup> Pipe capacity is based on BPR Design Charts for Open-Channel Flow



**Appendix F – Reference Materials:**

- 1.) *Urban Hydrology for Small Watersheds-Cover sheet*
- 2.) *TR-55 Figure 3-1: Average Velocities for estimating travel time.*
- 3.) *Rainfall intensity curves for Rockland County*
- 4.) *Newyork State Stormwater Management Design Manual-Cover sheet*
- 5.) *Unified Stormwater sizing Criteria*
- 6.) *Appendix A: The Simple Method to Calculate Urban Stormwater Load*
- 7.) *Table A.2 Pollutant Concentrations from Source Areas*
- 8.) *Table 1.1: Urban 'C' Values for use with the Simple Method (mg/l)*
- 9.) *Figure 15: Comparative Pollutant Removal of Urban BMP Designs*



United States  
Department of  
Agriculture

Soil  
Conservation  
Service

Engineering  
Division

Technical  
Release 55

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# Urban Hydrology for Small Watersheds



REPRODUCED BY  
U.S. DEPARTMENT OF COMMERCE  
NATIONAL TECHNICAL  
INFORMATION SERVICE  
SPRINGFIELD, VA. 22161



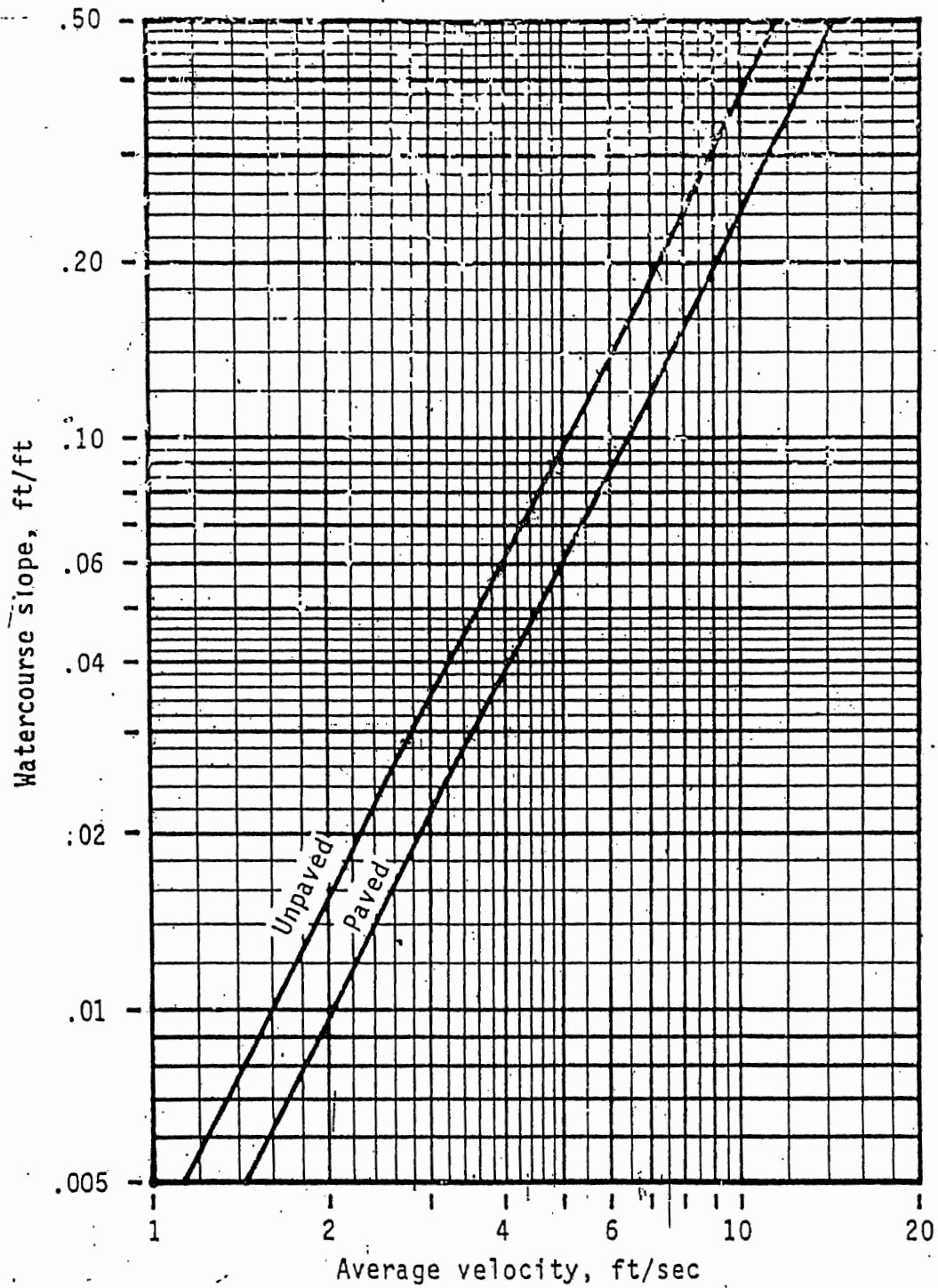
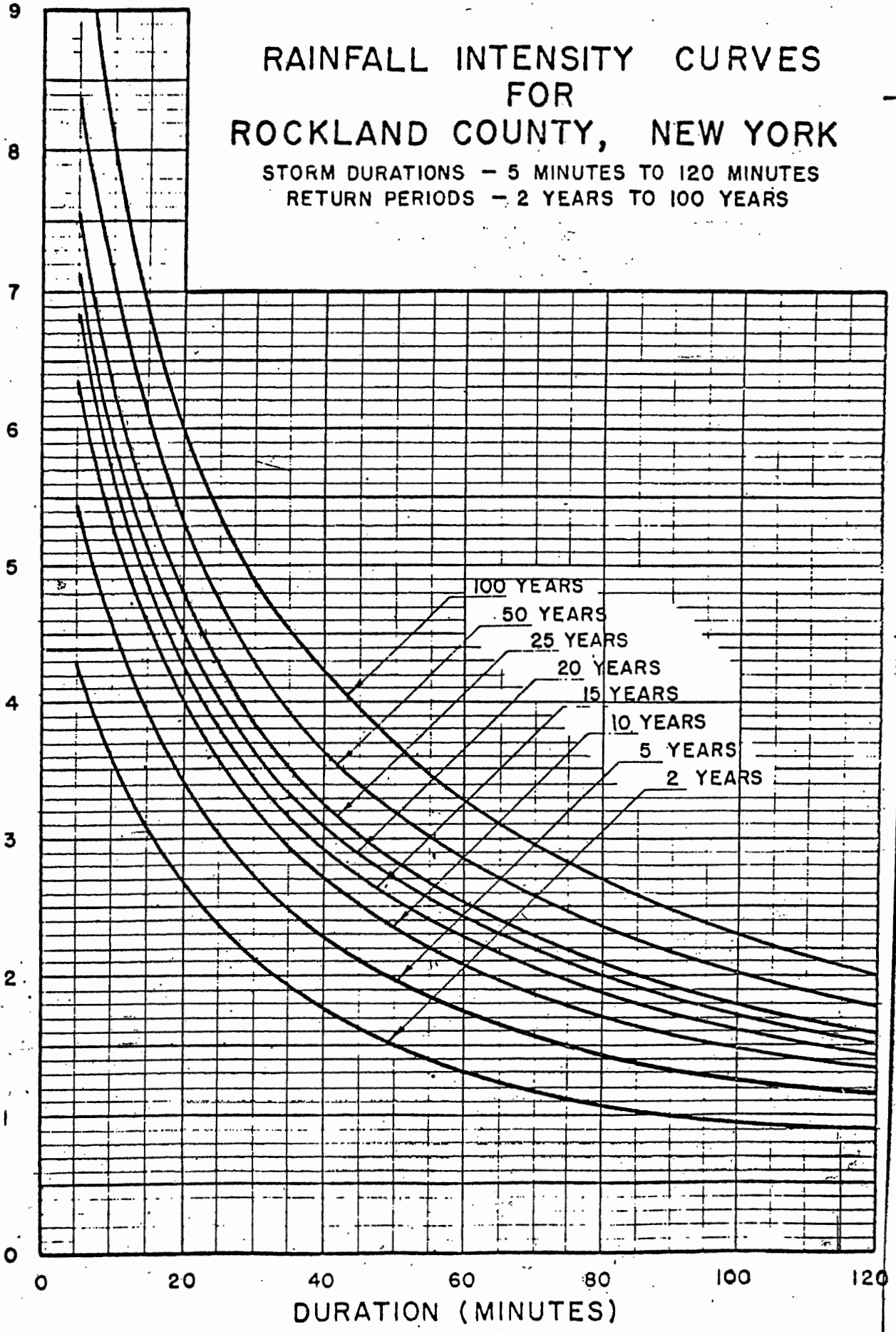


Figure 3-1.—Average velocities for estimating travel time for shallow concentrated flow.

# RAINFALL INTENSITY CURVES FOR ROCKLAND COUNTY, NEW YORK

STORM DURATIONS - 5 MINUTES TO 120 MINUTES  
RETURN PERIODS - 2 YEARS TO 100 YEARS

INTENSITY (INCHES PER HOUR)



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# New York State Stormwater Management Design Manual

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August 2003

Prepared by  
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For:  
New York State  
Department of Environmental Conservation  
625 Broadway  
Albany, NY 12233



George E. Pataki, Governor    Erin M. Crotty, Commissioner

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# Chapter 4

## Unified Stormwater Sizing Criteria

## Chapter 4: Unified Stormwater Sizing Criteria

### Section 4.1 Introduction

This chapter presents a unified approach for sizing SMPs in the State of New York to meet pollutant removal goals, reduce channel erosion, prevent overbank flooding, and help control extreme floods. For a summary, please consult Table 4.1 below. The remaining sections describe the four sizing criteria in detail and present guidance on how to properly compute and apply the required storage volumes.

**Table 4.1 New York Stormwater Sizing Criteria**

|                                                                                                                                                                                                                                                                                            |                                                                                                                                                                                                                                                                                                                                                                                           |
|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| <b>Water Quality (WQ<sub>v</sub>)</b>                                                                                                                                                                                                                                                      | <p><b>90% Rule:</b></p> $WQ_v = [(P)(R_v)(A)] / 12$ $R_v = 0.05 + 0.009(I)$ <p>I = Impervious Cover (Percent)<br/>           Minimum R<sub>v</sub> = 0.2<br/>           P = 90% Rainfall Event Number (See Figure 4.1)<br/>           A = site area in acres</p>                                                                                                                          |
| <b>Channel Protection (C<sub>p</sub><sub>v</sub>)</b>                                                                                                                                                                                                                                      | <p><b>Default Criterion:</b><br/>           C<sub>p</sub><sub>v</sub> = 24 hour extended detention of post-developed 1-year, 24-hour storm event.</p> <p><b>Option for Sites Larger than 50 Acres:</b><br/>           Distributed Runoff Control - geomorphic assessment to determine the bankfull channel characteristics and thresholds for channel stability and bedload movement.</p> |
| <b>Overbank Flood (Q<sub>p</sub>)</b>                                                                                                                                                                                                                                                      | Control the peak discharge from the 10-year storm to 10-year predevelopment rates.                                                                                                                                                                                                                                                                                                        |
| <b>Extreme Storm (Q<sub>f</sub>)</b>                                                                                                                                                                                                                                                       | Control the peak discharge from the 100-year storm to 100-year predevelopment rates.<br>Safely pass the 100-year storm event.                                                                                                                                                                                                                                                             |
| <p><i>Note: Channel protection, overbank flood, and extreme storm requirements may be waived in some instances if the conditions specified in this chapter are met. For SMPs involving dams, follow Appendix A Guidelines for Design of Dams for safe passage of the design flood.</i></p> |                                                                                                                                                                                                                                                                                                                                                                                           |

**Section 4.2 Water Quality Volume (WQ<sub>v</sub>)**

The Water Quality Volume (denoted as the WQ<sub>v</sub>) is designed to improve water quality sizing to capture and treat 90% of the average annual stormwater runoff volume. The WQ<sub>v</sub> is directly related to the amount of impervious cover created at a site. Contour lines of the 90% rainfall event are presented in Figure 4.1.

The following equation can be used to determine the water quality storage volume WQ<sub>v</sub> (in acre-feet of storage):

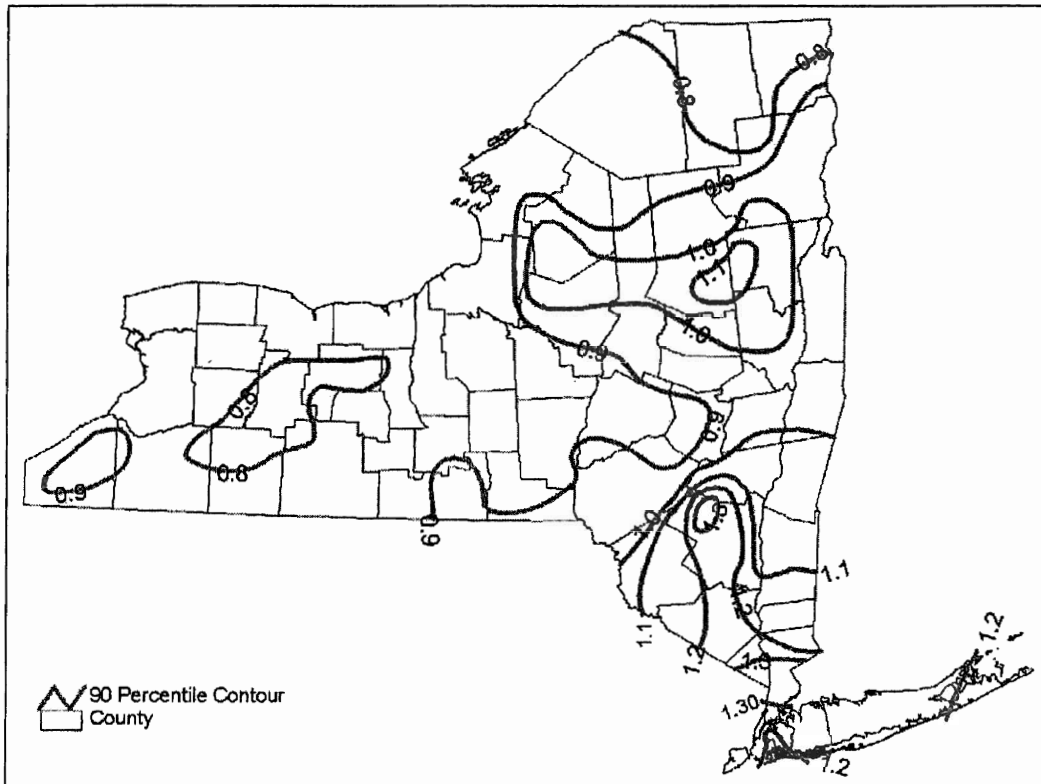
$$WQ_v = \frac{(P)(R_v)(A)}{12}$$

where:

- WQ<sub>v</sub> = water quality volume (in acre-feet)
- P = 90% Rainfall Event Number (see Figure 4.1)
- R<sub>v</sub> = 0.05 + 0.009(I), where I is percent impervious cover
- A = site area in acres (contributing area)

A minimum R<sub>v</sub> of 0.2 will be applied to regulated sites. (tributary area)

**Figure 4.1 90% Rainfall in New York State**



## Appendix A: The Simple Method to Calculate Urban Stormwater Loads

This appendix presents data and methodologies for using the Simple Method (Schueler, 1987) to estimate pollutant load from a site or drainage area. This appendix is meant for planning purposes only, and should not be used for SMP design.

The Simple Method estimates stormwater runoff pollutant loads for urban areas. The technique requires a modest amount of information, including the subwatershed drainage area and impervious cover, stormwater runoff pollutant concentrations, and annual precipitation. With the Simple Method, the investigator can either break up land use into specific areas, such as residential, commercial, industrial, and roadway and calculate annual pollutant loads for each type of land, or utilize more generalized pollutant values for urban runoff. It is also important to note that these values may vary depending on other variables such as the age of development.

The Simple Method estimates pollutant loads for chemical constituents as a product of annual runoff volume and pollutant concentration, as:

$$L = 0.226 * R * C * A$$

Where: L = Annual load (lbs)  
R = Annual runoff (inches)  
C = Pollutant concentration (mg/l)  
A = Area (acres)  
0.226 = Unit conversion factor

For bacteria, the equation is slightly different, to account for the differences in units. The modified equation for bacteria is:

$$L = 103 * R * C * A$$

Where: L = Annual load (Billion Colonies)  
R = Annual runoff (inches)  
C = Bacteria concentration (1,000/ ml)  
A = Area (acres)  
103 = Unit conversion factor

| Table A.2 Pollutant Concentrations from Source Areas                       |                  |                 |                 |                     |                 |                 |                 |
|----------------------------------------------------------------------------|------------------|-----------------|-----------------|---------------------|-----------------|-----------------|-----------------|
| Constituent                                                                | TSS <sup>1</sup> | TP <sup>2</sup> | TN <sup>3</sup> | F Coll <sup>1</sup> | Cu <sup>1</sup> | Pb <sup>1</sup> | Zn <sup>1</sup> |
|                                                                            | mg/l             | mg/L            | mg/l            | 1,000<br>col/ml     | ug/l            | ug/l            | ug/l            |
| Resid Roof                                                                 | 19               | 0.11            | 1.5             | 0.26                | 20              | 21              | 312             |
| Comm Roof                                                                  | 9                | 0.14            | 2.1             | 1.1                 | 7               | 17              | 256             |
| Indust Roof                                                                | 17               | -               | -               | 5.8                 | 62              | 43              | 1,390           |
| C/R Parking                                                                | 27               | 0.15            | 1.9             | 1.8                 | 51              | 28              | 139             |
| Indust<br>Parking                                                          | 228              | -               | -               | 2.7                 | 34              | 85              | 224             |
| Res Street                                                                 | 172              | 0.55            | 1.4             | 37                  | 25              | 51              | 173             |
| Comm Street                                                                | 468              | -               | -               | 12                  | 73              | 170             | 450             |
| Rural<br>Highway                                                           | 51               | -               | 22              | -                   | 22              | 80              | 80              |
| Urban<br>Highway                                                           | 142              | 0.32            | 3.0             | -                   | 54              | 400             | 329             |
| Lawns                                                                      | 602              | 2.1             | 9.1             | 24                  | 17              | 17              | 50              |
| Landscaping                                                                | 37               | -               | -               | 94                  | 94              | 29              | 263             |
| Driveway                                                                   | 173              | 0.56            | 2.1             | 17                  | 17              | -               | 107             |
| Gas Station                                                                | 31               | -               | -               | -                   | 88              | 80              | 290             |
| Auto Recycler                                                              | 335              | -               | -               | -                   | 103             | 182             | 520             |
| Heavy<br>Industrial                                                        | 124              | -               | -               | -                   | 148             | 290             | 1600            |
| 1: Claytor and Schueler (1996)                                             |                  |                 |                 |                     |                 |                 |                 |
| 2: Average of Steuer et al. (1997), Bannerman (1993) and Waschbusch (2000) |                  |                 |                 |                     |                 |                 |                 |
| 3: Steuer et al. (1997)                                                    |                  |                 |                 |                     |                 |                 |                 |

4. NATIONAL RUNOFF CONCENTRATIONS were obtained from over 2300 storms monitored at 22 NURP project sites across the nation (US EPA, 1983). These average values are recommended for use in areas outside of the Middle Atlantic states. The national C values are slightly higher than the values for new suburban sites in the Washington, D.C. area, and slightly lower than values for the older urban areas of Baltimore.
5. NATIONAL URBAN HIGHWAY CONCENTRATIONS were computed from over 250 storm EMC samples collected at eight urban highway sites across the nation as part of a Federal Highway Administration study (Shelley and Gaboury, 1986). The high concentration of metals and phosphate apparently reflects the impact of vehicle emissions. The same study indicated that pollutant concentrations in rural highway runoff were typically one half of the NURP urban runoff average.

The Simple Method has been designed such that any urban storm monitoring dataset can be used as a basis for estimating loads. Thus, if newer or more site specific pollutant concentration data becomes available in the future, the Simple Method can be easily modified to incorporate the new C values. The appropriate procedures for developing new C values are given in Section 3 of Appendix A.

Table 1.1: Urban 'C' Values For Use With the Simple Method (mg/l)

| POLLUTANT         | NEW<br>SUBURBAN<br>NURP SITES<br>(Wash.,DC) | OLDER<br>URBAN<br>AREAS<br>(Baltimore) | CENTRAL<br>BUSINESS<br>DISTRICT<br>(Wash.,DC) | NATIONAL<br>NURP<br>STUDY<br>AVERAGE | HARDWOOD<br>FOREST<br>(Northern<br>Virginia) | NATIONAL<br>URBAN<br>HIGHWAY<br>RUNOFF |
|-------------------|---------------------------------------------|----------------------------------------|-----------------------------------------------|--------------------------------------|----------------------------------------------|----------------------------------------|
| <b>PHOSPHORUS</b> |                                             |                                        |                                               |                                      |                                              |                                        |
| Total             | 0.26                                        | 1.08                                   | -                                             | 0.46                                 | 0.15                                         | -                                      |
| Ortho             | 0.12                                        | 0.26                                   | 1.01                                          | -                                    | 0.02                                         | -                                      |
| Soluble           | 0.16                                        | -                                      | -                                             | 0.16                                 | 0.04                                         | 0.59                                   |
| Organic           | 0.10                                        | 0.82                                   | -                                             | 0.13                                 | 0.11                                         | -                                      |
| <b>NITROGEN</b>   |                                             |                                        |                                               |                                      |                                              |                                        |
| Total             | 2.00                                        | 13.6                                   | 2.17                                          | 3.31                                 | 0.78                                         | -                                      |
| Nitrate           | 0.48                                        | 8.9                                    | 0.84                                          | 0.96                                 | 0.17                                         | -                                      |
| Ammonia           | 0.26                                        | 1.1                                    | -                                             | -                                    | 0.07                                         | -                                      |
| Organic           | 1.25                                        | -                                      | -                                             | -                                    | 0.54                                         | -                                      |
| TKN               | 1.51                                        | 7.2                                    | 1.49                                          | 2.35                                 | 0.61                                         | 2.72                                   |
| COD               | 35.6                                        | 163.0                                  | -                                             | 90.8                                 | >40.0                                        | 124.0                                  |
| BOD (5-day)       | 5.1                                         | -                                      | 36.0                                          | 11.9                                 | -                                            | -                                      |
| <b>METALS</b>     |                                             |                                        |                                               |                                      |                                              |                                        |
| Zinc              | 0.037                                       | 0.397                                  | 0.250                                         | 0.176                                | -                                            | 0.380                                  |
| Lead              | 0.018                                       | 0.389                                  | 0.370                                         | 0.180                                | -                                            | 0.550                                  |
| Copper            | -                                           | 0.105                                  | -                                             | 0.047                                | -                                            | -                                      |

Figure 15: Comparative Pollutant Removal of Urban BMP Designs

| BMP/design                     |                    |                  |                |               |              |          | OVERALL REMOVAL CAPABILITY |
|--------------------------------|--------------------|------------------|----------------|---------------|--------------|----------|----------------------------|
|                                | SUSPENDED SEDIMENT | TOTAL PHOSPHORUS | TOTAL NITROGEN | OXYGEN DEMAND | TRACE METALS | BACTERIA |                            |
| <b>EXTENDED DETENTION POND</b> |                    |                  |                |               |              |          |                            |
| DESIGN 1                       | ●                  | ◐                | ◑              | ◑             | ◑            | ⊗        | MODERATE                   |
| DESIGN 2                       | ●                  | ◐                | ◑              | ◑             | ◑            | ⊗        | MODERATE                   |
| DESIGN 3                       | ●                  | ◐                | ◑              | ◑             | ◑            | ⊗        | HIGH                       |
| <b>WET POND</b>                |                    |                  |                |               |              |          |                            |
| DESIGN 4                       | ●                  | ◐                | ◑              | ◑             | ◑            | ⊗        | MODERATE                   |
| DESIGN 5                       | ●                  | ◐                | ◑              | ◑             | ◑            | ⊗        | MODERATE                   |
| DESIGN 6                       | ●                  | ◐                | ◑              | ◑             | ◑            | ⊗        | HIGH                       |
| <b>INFILTRATION TRENCH</b>     |                    |                  |                |               |              |          |                            |
| DESIGN 7                       | ●                  | ◐                | ◑              | ◑             | ◑            | ●        | MODERATE                   |
| DESIGN 8                       | ●                  | ◐                | ◑              | ◑             | ◑            | ●        | HIGH                       |
| DESIGN 9                       | ●                  | ◐                | ◑              | ◑             | ◑            | ●        | HIGH                       |
| <b>INFILTRATION BASIN</b>      |                    |                  |                |               |              |          |                            |
| DESIGN 7                       | ●                  | ◐                | ◑              | ◑             | ◑            | ●        | MODERATE                   |
| DESIGN 8                       | ●                  | ◐                | ◑              | ◑             | ◑            | ●        | HIGH                       |
| DESIGN 9                       | ●                  | ◐                | ◑              | ◑             | ◑            | ●        | HIGH                       |
| <b>POROUS PAVEMENT</b>         |                    |                  |                |               |              |          |                            |
| DESIGN 7                       | ●                  | ◐                | ◑              | ◑             | ◑            | ●        | MODERATE                   |
| DESIGN 8                       | ●                  | ◐                | ◑              | ◑             | ◑            | ●        | HIGH                       |
| DESIGN 9                       | ●                  | ◐                | ◑              | ◑             | ◑            | ●        | HIGH                       |
| <b>WATER QUALITY INLET</b>     |                    |                  |                |               |              |          |                            |
| DESIGN 10                      | ○                  | ⊗                | ⊗              | ⊗             | ⊗            | ⊗        | LOW                        |
| <b>FILTER STRIP</b>            |                    |                  |                |               |              |          |                            |
| DESIGN 11                      | ◐                  | ○                | ○              | ○             | ◐            | ⊗        | LOW                        |
| DESIGN 12                      | ●                  | ◐                | ◑              | ◑             | ◑            | ⊗        | MODERATE                   |
| <b>GRASSED SWALE</b>           |                    |                  |                |               |              |          |                            |
| DESIGN 13                      | ○                  | ○                | ○              | ○             | ○            | ⊗        | LOW                        |
| DESIGN 14                      | ◐                  | ◑                | ◑              | ◑             | ○            | ⊗        | LOW                        |

KEY:

- 0 TO 20% REMOVAL
- ◐ 20 TO 40% REMOVAL
- ◑ 40 TO 60% REMOVAL
- ◒ 60 TO 80% REMOVAL
- 80 TO 100% REMOVAL
- ⊗ INSUFFICIENT KNOWLEDGE

- Design 1: First-flush runoff volume detained for 6-12 hours.
- Design 2: Runoff volume produced by 1.0 inch, detained 24 hours.
- Design 3: As in Design 2, but with shallow marsh in bottom stage.
- Design 4: Permanent pool equal to 0.5 inch storage per impervious acre.
- Design 5: Permanent pool equal to 2.5 (Vr); where Vr=mean storm runoff.
- Design 6: Permanent pool equal to 4.0 (Vr); approx. 2 weeks retention.
- Design 7: Facility exfiltrates first-flush; 0.5 inch runoff/imper. acre.
- Design 8: Facility exfiltrates one inch runoff volume per imper. acre.
- Design 9: Facility exfiltrates all runoff, up to the 2 year design storm.
- Design 10: 400 cubic feet wet storage per impervious acre.
- Design 11: 20 foot wide turf strip.
- Design 12: 100 foot wide forested strip, with level spreader.
- Design 13: High slope swales, with no check dams.
- Design 14: Low gradient swales with check dams.

(Source: MWCG, 1987)

### Stormwater Pollutant Concentrations

| LAND USE    | POLLUTANT CONCENTRATIONS (mg/l) |                   |                  |                  |
|-------------|---------------------------------|-------------------|------------------|------------------|
|             | TP                              | TN                | TSS              | BOD              |
| Undeveloped | 0.15 <sup>3</sup>               | 0.78 <sup>3</sup> | 70 <sup>1</sup>  | 7.7 <sup>3</sup> |
| Developed   | 0.26 <sup>2</sup>               | 2.00 <sup>2</sup> | 100 <sup>1</sup> | 9.0 <sup>1</sup> |

<sup>1</sup> NURP 50<sup>th</sup> percentile (median) event mean concentration.

<sup>2</sup> New suburban NURP sites (Washington, DC) event mean concentrations.

<sup>3</sup> Hardwood forest, Northern Virginia (NYSDEC 1992) event mean concentrations.

Appendix G - Hec-1 Analyses:

- 1.) Existing Conditions (Hec-1 Model- "ex.h1out")
- 2.) Developed Conditions (Hec-1 Model- "dev.h1out")



# EXISTING CONDITIONS

```

1*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* SEPTEMBER 1990
* VERSION 4.0
* RUN DATE 01/28/2004 TIME 15:10:03
*****
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*****

```

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X X XXXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXX XXXX X
X X X X X X
X X X X X X
X X XXXXXXXX XXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIME- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION.

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMET INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

```

1 ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
LINE HYDROLOGY FOR: COURTYARD AT UPPER NYACK
2 ID VILLAGE OF UPPER NYACK, NY
3 ID
4 ID ANALYSIS PREPARED BY: LEONARD JACKSON ASSOCIATES
5 ID COURTYARD AT UPPER NYACK 03118
6 ID JANUARY 2004
7 ID
8 ID *****
9 ID ANALYSIS PARAMETERS:
10 ID EXISTING CONDITIONS RUN
11 ID STORM RECURRENCE INTERVALS = 2-, 5-, 10-, 25- & 100-YEAR
12 ID HYDROGRAPH METHOD: SCS
13 ID RAINFALL DISTRIBUTION: SCS TYPE III
14 ID *****
15 ID
16 ID
17 ID FOR THE EXISTING CONDITIONS MODEL, 10 SUBAREA WERE UTILIZED, 4 ONSITE
18 ID AND 6 OFFSITE
19 ID
20 ID
21 ID

```

22 ID SUBAREA 1: Offsite area west of the site, contributing to the stream  
 23 ID which runs through the site to Point of Interest 'A'. This  
 24 ID area is unchanged between existing and developed conditions  
 25 ID SUBAREA 2: Offsite area to the west of the site which drains through  
 26 ID the site to Point of Interest 'C'. This area includes a  
 27 ID portion of Route 9W and grass area on the shoulder of the  
 28 ID road.  
 29 ID SUBAREA 3: Offsite area located to the west of the site, and south of  
 30 ID Subarea 3, draining to Point of Interest 'B'. Included in  
 31 ID this area is pavement from Route 9W and grass on the road  
 32 ID shoulder.  
 33 ID SUBAREA 4: Offsite area west of the site between Route 9W and the  
 34 ID site, which drains to Point of Interest 'A'. This area  
 35 ID consists of grass cover.  
 36 ID SUBAREA 5: Onsite area in the northern portion of the site, draining  
 37 ID to Point of Interest 'C'. It is considered to be  
 38 ID completely wooded under existing conditions.  
 39 ID SUBAREA 6: Onsite area in the north-central part of the site, which  
 40 ID drains to Point of Interest 'B', and is completely wooded  
 41 ID for existing conditions.  
 42 ID SUBAREA 7: Onsite area in the central and southern part of the site,  
 43 ID encompassing the majority of the site area. There is an  
 44 ID existing stream which flows through this subarea from  
 45 ID subarea 1, all of which is directed to Point of  
 46 ID Interest 'A'. This area is completely wooded under  
 47 ID existing conditions.  
 48 ID SUBAREA 8: Onsite area located in the southwest portion of the site,  
 49 ID draining to Point of Interest 'D'. For existing conditions  
 50 ID this area is wooded.  
 51 ID SUBAREA 9: Offsite area to the east of the site, consisting of a  
 52 ID drainage swale uphill of Wanamaker Lane. The swale directs  
 53 ID the runoff from Subareas 3 and 6 to Point of Interest 'B'.  
 54 ID SUBAREA 10: Offsite area located to the east of the site, containing a  
 55 ID drainage swale uphill of Wanamaker Lane. This swale  
 HEC-1 INPUT

56 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10  
 57 ID collects the runoff from Subareas 1, 4 and 7 and directs  
 58 ID it to Point of Interest 'A'.  
 59 ID  
 60 ID  
 61 ID  
 62 ID  
 63 ID  
 64 ID  
 65 ID  
 66 ID  
 67 ID  
 68 ID  
 69 ID  
 70 ID  
 71 ID  
 72 ID  
 73 ID  
 74 ID  
 75 ID  
 76 ID  
 77 ID  
 78 ID  
 79 ID  
 80 ID  
 81 ID  
 82 ID  
 83 ID  
 84 ID

EXISTING CONDITIONS HYDROGRAPH COMBINATION:

THE HYDROGRAPHS FOR SUBAREAS 1, 4, 7, AND 10 WERE COMBINED TO GIVE  
 THE PEAK DISCHARGE AT POINT OF INTEREST 'A'  
 THE HYDROGRAPHS FOR SUBAREAS 3, 6, AND 9 WERE COMBINED TO GIVE THE  
 DISCHARGE AT POINT OF INTEREST 'B'  
 THE HYDROGRAPHS FOR SUBAREAS 2 AND 5 WERE COMBINED TO GIVE THE  
 DISCHARGE AT POINT OF INTEREST 'C'  
 THE HYDROGRAPH FOR SUBAREA 8 GIVES THE DISCHARGE AT POINT OF  
 INTEREST 'D'.

\*\*\*\*\*  
 INPUT DATA:  
 \*\*\*\*\*  
 SUBAREA 1: OFFSITE TO PT A      BASIN AREA= 0.02411 SQ MI  
 BA CARD:                              INITIAL RAINFALL LOSS= 1%  
 LU CARD:                              UNIFORM RAINFALL LOSS= 0.1 "/HR  
                                         PERCENT IMPERVIOUS= 15%  
 UC CARD:                              TIME OF CONCENTRATION= .26 HOURS  
                                         SCS CURVE NUMBER = 41.6  
 \*\*\*\*\*  
 SUBAREA 2: OFFSITE TO PT C      BASIN AREA= 0.00038 SQ MI  
 BA CARD:                              INITIAL RAINFALL LOSS= 1%  
 LU CARD:                              UNIFORM RAINFALL LOSS= 0.1 "/HR  
                                         PERCENT IMPERVIOUS= 48%  
 UC CARD:                              TIME OF CONCENTRATION= 0.02 HOUR  
                                         SCS CURVE NUMBER = 49.5  
 \*\*\*\*\*

85 ID SUBAREA 3: OFFSITE TO PT B SUBAREA 4: ONSITE TO PT A  
 86 BA CARD: BASIN AREA= 0.00013 SQ MI BA CARD: BASIN AREA= 0.00030 SQ MI  
 87 LU CARD: INITIAL RAINFALL LOSS= 1" LU CARD: INITIAL RAINFALL LOSS= 1"  
 88 UNIFORM RAINFALL LOSS= 0.1 IN/HOUR UNIFORM RAINFALL LOSS= 0.1 \*/HR  
 89 PERCENT IMPERVIOUS= 31% PERCENT IMPERVIOUS= 0%  
 90 UC CARD: TIME OF CONCENTRATION= .01 HOURS UC CARD: TIME OF CONCENTRATION= 0.02 HOUR  
 91 SCS CURVE NUMBER = 49 SCS CURVE NUMBER = 46.5  
 92  
 93  
 94  
 95 SUBAREA 5: ONSITE TO PT C SUBAREA 6: ONSITE TO PT B  
 96 BA CARD: BASIN AREA= 0.00563 SQ MI BA CARD: BASIN AREA= 0.00235 SQ MI  
 97 LU CARD: INITIAL RAINFALL LOSS= 1" LU CARD: INITIAL RAINFALL LOSS= 1"  
 98 UNIFORM RAINFALL LOSS= 0.1 IN/HOUR UNIFORM RAINFALL LOSS= 0.1 \*/HR  
 99 PERCENT IMPERVIOUS= 0% PERCENT IMPERVIOUS= 0%  
 100 UC CARD: TIME OF CONCENTRATION= .36 HOURS UC CARD: TIME OF CONCENTRATION= 0.34 HOUR  
 101 SCS CURVE NUMBER = 36.6 SCS CURVE NUMBER = 36.85  
 102  
 103  
 104  
 105 SUBAREA 7: ONSITE TO PT A SUBAREA 8: ONSITE TO PT D  
 106 BA CARD: BASIN AREA= 0.00927 SQ MI BA CARD: BASIN AREA= 0.00024 SQ MI  
 107 LU CARD: HEC-1 INPUT LU CARD:  
 108  
 109  
 110  
 111 ID .....1.....2.....3.....4.....5.....6.....7.....8.....9.....10  
 112 ID INITIAL RAINFALL LOSS= 1" INITIAL RAINFALL LOSS= 1"  
 113 ID UNIFORM RAINFALL LOSS= 0.1 IN/HOUR UNIFORM RAINFALL LOSS= 0.1 \*/HR  
 114 ID PERCENT IMPERVIOUS= 0% PERCENT IMPERVIOUS= 0%  
 115 ID UC CARD: TIME OF CONCENTRATION= .34 HOURS UC CARD: TIME OF CONCENTRATION= 0.14 HOUR  
 116 ID SCS CURVE NUMBER = 37.15 SCS CURVE NUMBER = 36  
 117  
 118  
 119 SUBAREA 9: OFFSITE TO PT B SUBAREA 10: OFFSITE TO PT A  
 120 BA CARD: BASIN AREA= 0.00004 SQ MI BA CARD: BASIN AREA= 0.00025 SQ MI  
 121 LU CARD: INITIAL RAINFALL LOSS= 1" LU CARD: INITIAL RAINFALL LOSS= 1"  
 122 UNIFORM RAINFALL LOSS= 0.1 IN/HOUR UNIFORM RAINFALL LOSS= 0.1 \*/HR  
 123 PERCENT IMPERVIOUS= 0% PERCENT IMPERVIOUS= 0%  
 124 UC CARD: TIME OF CONCENTRATION= .13 HOURS UC CARD: TIME OF CONCENTRATION= 0.18 HOUR  
 125 SCS CURVE NUMBER = 55 SCS CURVE NUMBER = 51  
 126  
 127  
 128  
 129  
 130  
 131  
 132 \*\*\*\*\*  
 133 \*DIAGRAM 6 0 0 300  
 134 IT 3 0 0  
 135 JR PREC 3.2 4.2 5.0 5.6 7.2  
 136 KK SUB1\*\*\*\*\*  
 137 KO 1  
 138 BA .02411  
 139 PB 1  
 140 IN 6  
 141 PC 0 0.001 0.002 0.003 0.004 0.005 0.006 0.007 0.008 0.009  
 142 PC 0.010 0.011 0.012 0.013 0.014 0.015 0.016 0.017 0.018 0.019  
 143 PC 0.020 0.021 0.022 0.023 0.024 0.026 0.027 0.028 0.029 0.0295  
 144 PC 0.030 0.031 0.032 0.034 0.035 0.036 0.037 0.038 0.040 0.041  
 145 PC 0.042 0.043 0.045 0.046 0.047 0.049 0.050 0.051 0.053 0.054

|      |    |        |        |        |             |        |        |        |        |        |         |
|------|----|--------|--------|--------|-------------|--------|--------|--------|--------|--------|---------|
| 146  | PC | 0.055  | 0.057  | 0.058  | 0.060       | 0.061  | 0.063  | 0.064  | 0.066  | 0.067  | 0.069   |
| 147  | PC | 0.070  | 0.072  | 0.074  | 0.075       | 0.077  | 0.079  | 0.080  | 0.082  | 0.084  | 0.085   |
| 148  | PC | 0.087  | 0.089  | 0.091  | 0.093       | 0.095  | 0.097  | 0.100  | 0.103  | 0.106  | 0.109   |
| 149  | PC | 0.112  | 0.115  | 0.118  | 0.121       | 0.124  | 0.127  | 0.130  | 0.134  | 0.137  | 0.140   |
| 150  | PC | 0.144  | 0.148  | 0.151  | 0.155       | 0.159  | 0.163  | 0.167  | 0.171  | 0.176  | 0.180   |
| 151  | PC | 0.185  | 0.189  | 0.194  | 0.199       | 0.205  | 0.210  | 0.216  | 0.222  | 0.228  | 0.235   |
| 152  | PC | 0.242  | 0.250  | 0.258  | 0.266       | 0.276  | 0.287  | 0.298  | 0.312  | 0.328  | 0.363   |
| 153  | PC | 0.416  | 0.500  | 0.584  | 0.638       | 0.673  | 0.689  | 0.702  | 0.714  | 0.725  | 0.734   |
| 154  | PC | 0.743  | 0.751  | 0.758  | 0.766       | 0.772  | 0.779  | 0.785  | 0.790  | 0.796  | 0.801   |
| 155  | PC | 0.806  | 0.811  | 0.816  | 0.821       | 0.825  | 0.829  | 0.834  | 0.838  | 0.842  | 0.845   |
| 156  | PC | 0.849  | 0.853  | 0.857  | 0.860       | 0.864  | 0.867  | 0.870  | 0.874  | 0.877  | 0.880   |
| 157  | PC | 0.886  | 0.889  | 0.892  | 0.895       | 0.898  | 0.900  | 0.903  | 0.906  | 0.908  | 0.910   |
| 158  | PC | 0.911  | 0.913  | 0.915  | 0.917       | 0.919  | 0.920  | 0.922  | 0.924  | 0.925  | 0.927   |
| 159  | PC | 0.929  | 0.930  | 0.932  | 0.933       | 0.935  | 0.936  | 0.938  | 0.939  | 0.941  | 0.942   |
| 160  | PC | 0.944  | 0.945  | 0.946  | 0.948       | 0.949  | 0.951  | 0.952  | 0.953  | 0.955  | 0.956   |
| 161  | PC | 0.957  | 0.958  | 0.960  | 0.961       | 0.962  | 0.963  | 0.965  | 0.966  | 0.967  | 0.968   |
| 162  | PC | 0.969  | 0.971  | 0.972  | 0.973       | 0.974  | 0.975  | 0.976  | 0.977  | 0.978  | 0.979   |
| 163  | PC | 0.981  | 0.982  | 0.983  | 0.984       | 0.985  | 0.986  | 0.987  | 0.988  | 0.989  | 0.990   |
|      |    |        |        |        | HEC-1 INPUT |        |        |        |        |        |         |
| LINE | ID | .....1 | .....2 | .....3 | .....4      | .....5 | .....6 | .....7 | .....8 | .....9 | .....10 |
| 164  | PC | 0.991  | 0.992  | 0.993  | 0.994       | 0.995  | 0.996  | 0.997  | 0.998  | 0.999  | 1.000   |
| 165  | LS | 1      | 47     | 15     |             |        |        |        |        |        |         |
| 166  | UD | 0.158  |        |        |             |        |        |        |        |        |         |
| 167  | KK | SUB4   |        |        |             |        |        |        |        |        |         |
| 168  | KK |        |        |        |             |        |        |        |        |        |         |
| 169  | BA | .0003  | 46.5   | 0      |             |        |        |        |        |        |         |
| 170  | LS | 1      |        |        |             |        |        |        |        |        |         |
| 171  | UD | 0.010  |        |        |             |        |        |        |        |        |         |
| 172  | KK | SUB7   |        |        |             |        |        |        |        |        |         |
| 173  | KK |        |        |        |             |        |        |        |        |        |         |
| 174  | BA | .00927 |        |        |             |        |        |        |        |        |         |
| 175  | LS | 1      | 37.15  | 0      |             |        |        |        |        |        |         |
| 176  | UD | 0.203  |        |        |             |        |        |        |        |        |         |
| 177  | KK | SUB10  |        |        |             |        |        |        |        |        |         |
| 178  | KK |        |        |        |             |        |        |        |        |        |         |
| 179  | BA | .00025 |        |        |             |        |        |        |        |        |         |
| 180  | LS | 1      | 51     | 0      |             |        |        |        |        |        |         |
| 181  | UD | 0.111  |        |        |             |        |        |        |        |        |         |
| 182  | KK | COMB A |        |        |             |        |        |        |        |        |         |
| 183  | KK |        |        |        |             |        |        |        |        |        |         |
| 184  | HC | 4      |        |        |             |        |        |        |        |        |         |
|      |    |        |        |        |             |        |        |        |        |        |         |
| 185  | KK | SUB3   |        |        |             |        |        |        |        |        |         |
| 186  | KK |        |        |        |             |        |        |        |        |        |         |
| 187  | BA | .00013 |        |        |             |        |        |        |        |        |         |
| 188  | LS | 1      | 49     | 31     |             |        |        |        |        |        |         |
| 189  | UD | 0.007  |        |        |             |        |        |        |        |        |         |
| 190  | KK | SUB6   |        |        |             |        |        |        |        |        |         |
| 191  | KK |        |        |        |             |        |        |        |        |        |         |
| 192  | BA | .00235 |        |        |             |        |        |        |        |        |         |
| 193  | LS | 1      | 36.85  | 0      |             |        |        |        |        |        |         |
| 194  | UD | 0.207  |        |        |             |        |        |        |        |        |         |
| 195  | KK | SUB9   |        |        |             |        |        |        |        |        |         |
| 196  | KK |        |        |        |             |        |        |        |        |        |         |
| 197  | BA | .00004 |        |        |             |        |        |        |        |        |         |
| 198  | LS | 1      | 55     | 0      |             |        |        |        |        |        |         |
| 199  | UD | 0.077  |        |        |             |        |        |        |        |        |         |
| 200  | KK | COMB B |        |        |             |        |        |        |        |        |         |

KM COMBINED RUNOFF DRAINING TO POINT OF INTEREST 'B'

201 HC 3  
 202  
 203 KK SUB2\*  
 204 KM  
 205 BA .00038  
 206 LS 1 49.5 48  
 207 UD 0.010

HEC-1 INPUT  
 ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

208 KK SUB5\*  
 209 KM  
 210 BA .00563  
 211 LS 1 36.6 0  
 212 UD 0.214

KK COME C\*  
 KM COMBINED RUNOFF DRAINING TO POINT OF INTEREST 'C'

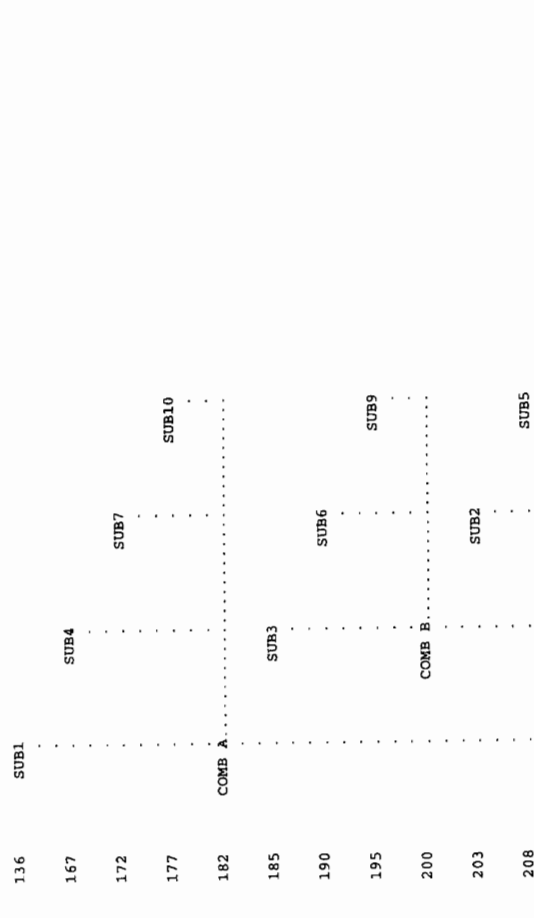
213 HC 2  
 214  
 215  
 216 KK SUB8\*  
 217 KM TOTAL RUNOFF DRAINING TO POINT OF INTEREST 'D'

218 BA .00024  
 219 LS 1 36 0  
 220 UD 0.082  
 221 ZZ

1 SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW

NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW





Interest 'A'. This area is completely wooded under existing conditions.

SUBAREA 8: Onsite area located in the southwest portion of the site, draining to Point of Interest 'D'. For existing conditions this area is wooded.

SUBAREA 9: Offsite area to the east of the site, consisting of a drainage swale uphill of Wanamaker Lane. The swale directs the runoff from Subareas 3 and 6 to Point of Interest 'B'.

SUBAREA 10: Offsite area located to the east of the site, containing a drainage swale uphill of Wanamaker Lane. This swale collects the runoff from Subareas 1, 4 and 7 and directs it to Point of Interest 'A'.

EXISTING CONDITIONS HYDROGRAPH COMBINATION:

THE HYDROGRAPHS FOR SUBAREAS 1, 4, 7, AND 10 WERE COMBINED TO GIVE THE PEAK DISCHARGE AT POINT OF INTEREST 'A'.  
 THE HYDROGRAPHS FOR SUBAREAS 3, 6, AND 9 WERE COMBINED TO GIVE THE DISCHARGE AT POINT OF INTEREST 'B'.  
 THE HYDROGRAPHS FOR SUBAREAS 2 AND 5 WERE COMBINED TO GIVE THE DISCHARGE AT POINT OF INTEREST 'C'.  
 THE HYDROGRAPH FOR SUBAREA 8 GIVES THE DISCHARGE AT POINT OF INTEREST 'D'.

\*\*\*\*\*  
 INPUT DATA  
 \*\*\*\*\*

|                                           |                                           |
|-------------------------------------------|-------------------------------------------|
| SUBAREA 1: OFFSITE TO PT A                | SUBAREA 2: OFFSITE TO PT C                |
| BA CARD: BASIN AREA= 0.02411 SQ MI        | BA CARD: BASIN AREA= 0.00038 SQ MI        |
| LU CARD: INITIAL RAINFALL LOSS= 1*        | LU CARD: INITIAL RAINFALL LOSS= 1*        |
| UNIFORM RAINFALL LOSS= 0.1 IN/HOUR        | UNIFORM RAINFALL LOSS= 0.1 */HR           |
| PERCENT IMPERVIOUS= 15%                   | PERCENT IMPERVIOUS= 48%                   |
| UC CARD: TIME OF CONCENTRATION= .26 HOURS | UC CARD: TIME OF CONCENTRATION= 0.02 HOUR |
| SCS CURVE NUMBER = 41.6                   | SCS CURVE NUMBER = 49.5                   |
| SUBAREA 3: OFFSITE TO PT B                | SUBAREA 4: ONSITE TO PT A                 |
| BA CARD: BASIN AREA= 0.00013 SQ MI        | BA CARD: BASIN AREA= 0.00030 SQ MI        |
| LU CARD: INITIAL RAINFALL LOSS= 1*        | LU CARD: INITIAL RAINFALL LOSS= 1*        |
| UNIFORM RAINFALL LOSS= 0.1 IN/HOUR        | UNIFORM RAINFALL LOSS= 0.1 */HR           |
| PERCENT IMPERVIOUS= 31%                   | PERCENT IMPERVIOUS= 0%                    |
| UC CARD: TIME OF CONCENTRATION= .01 HOURS | UC CARD: TIME OF CONCENTRATION= 0.02 HOUR |
| SCS CURVE NUMBER = 49                     | SCS CURVE NUMBER = 46.5                   |
| SUBAREA 5: ONSITE TO PT C                 | SUBAREA 6: ONSITE TO PT B                 |
| BA CARD: BASIN AREA= 0.00563 SQ MI        | BA CARD: BASIN AREA= 0.00235 SQ MI        |
| LU CARD: INITIAL RAINFALL LOSS= 1*        | LU CARD: INITIAL RAINFALL LOSS= 1*        |
| UNIFORM RAINFALL LOSS= 0.1 IN/HOUR        | UNIFORM RAINFALL LOSS= 0.1 */HR           |
| PERCENT IMPERVIOUS= 0%                    | PERCENT IMPERVIOUS= 0%                    |
| UC CARD: TIME OF CONCENTRATION= .36 HOURS | UC CARD: TIME OF CONCENTRATION= 0.34 HOUR |
| SCS CURVE NUMBER = 36.6                   | SCS CURVE NUMBER = 36.85                  |
| SUBAREA 7: ONSITE TO PT A                 | SUBAREA 8: ONSITE TO PT D                 |
| BA CARD: BASIN AREA= 0.00927 SQ MI        | BA CARD: BASIN AREA= 0.00024 SQ MI        |
| LU CARD: INITIAL RAINFALL LOSS= 1*        | LU CARD: INITIAL RAINFALL LOSS= 1*        |
| UNIFORM RAINFALL LOSS= 0.1 IN/HOUR        | UNIFORM RAINFALL LOSS= 0.1 */HR           |
| PERCENT IMPERVIOUS= 0%                    | PERCENT IMPERVIOUS= 0%                    |
| UC CARD: TIME OF CONCENTRATION= .36 HOURS | UC CARD: TIME OF CONCENTRATION= 0.34 HOUR |
| SCS CURVE NUMBER = 36.6                   | SCS CURVE NUMBER = 36.85                  |

PERCENT IMPERVIOUS= 0%  
 UC CARD:  
 TIME OF CONCENTRATION= 0.14 HOUR  
 SCS CURVE NUMBER = 36

PERCENT IMPERVIOUS= 0%  
 UC CARD:  
 TIME OF CONCENTRATION= .34 HOURS  
 SCS CURVE NUMBER = 37.15

SUBAREA 9: OFFSITE TO FT B  
 BA CARD:  
 BASIN AREA= 0.00004 SQ MI  
 LU CARD:  
 INITIAL RAINFALL LOSS= 1\*  
 UNIFORM RAINFALL LOSS= 0.1 IN/HOUR  
 PERCENT IMPERVIOUS= 0%  
 UC CARD:  
 TIME OF CONCENTRATION= .13 HOURS  
 SCS CURVE NUMBER = 55

SUBAREA 10: OFFSITE TO PT A  
 BA CARD:  
 BASIN AREA= 0.00025 SQ MI  
 LU CARD:  
 INITIAL RAINFALL LOSS= 1\*  
 UNIFORM RAINFALL LOSS= 0.1 "/HR  
 PERCENT IMPERVIOUS= 0%  
 UC CARD:  
 TIME OF CONCENTRATION= 0.18 HOUR  
 SCS CURVE NUMBER = 51

\*\*\*\*\*

134 IO OUTPUT CONTROL VARIABLES  
 IPRINT 3 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCALE 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
 NMIN 6 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1 0 STARTING DATE  
 ITIME 0000 STARTING TIME  
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 2 0 ENDING DATE  
 NDTIME 0554 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .10 HOURS  
 TOTAL TIME BASE 29.90 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRES-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION 1 NUMBER OF PLANS  
 MPLAN

JR MULTI-RATIO OPTION  
 RATIOS OF PRECIPITATION 3.20 4.20 5.00 5.60 7.20

\*\*\*\*\*

136 KK \*\*\*\*\*  
 \* \* SUB1 \* \*\*\*\*\*

137 KO OUTPUT CONTROL VARIABLES  
 IPRINT 3 PRINT CONTROL



CUMULATIVE AREA = .02 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SUB1  
FOR PLAN 1, RATIO = 3.20

TOTAL RAINFALL = 3.20, TOTAL LOSS = 2.41, TOTAL EXCESS = .79

| PEAK FLOW TIME | 6-HR | 24-HR | 72-HR | 29.90-HR |
|----------------|------|-------|-------|----------|
| (CFS)          |      |       |       |          |
| + 8. 12.30     | 1.   | 1.    | 0.    | 0.       |
|                | .560 | .785  | .785  | .785     |
|                | 1.   | 1.    | 1.    | 1.       |

CUMULATIVE AREA = .02 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SUB1  
FOR PLAN 1, RATIO = 4.20

TOTAL RAINFALL = 4.20, TOTAL LOSS = 2.97, TOTAL EXCESS = 1.23

| PEAK FLOW TIME | 6-HR | 24-HR | 72-HR | 29.90-HR |
|----------------|------|-------|-------|----------|
| (CFS)          |      |       |       |          |
| + 13. 12.30    | 2.   | 1.    | 1.    | 1.       |
|                | .905 | 1.230 | 1.231 | 1.231    |
|                | 1.   | 2.    | 2.    | 2.       |

CUMULATIVE AREA = .02 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SUB1  
FOR PLAN 1, RATIO = 5.00

TOTAL RAINFALL = 5.00, TOTAL LOSS = 3.36, TOTAL EXCESS = 1.64

| PEAK FLOW TIME | 6-HR  | 24-HR | 72-HR | 29.90-HR |
|----------------|-------|-------|-------|----------|
| (CFS)          |       |       |       |          |
| + 18. 12.30    | 3.    | 1.    | 1.    | 1.       |
|                | 1.226 | 1.639 | 1.640 | 1.640    |
|                | 2.    | 2.    | 2.    | 2.       |

CUMULATIVE AREA = .02 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SUB1  
FOR PLAN 1, RATIO = 5.60

TOTAL RAINFALL = 5.60, TOTAL LOSS = 3.63, TOTAL EXCESS = 1.97

| PEAK FLOW TIME | 6-HR | 24-HR | 72-HR | 29.90-HR |
|----------------|------|-------|-------|----------|
| (CFS)          |      |       |       |          |
| + 6-HR         |      |       |       |          |
|                |      |       |       |          |





\*\*\*  
 HYDROGRAPH AT STATION SUB4  
 FOR PLAN 1, RATIO = 5.00  
 TOTAL RAINFALL = 5.00, TOTAL LOSS = 3.97, TOTAL EXCESS = 1.03  
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
 (CFS) (HR) 24-HR 72-HR 29.90-HR  
 + 0. 12.20 0. 0. 0.  
 (INCHES) .843 1.032 1.032 1.032  
 (AC-FT) 0. 0. 0.  
 CUMULATIVE AREA = .00 SQ MI

\*\*\*  
 HYDROGRAPH AT STATION SUB4  
 FOR PLAN 1, RATIO = 5.60  
 TOTAL RAINFALL = 5.60, TOTAL LOSS = 4.29, TOTAL EXCESS = 1.31  
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
 (CFS) (HR) 24-HR 72-HR 29.90-HR  
 + 0. 12.20 0. 0. 0.  
 (INCHES) 1.073 1.314 1.314 1.314  
 (AC-FT) 0. 0. 0.  
 CUMULATIVE AREA = .00 SQ MI

\*\*\*  
 HYDROGRAPH AT STATION SUB4  
 FOR PLAN 1, RATIO = 7.20  
 TOTAL RAINFALL = 7.20, TOTAL LOSS = 5.03, TOTAL EXCESS = 2.17  
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
 (CFS) (HR) 24-HR 72-HR 29.90-HR  
 + 0. 12.20 0. 0. 0.  
 (INCHES) 1.767 2.171 2.171 2.171  
 (AC-FT) 0. 0. 0.  
 CUMULATIVE AREA = .00 SQ MI

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\*\*\*\*\*  
 172 KK \* SUB7 \*  
 \*\*\*\*\*



FOR PLAN 1, RATIO = 3.20

TOTAL RAINFALL = 3.20, TOTAL LOSS = 2.95, TOTAL EXCESS = .25

| PEAK FLOW                   | TIME  | 6-HR     | 24-HR | 72-HR | 29.90-HR |
|-----------------------------|-------|----------|-------|-------|----------|
| (CFS)                       | (HR)  |          |       |       |          |
| +                           | 1.    | 0.       | 0.    | 0.    | 0.       |
|                             | 12.40 | .202     | .253  | .253  | .253     |
|                             |       | (INCHES) |       |       |          |
|                             |       | (AC-FT)  | 0.    | 0.    | 0.       |
| CUMULATIVE AREA = .01 SQ MI |       |          |       |       |          |

\*\*\*

HYDROGRAPH AT STATION SUB7  
FOR PLAN 1, RATIO = 4.20

TOTAL RAINFALL = 4.20, TOTAL LOSS = 3.69, TOTAL EXCESS = .51

| PEAK FLOW                   | TIME  | 6-HR     | 24-HR | 72-HR | 29.90-HR |
|-----------------------------|-------|----------|-------|-------|----------|
| (CFS)                       | (HR)  |          |       |       |          |
| +                           | 2.    | 0.       | 0.    | 0.    | 0.       |
|                             | 12.40 | .412     | .509  | .509  | .509     |
|                             |       | (INCHES) |       |       |          |
|                             |       | (AC-FT)  | 0.    | 0.    | 0.       |
| CUMULATIVE AREA = .01 SQ MI |       |          |       |       |          |

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HYDROGRAPH AT STATION SUB7  
FOR PLAN 1, RATIO = 5.00

TOTAL RAINFALL = 5.00, TOTAL LOSS = 4.24, TOTAL EXCESS = .76

| PEAK FLOW                   | TIME  | 6-HR     | 24-HR | 72-HR | 29.90-HR |
|-----------------------------|-------|----------|-------|-------|----------|
| (CFS)                       | (HR)  |          |       |       |          |
| +                           | 3.    | 1.       | 0.    | 0.    | 0.       |
|                             | 12.40 | .620     | .765  | .765  | .765     |
|                             |       | (INCHES) |       |       |          |
|                             |       | (AC-FT)  | 0.    | 0.    | 0.       |
| CUMULATIVE AREA = .01 SQ MI |       |          |       |       |          |

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HYDROGRAPH AT STATION SUB7  
FOR PLAN 1, RATIO = 5.60

TOTAL RAINFALL = 5.60, TOTAL LOSS = 4.62, TOTAL EXCESS = .98

| PEAK FLOW                   | TIME  | 6-HR     | 24-HR | 72-HR | 29.90-HR |
|-----------------------------|-------|----------|-------|-------|----------|
| (CFS)                       | (HR)  |          |       |       |          |
| +                           | 4.    | 1.       | 0.    | 0.    | 0.       |
|                             | 12.40 | .797     | .983  | .983  | .983     |
|                             |       | (INCHES) |       |       |          |
|                             |       | (AC-FT)  | 0.    | 0.    | 0.       |
| CUMULATIVE AREA = .01 SQ MI |       |          |       |       |          |



180 LS SCS LOSS RATE  
 STRTL 1.00 INITIAL ABSTRACTION  
 CRVNR 51.00 CURVE NUMBER  
 RTIMP .00 PERCENT IMPERVIOUS AREA

181 UD SCS DIMENSIONLESS UNITGRAPH  
 TLAG .11 LAG

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UNIT HYDROGRAPH  
 8 END-OF-PERIOD ORDINATES

1. 1. 0. 0. 0. 0. 0. 0.

TOTAL RAINFALL = 1.00, TOTAL LOSS = 1.00, TOTAL EXCESS = .00

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | 72-HR<br>(CFS) | 29.90-HR<br>(INCHES)<br>(AC-FT) |
|--------------------|--------------|---------------|------------------------------|----------------|---------------------------------|
| +                  | 0.           | 0.            | .000                         | 0.             | 0.                              |
| +                  | .10          | 0.            | .000                         | 0.             | .000                            |
|                    |              | 0.            | 0.                           | 0.             | 0.                              |

CUMULATIVE AREA = .00 SQ MI

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HYDROGRAPH AT STATION SUB10  
 FOR PLAN 1, RATIO = 3.20

TOTAL RAINFALL = 3.20, TOTAL LOSS = 2.79, TOTAL EXCESS = .41

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | 72-HR<br>(CFS) | 29.90-HR<br>(INCHES)<br>(AC-FT) |
|--------------------|--------------|---------------|------------------------------|----------------|---------------------------------|
| +                  | 0.           | 0.            | .410                         | 0.             | .410                            |
| +                  | 12.30        | .331          | .410                         | .410           | .410                            |
|                    |              | 0.            | 0.                           | 0.             | 0.                              |

CUMULATIVE AREA = .00 SQ MI

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HYDROGRAPH AT STATION SUB10  
 FOR PLAN 1, RATIO = 4.20

TOTAL RAINFALL = 4.20, TOTAL LOSS = 3.40, TOTAL EXCESS = .80

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | 72-HR<br>(CFS) | 29.90-HR<br>(INCHES)<br>(AC-FT) |
|--------------------|--------------|---------------|------------------------------|----------------|---------------------------------|
| +                  | 0.           | 0.            | .800                         | 0.             | .800                            |
| +                  | 12.30        | .654          | .800                         | .800           | .800                            |
|                    |              | 0.            | 0.                           | 0.             | 0.                              |

CUMULATIVE AREA = .00 SQ MI

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HYDROGRAPH AT STATION SUB10  
 FOR PLAN 1, RATIO = 5.00

TOTAL RAINFALL = 5.00, TOTAL LOSS = 3.82, TOTAL EXCESS = 1.18

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | MAXIMUM AVERAGE FLOW<br>72-HR<br>(INCHES)<br>(AC-FT) | 29.90-HR<br>(INCHES)<br>(AC-FT) |
|--------------------|--------------|---------------|------------------------------|------------------------------------------------------|---------------------------------|
| 0.                 | 12.30        | 0.            | 0.                           | 0.                                                   | 0.                              |
|                    |              | .963          | 1.176                        | 1.176                                                | 1.176                           |
|                    |              | 0.            | 0.                           | 0.                                                   | 0.                              |

CUMULATIVE AREA = .00 SQ MI

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HYDROGRAPH AT STATION SUB10  
FOR PLAN 1, RATIO = 5.60

TOTAL RAINFALL = 5.60, TOTAL LOSS = 4.11, TOTAL EXCESS = 1.49

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | MAXIMUM AVERAGE FLOW<br>72-HR<br>(INCHES)<br>(AC-FT) | 29.90-HR<br>(INCHES)<br>(AC-FT) |
|--------------------|--------------|---------------|------------------------------|------------------------------------------------------|---------------------------------|
| 0.                 | 12.30        | 0.            | 0.                           | 0.                                                   | 0.                              |
|                    |              | 1.219         | 1.489                        | 1.489                                                | 1.489                           |
|                    |              | 0.            | 0.                           | 0.                                                   | 0.                              |

CUMULATIVE AREA = .00 SQ MI

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HYDROGRAPH AT STATION SUB10  
FOR PLAN 1, RATIO = 7.20

TOTAL RAINFALL = 7.20, TOTAL LOSS = 4.77, TOTAL EXCESS = 2.43

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | MAXIMUM AVERAGE FLOW<br>72-HR<br>(INCHES)<br>(AC-FT) | 29.90-HR<br>(INCHES)<br>(AC-FT) |
|--------------------|--------------|---------------|------------------------------|------------------------------------------------------|---------------------------------|
| 0.                 | 12.30        | 0.            | 0.                           | 0.                                                   | 0.                              |
|                    |              | 1.985         | 2.432                        | 2.432                                                | 2.432                           |
|                    |              | 0.            | 0.                           | 0.                                                   | 0.                              |

CUMULATIVE AREA = .00 SQ MI

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182 KK \*  
\* COMB A \*  
\* \* \* \* \*  
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COMBINED RUNOFF DRAINING TO POINT OF INTEREST 'A'

184 HC HYDROGRAPH COMBINATION 4 NUMBER OF HYDROGRAPHS TO COMBINE  
ICOMP

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 UNIT HYDROGRAPH  
 5 END-OF-PERIOD ORDINATES

1. 0 0. 0. .69, TOTAL EXCESS = .31

TOTAL RAINFALL = 1.00, TOTAL LOSS = .69, TOTAL EXCESS = .31

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(CFS) | 72-HR<br>(CFS) | 29.90-HR<br>(CFS) |
|--------------------|--------------|---------------|----------------|----------------|-------------------|
| 0.                 | 12.20        | 0.            | 0.             | 0.             | 0.                |
|                    |              | .219          | .310           | .310           | .310              |
|                    |              | (AC-FT)       | (AC-FT)        | (AC-FT)        | (AC-FT)           |
|                    |              | 0.            | 0.             | 0.             | 0.                |

CUMULATIVE AREA = .00 SQ MI

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HYDROGRAPH AT STATION SUB3  
 FOR PLAN 1, RATIO = 3.20

TOTAL RAINFALL = 3.20, TOTAL LOSS = 1.94, TOTAL EXCESS = 1.26

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(CFS) | 72-HR<br>(CFS) | 29.90-HR<br>(CFS) |
|--------------------|--------------|---------------|----------------|----------------|-------------------|
| 0.                 | 12.20        | 0.            | 0.             | 0.             | 0.                |
|                    |              | .886          | 1.257          | 1.257          | 1.257             |
|                    |              | (AC-FT)       | (AC-FT)        | (AC-FT)        | (AC-FT)           |
|                    |              | 0.            | 0.             | 0.             | 0.                |

CUMULATIVE AREA = .00 SQ MI

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HYDROGRAPH AT STATION SUB3  
 FOR PLAN 1, RATIO = 4.20

TOTAL RAINFALL = 4.20, TOTAL LOSS = 2.38, TOTAL EXCESS = 1.82

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(CFS) | 72-HR<br>(CFS) | 29.90-HR<br>(CFS) |
|--------------------|--------------|---------------|----------------|----------------|-------------------|
| 0.                 | 12.20        | 0.            | 0.             | 0.             | 0.                |
|                    |              | 1.305         | 1.821          | 1.821          | 1.821             |
|                    |              | (AC-FT)       | (AC-FT)        | (AC-FT)        | (AC-FT)           |
|                    |              | 0.            | 0.             | 0.             | 0.                |

CUMULATIVE AREA = .00 SQ MI

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HYDROGRAPH AT STATION SUB3  
 FOR PLAN 1, RATIO = 5.00

TOTAL RAINFALL = 5.00, TOTAL LOSS = 2.68, TOTAL EXCESS = 2.32

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(CFS) | 72-HR<br>(CFS) | 29.90-HR<br>(CFS) |
|--------------------|--------------|---------------|----------------|----------------|-------------------|
| 0.                 | 12.20        | 0.            | 0.             | 0.             | 0.                |
|                    |              | 1.305         | 1.821          | 1.821          | 1.821             |
|                    |              | (AC-FT)       | (AC-FT)        | (AC-FT)        | (AC-FT)           |
|                    |              | 0.            | 0.             | 0.             | 0.                |

CUMULATIVE AREA = .00 SQ MI

+ 0. 12.20 (INCHES) 1.679 0. 2.316 2.316 2.316 0.  
 (AC-FT) 0. 0. 0. 0. 0. 0.  
 CUMULATIVE AREA = .00 SQ MI

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HYDROGRAPH AT STATION SUB3  
 FOR PLAN 1, RATIO = 5.60

TOTAL RAINFALL = 5.60, TOTAL LOSS = 2.89, TOTAL EXCESS = 2.71

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>MAXIMUM AVERAGE FLOW | 24-HR<br>72-HR | 29.90-HR |
|--------------------|--------------|------------------------------|----------------|----------|
| + 0.               | 12.20        | 0.                           | 0.             | 0.       |
|                    |              | 1.977                        | 2.708          | 2.709    |
|                    |              | (INCHES)                     | (AC-FT)        |          |
|                    |              | 0.                           | 0.             | 0.       |
|                    |              | CUMULATIVE AREA =            | .00 SQ MI      |          |

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HYDROGRAPH AT STATION SUB3  
 FOR PLAN 1, RATIO = 7.20

TOTAL RAINFALL = 7.20, TOTAL LOSS = 3.37, TOTAL EXCESS = 3.83

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6 HR<br>MAXIMUM AVERAGE FLOW | 24-HR<br>72-HR | 29.90-HR |
|--------------------|--------------|------------------------------|----------------|----------|
| + 0.               | 12.20        | 0.                           | 0.             | 0.       |
|                    |              | 2.831                        | 3.828          | 3.829    |
|                    |              | (INCHES)                     | (AC-FT)        |          |
|                    |              | 0.                           | 0.             | 0.       |
|                    |              | CUMULATIVE AREA =            | .00 SQ MI      |          |

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190 KK \* SUB6 \*  
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192 BA SUBBASIN RUNOFF DATA  
 SUBBASIN CHARACTERISTICS  
 TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

| 139 PB | STORM                             | 1.00 | BASIN TOTAL PRECIPITATION |
|--------|-----------------------------------|------|---------------------------|
| 141 PI | INCREMENTAL PRECIPITATION PATTERN | .00  | .00                       |
|        | .00                               | .00  | .00                       |
|        | .00                               | .00  | .00                       |
|        | .00                               | .00  | .00                       |
|        | .00                               | .00  | .00                       |



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 HYDROGRAPH AT STATION SUB6  
 FOR PLAN 1, RATIO = 4.20  
 TOTAL RAINFALL = 4.20, TOTAL LOSS = 3.70, TOTAL EXCESS = .50

| PEAK FLOW TIME    | 6-HR      | 24-HR | 72-HR | 29.90-HR |
|-------------------|-----------|-------|-------|----------|
| (CFS)             | 0.        | 0.    | 0.    | 0.       |
| (INCHES)          | .408      | .504  | .504  | .504     |
| (AC-FT)           | 0.        | 0.    | 0.    | 0.       |
| CUMULATIVE AREA = | .00 SQ MI |       |       |          |

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 HYDROGRAPH AT STATION SUB6  
 FOR PLAN 1, RATIO = 5.00  
 TOTAL RAINFALL = 5.00, TOTAL LOSS = 4.24, TOTAL EXCESS = .76

| PEAK FLOW TIME    | 6-HR      | 24-HR | 72-HR | 29.90-HR |
|-------------------|-----------|-------|-------|----------|
| (CFS)             | 0.        | 0.    | 0.    | 0.       |
| (INCHES)          | .614      | .757  | .757  | .757     |
| (AC-FT)           | 0.        | 0.    | 0.    | 0.       |
| CUMULATIVE AREA = | .00 SQ MI |       |       |          |

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 HYDROGRAPH AT STATION SUB6  
 FOR PLAN 1, RATIO = 5.60  
 TOTAL RAINFALL = 5.60, TOTAL LOSS = 4.63, TOTAL EXCESS = .97

| PEAK FLOW TIME    | 6-HR      | 24-HR | 72-HR | 29.90-HR |
|-------------------|-----------|-------|-------|----------|
| (CFS)             | 0.        | 0.    | 0.    | 0.       |
| (INCHES)          | .789      | .973  | .973  | .973     |
| (AC-FT)           | 0.        | 0.    | 0.    | 0.       |
| CUMULATIVE AREA = | .00 SQ MI |       |       |          |

\*\*\*  
 HYDROGRAPH AT STATION SUB6  
 FOR PLAN 1, RATIO = 7.20  
 TOTAL RAINFALL = 7.20, TOTAL LOSS = 5.55, TOTAL EXCESS = 1.65

| PEAK FLOW TIME    | 6-HR      | 24-HR | 72-HR | 29.90-HR |
|-------------------|-----------|-------|-------|----------|
| (CFS)             | 0.        | 0.    | 0.    | 0.       |
| (INCHES)          | .973      | 1.165 | 1.165 | 1.165    |
| (AC-FT)           | 0.        | 0.    | 0.    | 0.       |
| CUMULATIVE AREA = | .00 SQ MI |       |       |          |



TOTAL RAINFALL = 1.00, TOTAL LOSS = 1.00, TOTAL EXCESS = .00

| PEAK FLOW                   | TIME | 6-HR     | 24-HR | 72-HR | 29.90-HR |
|-----------------------------|------|----------|-------|-------|----------|
| (CFS)                       | (HR) |          |       |       |          |
| +                           | 0.10 | 0.       | 0.    | 0.    | 0.       |
|                             |      | (INCHES) | .000  | .000  | .000     |
|                             |      | (AC-FT)  | 0.    | 0.    | 0.       |
| CUMULATIVE AREA = .00 SQ MI |      |          |       |       |          |

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HYDROGRAPH AT STATION SUB9  
FOR PLAN 1, RATIO = 3.20

TOTAL RAINFALL = 3.20, TOTAL LOSS = 2.73, TOTAL EXCESS = .47

| PEAK FLOW                   | TIME    | 6-HR     | 24-HR | 72-HR | 29.90-HR |
|-----------------------------|---------|----------|-------|-------|----------|
| (CFS)                       | (HR)    |          |       |       |          |
| +                           | 0.12.20 | 0.       | 0.    | 0.    | 0.       |
|                             |         | (INCHES) | .378  | .466  | .466     |
|                             |         | (AC-FT)  | 0.    | 0.    | 0.       |
| CUMULATIVE AREA = .00 SQ MI |         |          |       |       |          |

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HYDROGRAPH AT STATION SUB9  
FOR PLAN 1, RATIO = 4.20

TOTAL RAINFALL = 4.20, TOTAL LOSS = 3.30, TOTAL EXCESS = .90

| PEAK FLOW                   | TIME    | 6-HR     | 24-HR | 72-HR | 29.90-HR |
|-----------------------------|---------|----------|-------|-------|----------|
| (CFS)                       | (HR)    |          |       |       |          |
| +                           | 0.12.20 | 0.       | 0.    | 0.    | 0.       |
|                             |         | (INCHES) | .738  | .900  | .900     |
|                             |         | (AC-FT)  | 0.    | 0.    | 0.       |
| CUMULATIVE AREA = .00 SQ MI |         |          |       |       |          |

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HYDROGRAPH AT STATION SUB9  
FOR PLAN 1, RATIO = 5.00

TOTAL RAINFALL = 5.00, TOTAL LOSS = 3.69, TOTAL EXCESS = 1.31

| PEAK FLOW                   | TIME    | 6-HR     | 24-HR | 72-HR | 29.90-HR |
|-----------------------------|---------|----------|-------|-------|----------|
| (CFS)                       | (HR)    |          |       |       |          |
| +                           | 0.12.20 | 0.       | 0.    | 0.    | 0.       |
|                             |         | (INCHES) | 1.079 | 1.313 | 1.313    |
|                             |         | (AC-FT)  | 0.    | 0.    | 0.       |
| CUMULATIVE AREA = .00 SQ MI |         |          |       |       |          |

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 HYDROGRAPH AT STATION SUB9  
 FOR PLAN 1, RATIO = 5.60  
 TOTAL RAINFALL = 5.60, TOTAL LOSS = 3.94, TOTAL EXCESS = 1.66  
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
 (CFS) (HR) 6-HR 24-HR 72-HR 29.90-HR  
 + 0. 12.20 0. 0. 0. 0.  
 (INCHES) 1.360 1.655 1.655 1.655  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = .00 SQ MI

\*\*\*  
 HYDROGRAPH AT STATION SUB9  
 FOR PLAN 1, RATIO = 7.20  
 TOTAL RAINFALL = 7.20, TOTAL LOSS = 4.53, TOTAL EXCESS = 2.67  
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
 (CFS) (HR) 6-HR 24-HR 72-HR 29.90-HR  
 + 0. 12.20 0. 0. 0. 0.  
 (INCHES) 2.189 2.673 2.673 2.673  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = .00 SQ MI

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 200 KK \* COMB B \*  
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COMBINED RUNOFF DRAINING TO POINT OF INTEREST 'B'  
 202 HC HYDROGRAPH COMBINATION 3 NUMBER OF HYDROGRAPHS TO COMBINE  
 ICOMP \*\*\*\*\*  
 \*\*\*  
 HYDROGRAPH AT STATION COMB B  
 FOR PLAN 1, RATIO = 3.20  
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
 (CFS) (HR) 6-HR 24-HR 72-HR 29.90-HR  
 + 0. 12.40 0. 0. 0. 0.  
 (INCHES) .233 .305 .306 .306  
 (AC-FT) 0. 0. 0. 0.

CUMULATIVE AREA = .00 SQ MI

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HYDROGRAPH AT STATION COMB B  
FOR PLAN 1, RATIO = 4.20

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | 72-HR<br>(INCHES)<br>(AC-FT) | 29.90-HR<br>(INCHES)<br>(AC-FT) |
|--------------------|--------------|---------------|------------------------------|------------------------------|---------------------------------|
| +                  | 1.           | 0.            | .455                         | .577                         | .578                            |
|                    |              | 0.            | 0.                           | 0.                           | 0.                              |

CUMULATIVE AREA = .00 SQ MI

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HYDROGRAPH AT STATION COMB B  
FOR PLAN 1, RATIO = 5.00

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | 72-HR<br>(INCHES)<br>(AC-FT) | 29.90-HR<br>(INCHES)<br>(AC-FT) |
|--------------------|--------------|---------------|------------------------------|------------------------------|---------------------------------|
| +                  | 1.           | 0.            | .672                         | .846                         | .846                            |
|                    |              | 0.            | 0.                           | 0.                           | 0.                              |

CUMULATIVE AREA = .00 SQ MI

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HYDROGRAPH AT STATION COMB B  
FOR PLAN 1, RATIO = 5.60

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | 72-HR<br>(INCHES)<br>(AC-FT) | 29.90-HR<br>(INCHES)<br>(AC-FT) |
|--------------------|--------------|---------------|------------------------------|------------------------------|---------------------------------|
| +                  | 1.           | 0.            | .855                         | 1.073                        | 1.074                           |
|                    |              | 0.            | 0.                           | 0.                           | 0.                              |

CUMULATIVE AREA = .00 SQ MI

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HYDROGRAPH AT STATION COMB B  
FOR PLAN 1, RATIO = 7.20

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | 72-HR<br>(INCHES)<br>(AC-FT) | 29.90-HR<br>(INCHES)<br>(AC-FT) |
|--------------------|--------------|---------------|------------------------------|------------------------------|---------------------------------|
| +                  | 2.           | 0.            | 1.419                        | 1.775                        | 1.776                           |
|                    |              | 0.            | 0.                           | 0.                           | 0.                              |

CUMULATIVE AREA = .00 SQ MI



+ 0. 12.20 0. 0. 0. 0. 0.  
 (INCHES) .339 .480 .480 .480  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = .00 SQ MI

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 HYDROGRAPH AT STATION SUB2  
 FOR PLAN 1, RATIO = 3.20  
 TOTAL RAINFALL = 3.20, TOTAL LOSS = 1.46, TOTAL EXCESS = 1.74

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>MAXIMUM AVERAGE FLOW | 24-HR<br>MAXIMUM AVERAGE FLOW | 72-HR<br>MAXIMUM AVERAGE FLOW | 29.90-HR<br>MAXIMUM AVERAGE FLOW |
|--------------------|--------------|------------------------------|-------------------------------|-------------------------------|----------------------------------|
| 0.                 | 12.20        | 0.                           | 0.                            | 0.                            | 0.                               |
| 1.222              |              | 1.739                        | 1.739                         | 1.739                         | 1.739                            |

CUMULATIVE AREA = .00 SQ MI

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 HYDROGRAPH AT STATION SUB2  
 FOR PLAN 1, RATIO = 4.20  
 TOTAL RAINFALL = 4.20, TOTAL LOSS = 1.79, TOTAL EXCESS = 2.41

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>MAXIMUM AVERAGE FLOW | 24-HR<br>MAXIMUM AVERAGE FLOW | 72-HR<br>MAXIMUM AVERAGE FLOW | 29.90-HR<br>MAXIMUM AVERAGE FLOW |
|--------------------|--------------|------------------------------|-------------------------------|-------------------------------|----------------------------------|
| 0.                 | 12.20        | 0.                           | 0.                            | 0.                            | 0.                               |
| 1.711              |              | 2.413                        | 2.413                         | 2.413                         | 2.413                            |

CUMULATIVE AREA = .00 SQ MI

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 HYDROGRAPH AT STATION SUB2  
 FOR PLAN 1, RATIO = 5.00  
 TOTAL RAINFALL = 5.00, TOTAL LOSS = 2.01, TOTAL EXCESS = 2.99

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>MAXIMUM AVERAGE FLOW | 24-HR<br>MAXIMUM AVERAGE FLOW | 72-HR<br>MAXIMUM AVERAGE FLOW | 29.90-HR<br>MAXIMUM AVERAGE FLOW |
|--------------------|--------------|------------------------------|-------------------------------|-------------------------------|----------------------------------|
| 0.                 | 12.20        | 0.                           | 0.                            | 0.                            | 0.                               |
| 2.131              |              | 2.985                        | 2.985                         | 2.985                         | 2.985                            |

CUMULATIVE AREA = .00 SQ MI

\*\*\*  
 HYDROGRAPH AT STATION SUB2  
 FOR PLAN 1, RATIO = 5.60  
 TOTAL RAINFALL = 5.60, TOTAL LOSS = 2.17, TOTAL EXCESS = 3.43



211 LS SCS LOSS RATE  
 STRTL 1.00 INITIAL ABSTRACTION  
 CRVNR 36.60 CURVE NUMBER  
 RTIMP .00 PERCENT IMPERVIOUS AREA  
 TLAG .21 LAG

SCS DIMENSIONLESS UNITGRAPH  
 TLAG .21 LAG

UNIT HYDROGRAPH  
 13 END-OF-PERIOD ORDINATES

|    |    |     |    |    |    |    |    |    |
|----|----|-----|----|----|----|----|----|----|
| 3. | 9. | 10. | 7. | 3. | 2. | 1. | 1. | 0. |
| 0. | 0. | 0.  | 0. | 0. | 0. | 0. | 0. | 0. |

TOTAL RAINFALL = 1.00, TOTAL LOSS = 1.00, TOTAL EXCESS = .00

PEAK FLOW TIME  
 (CFS) (HR)

|   |    |     |          |      |      |      |      |      |
|---|----|-----|----------|------|------|------|------|------|
| + | 0. | .10 | 0.       | 0.   | 0.   | 0.   | 0.   | 0.   |
|   |    |     | (INCHES) | .000 | .000 | .000 | .000 | .000 |
|   |    |     | (AC-FT)  | 0.   | 0.   | 0.   | 0.   | 0.   |

CUMULATIVE AREA = .01 SQ MI

HYDROGRAPH AT STATION SUB5  
 FOR PLAN 1, RATIO = 3.20

TOTAL RAINFALL = 3.20, TOTAL LOSS = 2.95, TOTAL EXCESS = .25

PEAK FLOW TIME  
 (CFS) (HR)

|   |    |       |          |      |      |      |      |      |
|---|----|-------|----------|------|------|------|------|------|
| + | 1. | 12.40 | 0.       | 0.   | 0.   | 0.   | 0.   | 0.   |
|   |    |       | (INCHES) | .198 | .248 | .248 | .248 | .248 |
|   |    |       | (AC-FT)  | 0.   | 0.   | 0.   | 0.   | 0.   |

CUMULATIVE AREA = .01 SQ MI

HYDROGRAPH AT STATION SUB5  
 FOR PLAN 1, RATIO = 4.20

TOTAL RAINFALL = 4.20, TOTAL LOSS = 3.70, TOTAL EXCESS = .50

PEAK FLOW TIME  
 (CFS) (HR)

|   |      |                      |       |       |          |
|---|------|----------------------|-------|-------|----------|
| + | 6-HR | MAXIMUM AVERAGE FLOW | 24-HR | 72-HR | 29.90-HR |
|---|------|----------------------|-------|-------|----------|

+ 1. 12.40 (INCHES) 0. .404 0. .499 0. .499 0.  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = .01 SQ MI

\*\*\* HYDROGRAPH AT STATION SUB5  
 FOR PLAN 1, RATIO = 5.00

TOTAL RAINFALL = 5.00, TOTAL LOSS = 4.25, TOTAL EXCESS = .75

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | 72-HR<br>MAXIMUM AVERAGE FLOW<br>(INCHES)<br>(AC-FT) | 29.90-HR<br>MAXIMUM AVERAGE FLOW<br>(INCHES)<br>(AC-FT) |
|--------------------|--------------|---------------|------------------------------|------------------------------------------------------|---------------------------------------------------------|
| + 2                | 12.40        | 0.            | .608                         | .750                                                 | .750                                                    |
|                    |              | 0.            | 0.                           | 0.                                                   | 0.                                                      |

CUMULATIVE AREA = .01 SQ MI

\*\*\* HYDROGRAPH AT STATION SUB5  
 FOR PLAN 1, RATIO = 5.60

TOTAL RAINFALL = 5.60, TOTAL LOSS = 4.63, TOTAL EXCESS = .97

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | 72-HR<br>MAXIMUM AVERAGE FLOW<br>(INCHES)<br>(AC-FT) | 29.90-HR<br>MAXIMUM AVERAGE FLOW<br>(INCHES)<br>(AC-FT) |
|--------------------|--------------|---------------|------------------------------|------------------------------------------------------|---------------------------------------------------------|
| + 2                | 12.40        | 0.            | .782                         | .965                                                 | .965                                                    |
|                    |              | 0.            | 0.                           | 0.                                                   | 0.                                                      |

CUMULATIVE AREA = .01 SQ MI

\*\*\* HYDROGRAPH AT STATION SUB5  
 FOR PLAN 1, RATIO = 7.20

TOTAL RAINFALL = 7.20, TOTAL LOSS = 5.57, TOTAL EXCESS = 1.63

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | 72-HR<br>MAXIMUM AVERAGE FLOW<br>(INCHES)<br>(AC-FT) | 29.90-HR<br>MAXIMUM AVERAGE FLOW<br>(INCHES)<br>(AC-FT) |
|--------------------|--------------|---------------|------------------------------|------------------------------------------------------|---------------------------------------------------------|
| + 4                | 12.40        | 1.            | 1.322                        | 1.634                                                | 1.634                                                   |
|                    |              | 0.            | 0.                           | 0.                                                   | 0.                                                      |

CUMULATIVE AREA = .01 SQ MI

\*\*\*\*\*

213 KK \* COMB C \* \*\*\*\*\*  
 \* \* \* \* \*  
 \*\*\*\*\*

COMBINED RUNOFF DRAINING TO POINT OF INTEREST 'C'

215 HC HYDROGRAPH COMBINATION 2 NUMBER OF HYDROGRAPHS TO COMBINE  
 ICOMP \*\*\*\*\*

\*\*\*  
 \*\*\*  
 HYDROGRAPH AT STATION COMB C  
 FOR PLAN 1, RATIO = 3.20  
 \*\*\*  
 PEAK FLOW TIME  
 (HR) 6-HR 24-HR 72-HR 29.90-HR  
 + (CFS) 0 0 0 0  
 + 1. 12.40 (INCHES) .254 .342 .342 .342  
 (AC-FT) 0 0 0 0  
 CUMULATIVE AREA = .01 SQ MI

\*\*\*  
 \*\*\*  
 HYDROGRAPH AT STATION COMB C  
 FOR PLAN 1, RATIO = 4.20  
 \*\*\*  
 PEAK FLOW TIME  
 (HR) 6-HR 24-HR 72-HR 29.90-HR  
 + (CFS) 0 0 0 0  
 + 1. 12.40 (INCHES) .477 .619 .620 .620  
 (AC-FT) 0 0 0 0  
 CUMULATIVE AREA = .01 SQ MI

\*\*\*  
 \*\*\*  
 HYDROGRAPH AT STATION COMB C  
 FOR PLAN 1, RATIO = 5.00  
 \*\*\*  
 PEAK FLOW TIME  
 (HR) 6-HR 24-HR 72-HR 29.90-HR  
 + (CFS) 0 0 0 0  
 + 2. 12.40 (INCHES) .696 .891 .892 .892  
 (AC-FT) 0 0 0 0  
 CUMULATIVE AREA = .01 SQ MI

\*\*\*  
 \*\*\*  
 HYDROGRAPH AT STATION COMB C  
 FOR PLAN 1, RATIO = 5.60  
 \*\*\*  
 PEAK FLOW TIME  
 (HR) 6-HR 24-HR 72-HR 29.90-HR  
 + (CFS) 0 0 0 0



219 LS SCS LOSS RATE 1.00 INITIAL ABSTRACTION  
 STPFL 36.00 CURVE NUMBER  
 CRVNR .00 PERCENT IMPERVIOUS AREA  
 RTIMP .00 PERCENT IMPERVIOUS AREA

220 UD SCS DIMENSIONLESS UNITGRAPH  
 TLAG .08 LAG

UNIT HYDROGRAPH  
 6 END-OF-PERIOD ORDINATES

TOTAL RAINFALL = 1.00, TOTAL LOSS = 1.00, TOTAL EXCESS = .00

| PEAK FLOW TIME | 6-HR | 24-HR | 72-HR | 29.90-HR |
|----------------|------|-------|-------|----------|
| (CFS)          | 0.   | 0.    | 0.    | 0.       |
| (INCHES)       | .000 | .000  | .000  | .000     |
| (AC-FT)        | 0.   | 0.    | 0.    | 0.       |

CUMULATIVE AREA = .00 SQ MI

HYDROGRAPH AT STATION SUB8  
 FOR PLAN 1, RATIO = 3.20

TOTAL RAINFALL = 3.20, TOTAL LOSS = 2.96, TOTAL EXCESS = .24

| PEAK FLOW TIME | 6-HR | 24-HR | 72-HR | 29.90-HR |
|----------------|------|-------|-------|----------|
| (CFS)          | 0.   | 0.    | 0.    | 0.       |
| (INCHES)       | .194 | .242  | .242  | .242     |
| (AC-FT)        | 0.   | 0.    | 0.    | 0.       |

CUMULATIVE AREA = .00 SQ MI

HYDROGRAPH AT STATION SUB8  
 FOR PLAN 1, RATIO = 4.20

TOTAL RAINFALL = 4.20, TOTAL LOSS = 3.71, TOTAL EXCESS = .49

| PEAK FLOW TIME | 6-HR | 24-HR | 72-HR | 29.90-HR |
|----------------|------|-------|-------|----------|
| (CFS)          | 0.   | 0.    | 0.    | 0.       |
| (INCHES)       | .396 | .488  | .488  | .488     |
| (AC-FT)        | 0.   | 0.    | 0.    | 0.       |

CUMULATIVE AREA = .00 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SUB8  
FOR PLAN 1, RATIO = 5.00

TOTAL RAINFALL = 5.00, TOTAL LOSS = 4.27, TOTAL EXCESS = .73

| PEAK FLOW<br>(CFS)          | TIME<br>(HR) | 6-HR<br>MAXIMUM AVERAGE FLOW | 24-HR<br>MAXIMUM AVERAGE FLOW | 72-HR<br>MAXIMUM AVERAGE FLOW | 29.90-HR<br>MAXIMUM AVERAGE FLOW |
|-----------------------------|--------------|------------------------------|-------------------------------|-------------------------------|----------------------------------|
| 0.                          | 12.20        | 0.                           | 0.                            | 0.                            | 0.                               |
|                             |              | .596                         | .735                          | .735                          | .735                             |
|                             |              | (AC-FT)                      | (AC-FT)                       | (AC-FT)                       | (AC-FT)                          |
| CUMULATIVE AREA = .00 SQ MI |              |                              |                               |                               |                                  |

\*\*\* \*\*

HYDROGRAPH AT STATION SUB8  
FOR PLAN 1, RATIO = 5.60

TOTAL RAINFALL = 5.60, TOTAL LOSS = 4.65, TOTAL EXCESS = .95

| PEAK FLOW<br>(CFS)          | TIME<br>(HR) | 6-HR<br>MAXIMUM AVERAGE FLOW | 24-HR<br>MAXIMUM AVERAGE FLOW | 72-HR<br>MAXIMUM AVERAGE FLOW | 29.90-HR<br>MAXIMUM AVERAGE FLOW |
|-----------------------------|--------------|------------------------------|-------------------------------|-------------------------------|----------------------------------|
| 0.                          | 12.20        | 0.                           | 0.                            | 0.                            | 0.                               |
|                             |              | .767                         | .946                          | .946                          | .946                             |
|                             |              | (AC-FT)                      | (AC-FT)                       | (AC-FT)                       | (AC-FT)                          |
| CUMULATIVE AREA = .00 SQ MI |              |                              |                               |                               |                                  |

\*\*\* \*\*

HYDROGRAPH AT STATION SUB8  
FOR PLAN 1, RATIO = 7.20

TOTAL RAINFALL = 7.20, TOTAL LOSS = 5.60, TOTAL EXCESS = 1.60

| PEAK FLOW<br>(CFS)          | TIME<br>(HR) | 6-HR<br>MAXIMUM AVERAGE FLOW | 24-HR<br>MAXIMUM AVERAGE FLOW | 72-HR<br>MAXIMUM AVERAGE FLOW | 29.90-HR<br>MAXIMUM AVERAGE FLOW |
|-----------------------------|--------------|------------------------------|-------------------------------|-------------------------------|----------------------------------|
| 0.                          | 12.20        | 0.                           | 0.                            | 0.                            | 0.                               |
|                             |              | 1.297                        | 1.603                         | 1.603                         | 1.603                            |
|                             |              | (AC-FT)                      | (AC-FT)                       | (AC-FT)                       | (AC-FT)                          |
| CUMULATIVE AREA = .00 SQ MI |              |                              |                               |                               |                                  |

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
TIME TO PEAK IN HOURS

| OPERATION | STATION | AREA | PLAN | RATIOS APPLIED TO PRECIPITATION |              |               |               |               |               |
|-----------|---------|------|------|---------------------------------|--------------|---------------|---------------|---------------|---------------|
|           |         |      |      | RATIO 1                         | RATIO 2      | RATIO 3       | RATIO 4       | RATIO 5       |               |
| +         | SUB1    | .02  | 1    | FLOW<br>TIME                    | 8.2<br>12.30 | 13.5<br>12.30 | 18.4<br>12.30 | 22.4<br>12.30 | 34.3<br>12.30 |
|           |         |      |      |                                 | 3.20         | 4.20          | 5.00          | 5.60          | 7.20          |

|   |               |        |     |   |      |       |       |       |       |       |
|---|---------------|--------|-----|---|------|-------|-------|-------|-------|-------|
| + | HYDROGRAPH AT | SUB4   | .00 | 1 | FLOW | .1    | .1    | .2    | .2    | .4    |
|   |               |        |     |   | TIME | 12.20 | 12.20 | 12.20 | 12.20 | 12.20 |
| + | HYDROGRAPH AT | SUB7   | .01 | 1 | FLOW | .9    | 2.0   | 3.1   | 4.1   | 7.1   |
|   |               |        |     |   | TIME | 12.40 | 12.40 | 12.40 | 12.40 | 12.40 |
| + | HYDROGRAPH AT | SUB10  | .00 | 1 | FLOW | .0    | .1    | .2    | .2    | .3    |
|   |               |        |     |   | TIME | 12.30 | 12.30 | 12.30 | 12.30 | 12.30 |
| + | 4 COMBINED AT | COMB A | .03 | 1 | FLOW | 9.0   | 15.5  | 21.5  | 26.6  | 41.6  |
|   |               |        |     |   | TIME | 12.30 | 12.30 | 12.30 | 12.30 | 12.30 |
| + | HYDROGRAPH AT | SUB3   | .00 | 1 | FLOW | .1    | .1    | .2    | .2    | .3    |
|   |               |        |     |   | TIME | 12.20 | 12.20 | 12.20 | 12.20 | 12.20 |
| + | HYDROGRAPH AT | SUB6   | .00 | 1 | FLOW | .2    | .5    | .8    | 1.0   | 1.8   |
|   |               |        |     |   | TIME | 12.40 | 12.40 | 12.40 | 12.40 | 12.40 |
| + | HYDROGRAPH AT | SUB9   | .00 | 1 | FLOW | .0    | .0    | .0    | .0    | .1    |
|   |               |        |     |   | TIME | 12.20 | 12.20 | 12.20 | 12.20 | 12.20 |
| + | 3 COMBINED AT | COMB B | .00 | 1 | FLOW | 3     | 6     | 9     | 1.2   | 2.0   |
|   |               |        |     |   | TIME | 12.40 | 12.40 | 12.40 | 12.40 | 12.40 |
| + | HYDROGRAPH AT | SUB2   | .00 | 1 | FLOW | .3    | .5    | .6    | .7    | 1.0   |
|   |               |        |     |   | TIME | 12.20 | 12.20 | 12.20 | 12.20 | 12.20 |
| + | HYDROGRAPH AT | SUB5   | .01 | 1 | FLOW | .5    | 1.2   | 1.8   | 2.4   | 4.2   |
|   |               |        |     |   | TIME | 12.40 | 12.40 | 12.40 | 12.40 | 12.40 |
| + | 2 COMBINED AT | COMB C | .01 | 1 | FLOW | .7    | 1.4   | 2.2   | 2.8   | 4.7   |
|   |               |        |     |   | TIME | 12.40 | 12.40 | 12.40 | 12.40 | 12.40 |
| + | HYDROGRAPH AT | SUB8   | .00 | 1 | FLOW | .0    | .1    | .1    | .1    | .2    |
|   |               |        |     |   | TIME | 12.30 | 12.30 | 12.20 | 12.20 | 12.20 |

\*\*\* NORMAL END OF HEC-1 \*\*\*

\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* MAY 1991 \*  
 \* VERSION 4.0.1U \*  
 \* Lahey F77L-EM/32 version 5.01 \*  
 \* Dodson & Associates, Inc. \*  
 \* RUN DATE 08/22/06 TIME 16:03:22 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* U.S. ARMY CORPS OF ENGINEERS \*  
 \* HYDROLOGIC ENGINEERING CENTER \*  
 \* 609 SECOND STREET \*  
 \* DAVIS, CALIFORNIA 95616 \*  
 \* (916) 551-1748 \*  
 \*\*\*\*\*

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**DEVELOPED CONDITIONS**

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.  
 THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
 THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION.  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS-WRITE STAGE FREQUENCY,  
 DSS-READ TIME SERIES AT DESIRED CALCULATION INTERVAL, LOSS RATE-GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10  
 HEC-1 INPUT  
 -----DEV.IH1-----

HYDROLOGY FOR: COURTYARD AT UPPER NYACK #03118  
 VILLAGE OF UPPER NYACK, ROCKLAND COUNTY, NEW YORK

ANALYSIS PREPARED BY: LEONARD JACKSON ASSOCIATES  
 August 21, 2006 -PD

ANALYSIS PARAMETERS:  
 DEVELOPED CONDITIONS RUN  
 STORM RECURRENCE INTERVALS = 2, 5, 10, 25 & 100 YEAR  
 HYDROGRAPH METHOD: SCS  
 RAINFALL DISTRIBUTION: SCS TYPE III  
 24 HOUR RAINFALL 2 YEAR: 3.2 INCHES  
 5 YEAR: 4.2 INCHES  
 10 YEAR: 5.0 INCHES  
 25 YEAR: 5.6 INCHES  
 100 YEAR: 7.3 INCHES

\*\* NOTE: SCS METHOD USED

\*DIAGRAM  
 IT 6 0 0 300  
 IO 3 0  
 JR PREC 3.2 4.2 5 5.6 7.3

KK SUB-2OFFSITE RUNOFF TO THE NORTHERLY PORTION OF SITE TOWARD POINT #C

```

27 KM ***** DRAINAGE AREA = 0.10 AC = 0.0002 SQ. MI. ***** Q=0.32 cfs
28 KM * TIME OF CONCENTRATION = 1.0 MIN = 0.02 HR * 0.6 = 0.01 (SCS LAG) *****
29 KM *****
30 KM *****
31 KM *****
32 KM *****
33 BA 0.0002
34 PB 1.0
35 IN 6
36 PC 0 0.001 0.002 0.003 0.004 0.005 0.006 0.007 0.008 0.009
37 PC 0.010 0.011 0.012 0.013 0.014 0.015 0.016 0.017 0.018 0.019
38 PC 0.020 0.021 0.022 0.023 0.024 0.026 0.027 0.028 0.029 0.030
39 PC 0.0305 0.031 0.032 0.034 0.035 0.036 0.037 0.038 0.040 0.041
40 PC 0.042 0.043 0.045 0.046 0.047 0.049 0.050 0.051 0.053 0.054
41 PC 0.055 0.057 0.058 0.060 0.061 0.063 0.064 0.066 0.067 0.069
42 PC 0.070 0.072 0.074 0.075 0.077 0.079 0.080 0.082 0.084 0.085
43 PC 0.087 0.089 0.091 0.093 0.095 0.097 0.100 0.103 0.106 0.109
44 PC 0.112 0.115 0.118 0.121 0.124 0.127 0.130 0.134 0.137 0.140
45 PC 0.144 0.148 0.151 0.155 0.159 0.163 0.167 0.171 0.176 0.180
46 PC 0.185 0.189 0.194 0.199 0.205 0.210 0.216 0.222 0.228 0.235
47 PC 0.242 0.250 0.258 0.266 0.276 0.287 0.298 0.312 0.328 0.363
48 PC 0.416 0.500 0.584 0.638 0.673 0.689 0.702 0.714 0.725 0.734
49 PC 0.743 0.751 0.758 0.766 0.772 0.779 0.785 0.790 0.796 0.801
50 PC 0.806 0.811 0.816 0.821 0.825 0.829 0.834 0.838 0.842 0.845
51 PC 0.849 0.853 0.857 0.860 0.864 0.867 0.870 0.874 0.877 0.880
52 PC 0.886 0.889 0.892 0.895 0.898 0.900 0.903 0.906 0.908 0.910
53 PC 0.911 0.913 0.915 0.917 0.919 0.920 0.922 0.924 0.925 0.927
    HEC-1 INPUT
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
PC 0.929 0.930 0.932 0.933 0.935 0.936 0.938 0.939 0.941 0.942
PC 0.944 0.945 0.946 0.948 0.949 0.951 0.952 0.953 0.955 0.956
PC 0.957 0.958 0.960 0.961 0.962 0.963 0.965 0.966 0.967 0.968
PC 0.969 0.971 0.972 0.973 0.974 0.975 0.976 0.977 0.978 0.979
PC 0.981 0.982 0.983 0.984 0.985 0.986 0.987 0.988 0.989 0.990
PC 0.991 0.992 0.993 0.994 0.995 0.996 0.997 0.998 0.999 1.000
LS 1 25
LS 1 48
UD 0.01
KK SUB-SITE RUNOFF TO POINT # C
*****
62 KM ***** DRAINAGE AREA = 0.95 AC = 0.0015 SQ. MI. *****
63 KM * TIME OF CONCENTRATION = 21.4 MIN = 0.35 HR * 0.6 = 0.214 (SCS LAG) *****
64 KM *****
65 KM *****
66 KM *****
67 KM *****
68 KM *****
69 BA 0.0015
70 LS 1 52
71 UD 0.214
KK PT-COMBINE HYDROGRAPHS SUB-2 & SUB-6
HC 2
KK SUB-3SITE RUNOFF TO POINT # B
*****
74 KM ***** DRAINAGE AREA = 0.14 AC = 0.0002 SQ. MI. *****
75 KM * TIME OF CONCENTRATION = 0.7 MIN = 0.01 HR * 0.6 = 0.07 (SCS LAG) *****
76 KM *****
77 KM *****
78 KM *****
79 KM *****
80 KM *****
81 BA 0.0002
82 LS 1 75
83 UD 0.07
KK SUB-7SITE RUNOFF TO POINT # B
*****
84 KM *****
85 KM *****

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86 KM *****
87 KM * DRAINAGE AREA = 5.43 AC = 0.0085 SQ. MI. Q=11.83 cfs
88 KM * TIME OF CONCENTRATION =12.8 MIN = 0.21 HR * 0.6 = 0.128 (SCS LAG)
89 KM *****
90 KM
91 BA 0.0085
92 LS 1 60.05 24.49
93 UD 0.128
94 KK combcombine HYDROGRAPHS SUB-3 & SUB-7
95 HC 2
96 KK BASINROUTING IN BASIN PRIOR TO DISCHARGE TOWARD "PT-B"
97 KM
98 KM OUTLET STRUCTURE DATA:
99 KM *****
100 KM * TOP OF STRUCTURE OVERFLOW LENGTH: 13' LONG AT EL 435.0 *
101 KM * WEIR LENGTH = 2.0' WIDE AT EL 439.0 *
102 KM * ORIFICE #1: 3" DIAMETER AT EL.439.5 *
HEC-1 INPUT
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
KM *****
103 KM
104 KM
105 RS 1 ELEV 284 0
106 SA 0.075 0.1234 0.1693 0.1942
107 SE 284 286 288 289
108 SQ 0.07 0.17 0.2 0.27 1.51 5.43 5.73 6.3 9.73 15.29
109 SE 284.2 284.6 284.8 285.4 285.6 287.2 287.4 287.6 288 288.2
110 KK TO PTB*****
111 DT TO PTA
112 DI 0 1.3 1.86 2.27 4.72 6.24 7.45 8.49 9.41 10.25
113 DI 11.03 11.75 12.43 13.08 13.69
114 DQ 0 1.09 1.58 1.93 4.33 5.8 6.97 7.98 8.86 9.67
115 DQ 10.42 11.11 11.77 12.39 12.98
116 KK SUB-1-OFFSITE RUNOFF TO POINT #A
117 KM
118 KM *****
119 KM * DRAINAGE AREA = 7.75 AC = 0.0121 SQ. MI. Q=11.87 CFS
120 KM * TIME OF CONCENTRATION =14.8MIN = 0.24 HR * 0.6 = 0.148 (SCS LAG)
121 KM *****
122 KM
123 RA 0.0121
124 LS 1 54.7 8.35
125 UD 0.148
126 KK LAG-1LAG OFF-1 HYDROGRAPH TO POINT #A
127 RT 0 1
128 KK SUB-4OFFSITE RUNOFF TO POINT #A
129 KM
130 KM *****
131 KM * DRAINAGE AREA = 0.15 AC = 0.0002 SQ. MI. Q=0.48 CFS
132 KM * TIME OF CONCENTRATION =1.0MIN = 0.01 HR * 0.6 = 0.01 (SCS LAG)
133 KM *****
134 KM
135 RA 0.0002
136 LS 1 78 48
137 UD 0.01
138 KK SUB-8SITE RUNOFF TO POINT #A
139 KM
140 KM *****
141 KM * DRAINAGE AREA = 1.90 AC = 0.003 SQ. MI. Q=2.53 cfs

```

142 KM \* TIME OF CONCENTRATION =9.6 MIN = 0.16 HR \* 0.6 = 0.096 (SCS LAG) \*\*\*\*\*  
 143 KM \*\*\*\*\*  
 144 KM  
 145 BA 0.003  
 146 LS 1 52.8 0  
 147 UD 0.096  
 HEC-1 INPUT  
 ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

148 KK SUB-5SITE RUNOFF TO POINT #A  
 149 KM \*\*\*\*\*  
 150 KM \* DRAINAGE AREA = 0.12 AC = 0.0002 SQ. MI. Q=0.38 cfs  
 151 KM \* TIME OF CONCENTRATION =1.0 MIN = 0.016 HR \* 0.6 = 0.01 (SCS LAG) \*\*\*\*\*  
 152 KM \*\*\*\*\*  
 153 KM  
 154 KM  
 155 BA 0.0002  
 156 LS 1 52.8 48  
 157 UD 0.01  
 HEC-1 INPUT  
 ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

158 KK SUB-9SITE RUNOFF TO POINT #A  
 159 KM \*\*\*\*\*  
 160 KM \* DRAINAGE AREA = 2.90 AC = 0.0045 SQ. MI. Q=7.42 cfs  
 161 KM \* TIME OF CONCENTRATION =1.2 MIN = 0.05 HR \* 0.6 = 0.032 (SCS LAG) \*\*\*\*\*  
 162 KM \*\*\*\*\*  
 163 KM  
 164 KM  
 165 BA 0.0045  
 166 LS 1 53.9 33.45  
 167 UD 0.032  
 HEC-1 INPUT  
 ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

168 KK combCOMBINE HYDROGRAPHS SUB-5 & SUB-9  
 169 HC 2  
 HEC-1 INPUT  
 ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

170 KK BASINROUTING IN BASIN PRIOR TO DISCHARGE TOWARD 'PT-B'  
 171 KM  
 172 KM  
 173 KM  
 174 KM \* TOP OF STRUCTURE OVERFLOW LENGTH: 13' LONG AT EL.435.0 \*  
 175 KM \* WEIR LENGTH = 2.0' WIDE AT EL.439.0 \*  
 176 KM \* ORIFICE #1: 3" DIAMETER AT EL.439.5 \*  
 177 KM \*\*\*\*\*  
 178 KM  
 179 RS 1 ELEV 284 0  
 180 SA 0.058 0.1024 0.1469  
 181 SE 284 286 288  
 182 SQ 0.07 0.22 1.97 2.7 3.27 5.55 5.84 6.93 10.76  
 183 SE 284.2 285 285.2 285.4 285.6 286.8 287 287.2 287.4  
 HEC-1 INPUT  
 ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

184 KK combCOMBINE HYDROGRAPHS COMB-1, SITE-3 & OFF-3  
 185 KM  
 186 KM  
 187 KM \* DRAINAGE AREA = 0.19 AC = 0.0003 SQ. MI. Q=0.31 cfs  
 188 KM \* TIME OF CONCENTRATION =1.2 MIN = 0.18 HR \* 0.6 = 0.112 (SCS LAG) \*\*\*\*\*  
 189 KM \*\*\*\*\*  
 190 KM  
 191 KM  
 192 BA 0.0003  
 193 LS 1 60  
 UD 0.112  
 HEC-1 INPUT  
 ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10



```

194 . . . . . Comb. . . . .
198 . . . . . TO PTA
196 . . . . . RTRV
199 . . . . . PT-A. . . . .

```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.10 *
* Lahey F77L-EM/32 version 5.01 *
* Dodson & Associates, Inc. *
* RUN DATE 08/22/06 TIME 16:03:22 *
*****

```

```

*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 551-1748 *
*****

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-----DEV. IH1-----

HYDROLOGY FOR: COURTYARD AT UPPER NYACK #03118  
VILLAGE OF UPPER NYACK, ROCKLAND COUNTY, NEW YORK

ANALYSIS PREPARED BY: LEONARD JACKSON ASSOCIATES  
August 21, 2006 -PD

ANALYSIS PARAMETERS:  
DEVELOPED CONDITIONS RUN  
STORM RECURRENCE INTERVALS = 2, 5, 10, 25 & 100 YEAR  
HYDROGRAPH METHOD: SCS  
RAINFALL DISTRIBUTION: SCS TYPE III  
24 HOUR RAINFALL  
2 YEAR: 3.2 INCHES  
5 YEAR: 4.2 INCHES  
10 YEAR: 5.0 INCHES  
25 YEAR: 5.6 INCHES  
100 YEAR: 7.3 INCHES

\*\* NOTE: SCS METHOD USED

```

24 IO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
OSCAL 0. HYDROGRAPH PLOT SCALE

```

```

IT HYDROGRAPH TIME DATA
NMIN 6 MINUTES IN COMPUTATION INTERVAL
IDATE 1 0 STARTING DATE
ITIME 0000 STARTING TIME
NQ 300 NUMBER OF HYDROGRAPH ORDINATES
NDATE 2 0 ENDING DATE
NPTIME 0554 ENDING TIME
ICENT 19 CENTURY MARK

```

```

COMPUTATION INTERVAL 0.10 HOURS
TOTAL TIME BASE 29.90 HOURS

```

ENGLISH UNITS  
DRAINAGE AREA SQUARE MILES



0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00

60 LS

SCS LOSS RATE  
STRTL 1.00 INITIAL ABSTRACTION  
CRVNR 25.00 CURVE NUMBER  
RTIME 48.00 PERCENT IMPERVIOUS AREA  
SCS DIMENSIONLESS UNITGRAPH  
TLAG 0.01 LAG

61 UD

SCS DIMENSIONLESS UNITGRAPH  
TLAG 0.01 LAG

\*\*\*

UNIT HYDROGRAPH  
5 END-OF-PERIOD ORDINATES

1. 0. 0. 0. 0.

TOTAL RAINFALL = 1.00, TOTAL LOSS = 0.52, TOTAL EXCESS = 0.48

| PEAK FLOW | TIME     | 6-HR  | 24-HR | 72-HR | 29.90-HR |
|-----------|----------|-------|-------|-------|----------|
| +         | (CFS)    |       |       |       |          |
| +         | 0. 12.20 | 0.    | 0.    | 0.    | 0.       |
|           | (INCHES) | 0.339 | 0.480 | 0.480 | 0.480    |
|           | (AC-FT)  | 0.    | 0.    | 0.    | 0.       |

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

\*\*\*

\*\*\*

HYDROGRAPH AT STATION SUB-2  
FOR PLAN 1, RATIO = 3.20

TOTAL RAINFALL = 3.20, TOTAL LOSS = 1.59, TOTAL EXCESS = 1.61

| PEAK FLOW | TIME     | 6-HR  | 24-HR | 72-HR | 29.90-HR |
|-----------|----------|-------|-------|-------|----------|
| +         | (CFS)    |       |       |       |          |
| +         | 0. 12.20 | 0.    | 0.    | 0.    | 0.       |
|           | (INCHES) | 1.134 | 1.614 | 1.614 | 1.614    |
|           | (AC-FT)  | 0.    | 0.    | 0.    | 0.       |

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

\*\*\*

\*\*\*

HYDROGRAPH AT STATION SUB-2  
FOR PLAN 1, RATIO = 4.20

TOTAL RAINFALL = 4.20, TOTAL LOSS = 2.02, TOTAL EXCESS = 2.18

| PEAK FLOW | TIME     | 6-HR  | 24-HR | 72-HR | 29.90-HR |
|-----------|----------|-------|-------|-------|----------|
| +         | (CFS)    |       |       |       |          |
| +         | 0. 12.20 | 0.    | 0.    | 0.    | 0.       |
|           | (INCHES) | 1.531 | 2.176 | 2.176 | 2.176    |
|           | (AC-FT)  | 0.    | 0.    | 0.    | 0.       |

CUMULATIVE AREA = 0.00 SQ MI

\*\*\* HYDROGRAPH AT STATION SUB-2  
 FOR PLAN 1, RATIO = 5.00  
 TOTAL RAINFALL = 5.00, TOTAL LOSS = 2.36, TOTAL EXCESS = 2.64  
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
 (CFS) (HR) 6-HR 24-HR 72-HR 29.90-HR  
 + 0. 12.20 0. 0. 0. 0.  
 (INCHES) 1.864 2.644 2.645 2.645  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = 0.00 SQ MI

\*\*\* HYDROGRAPH AT STATION SUB-2  
 FOR PLAN 1, RATIO = 5.60  
 TOTAL RAINFALL = 5.60, TOTAL LOSS = 2.59, TOTAL EXCESS = 3.01  
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
 (CFS) (HR) 6-HR 24-HR 72-HR 29.90-HR  
 + 0. 12.20 0. 0. 0. 0.  
 (INCHES) 2.123 3.005 3.006 3.006  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = 0.00 SQ MI

\*\*\* HYDROGRAPH AT STATION SUB-2  
 FOR PLAN 1, RATIO = 7.30  
 TOTAL RAINFALL = 7.30, TOTAL LOSS = 3.23, TOTAL EXCESS = 4.07  
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
 (CFS) (HR) 6-HR 24-HR 72-HR 29.90-HR  
 + 0. 12.20 0. 0. 0. 0.  
 (INCHES) 2.891 4.072 4.073 4.073  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = 0.00 SQ MI

\*\*\*\*\*  
 \* SUB-6 \* SITE RUNOFF TO POINT # C  
 \*\*\*\*\*

\*\*\*\*\*  
 \* DRAINAGE AREA = 0.95 AC = 0.0015 SQ. MI. Q=1.06 cfs  
 \*\*\*\*\*



\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*  
 HYDROGRAPH AT STATION    SUB-6  
 FOR PLAN 1,    RATIO = 3.20  
 TOTAL RAINFALL =    3.20, TOTAL LOSS =    2.78, TOTAL EXCESS =    0.42  
 PEAK FLOW    TIME                    MAXIMUM AVERAGE FLOW  
 (CFS)        (HR)                    6-HR    24-HR    72-HR    29.90-HR  
 +            0.    12.40                    0.            0.            0.            0.  
               (INCHES)    0.341            0.423    0.423    0.423  
               (AC-FT)    0.            0.            0.            0.  
 CUMULATIVE AREA =    0.00 SQ MI

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*  
 HYDROGRAPH AT STATION    SUB-6  
 FOR PLAN 1,    RATIO = 4.20  
 TOTAL RAINFALL =    4.20, TOTAL LOSS =    3.38, TOTAL EXCESS =    0.82  
 PEAK FLOW    TIME                    MAXIMUM AVERAGE FLOW  
 (CFS)        (HR)                    6-HR    24-HR    72-HR    29.90-HR  
 +            1.    12.40                    0.            0.            0.            0.  
               (INCHES)    0.673            0.824    0.824    0.824  
               (AC-FT)    0.            0.            0.            0.  
 CUMULATIVE AREA =    0.00 SQ MI

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*  
 HYDROGRAPH AT STATION    SUB-6  
 FOR PLAN 1,    RATIO = 5.00  
 TOTAL RAINFALL =    5.00, TOTAL LOSS =    3.79, TOTAL EXCESS =    1.21  
 PEAK FLOW    TIME                    MAXIMUM AVERAGE FLOW  
 (CFS)        (HR)                    6-HR    24-HR    72-HR    29.90-HR  
 +            1.    12.40                    0.            0.            0.            0.  
               (INCHES)    0.990            1.209    1.209    1.209  
               (AC-FT)    0.            0.            0.            0.  
 CUMULATIVE AREA =    0.00 SQ MI

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*  
 HYDROGRAPH AT STATION    SUB-6  
 FOR PLAN 1,    RATIO = 5.60  
 TOTAL RAINFALL =    5.60, TOTAL LOSS =    4.07, TOTAL EXCESS =    1.53  
 PEAK FLOW    TIME                    MAXIMUM AVERAGE FLOW  
 (CFS)        (HR)                    6-HR    24-HR    72-HR    29.90-HR  
 +            1.    12.40                    0.            0.            0.            0.  
               (INCHES)    1.253            1.530    1.530    1.530  
               (AC-FT)    0.            0.            0.            0.

(AC-FT) 0. 0. 0. 0. 0.  
 CUMULATIVE AREA = 0.00 SQ MI

\*\*\*  
 HYDROGRAPH AT STATION SUB-6  
 FOR PLAN 1, RATIO = 7.30  
 TOTAL RAINFALL = 7.30, TOTAL LOSS = 4.74, TOTAL EXCESS = 2.56

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES) | 72-HR<br>(AC-FT) | 29.90-HR<br>(AC-FT) |
|--------------------|--------------|---------------|-------------------|------------------|---------------------|
| 2.                 | 12.40        | 0.            | 2.086             | 2.556            | 2.556               |
|                    |              | 0.            | 0.                | 0.               | 0.                  |

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*\*\*

72 KK \* PT-C \* COMBINE HYDROGRAPHS SUB-2 & SUB-6  
 \*\*\*\*\*

73 HC HYDROGRAPH COMBINATION  
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

\*\*\*  
 HYDROGRAPH AT STATION PT-C  
 FOR PLAN 1, RATIO = 3.20

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES) | 72-HR<br>(AC-FT) | 29.90-HR<br>(AC-FT) |
|--------------------|--------------|---------------|-------------------|------------------|---------------------|
| 0.                 | 12.40        | 0.            | 0.417             | 0.563            | 0.564               |
|                    |              | 0.            | 0.                | 0.               | 0.                  |

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*  
 HYDROGRAPH AT STATION PT-C  
 FOR PLAN 1, RATIO = 4.20

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES) | 72-HR<br>(AC-FT) | 29.90-HR<br>(AC-FT) |
|--------------------|--------------|---------------|-------------------|------------------|---------------------|
| 1.                 | 12.40        | 0.            | 0.757             | 0.982            | 0.983               |
|                    |              | 0.            | 0.                | 0.               | 0.                  |

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION PT-C  
FOR PLAN 1, RATIO = 5.00

| PEAK FLOW (CFS) | TIME (HR) | 6-HR (CFS) | 24-HR (CFS) | 72-HR (CFS) | 29.90-HR (CFS) |
|-----------------|-----------|------------|-------------|-------------|----------------|
| 0.              | 0.        | 0.         | 0.          | 0.          | 0.             |
| 1.378           | 12.40     | 1.077      | 1.377       | 1.378       | 1.378          |
| 0.              | 0.        | 0.         | 0.          | 0.          | 0.             |

CUMULATIVE AREA = 0.00 SQ MI

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION PT-C  
FOR PLAN 1, RATIO = 5.60

| PEAK FLOW (CFS) | TIME (HR) | 6-HR (CFS) | 24-HR (CFS) | 72-HR (CFS) | 29.90-HR (CFS) |
|-----------------|-----------|------------|-------------|-------------|----------------|
| 0.              | 0.        | 0.         | 0.          | 0.          | 0.             |
| 1.704           | 12.40     | 1.339      | 1.702       | 1.704       | 1.704          |
| 0.              | 0.        | 0.         | 0.          | 0.          | 0.             |

CUMULATIVE AREA = 0.00 SQ MI

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION PT-C  
FOR PLAN 1, RATIO = 7.30

| PEAK FLOW (CFS) | TIME (HR) | 6-HR (CFS) | 24-HR (CFS) | 72-HR (CFS) | 29.90-HR (CFS) |
|-----------------|-----------|------------|-------------|-------------|----------------|
| 0.              | 0.        | 0.         | 0.          | 0.          | 0.             |
| 2.734           | 12.40     | 2.168      | 2.732       | 2.734       | 2.734          |
| 0.              | 0.        | 0.         | 0.          | 0.          | 0.             |

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*\*\*

\* SUB-3 \* SITE RUNOFF TO POINT # B

\*\*\*\*\*

\*\*\*\*\*

\* DRAINAGE AREA = 0.14 AC = 0.0002 SQ. MI. Q=0.45 cfs

\* TIME OF CONCENTRATION = 0.7 MIN = 0.01 HR \* 0.6 = 0.07 (SCS LAG)

\*\*\*\*\*



FOR PLAN 1, RATIO = 3.20

TOTAL RAINFALL = 3.20, TOTAL LOSS = 1.21, TOTAL EXCESS = 1.99

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>MAXIMUM AVERAGE FLOW | 24-HR<br>MAXIMUM AVERAGE FLOW | 72-HR<br>MAXIMUM AVERAGE FLOW | 29.90-HR<br>MAXIMUM AVERAGE FLOW |
|--------------------|--------------|------------------------------|-------------------------------|-------------------------------|----------------------------------|
| 0.                 | 12.20        | 0.                           | 0.                            | 0.                            | 0.                               |
| 1.417              |              | 1.990                        | 1.991                         | 1.991                         | 1.991                            |
| 0.                 |              | 0.                           | 0.                            | 0.                            | 0.                               |

CUMULATIVE AREA = 0.00 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SUB-3  
FOR PLAN 1, RATIO = 4.20

TOTAL RAINFALL = 4.20, TOTAL LOSS = 1.37, TOTAL EXCESS = 2.83

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>MAXIMUM AVERAGE FLOW | 24-HR<br>MAXIMUM AVERAGE FLOW | 72-HR<br>MAXIMUM AVERAGE FLOW | 29.90-HR<br>MAXIMUM AVERAGE FLOW |
|--------------------|--------------|------------------------------|-------------------------------|-------------------------------|----------------------------------|
| 0.                 | 12.20        | 0.                           | 0.                            | 0.                            | 0.                               |
| 2.052              |              | 2.830                        | 2.831                         | 2.831                         | 2.831                            |
| 0.                 |              | 0.                           | 0.                            | 0.                            | 0.                               |

CUMULATIVE AREA = 0.00 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SUB-3  
FOR PLAN 1, RATIO = 5.00

TOTAL RAINFALL = 5.00, TOTAL LOSS = 1.47, TOTAL EXCESS = 3.53

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>MAXIMUM AVERAGE FLOW | 24-HR<br>MAXIMUM AVERAGE FLOW | 72-HR<br>MAXIMUM AVERAGE FLOW | 29.90-HR<br>MAXIMUM AVERAGE FLOW |
|--------------------|--------------|------------------------------|-------------------------------|-------------------------------|----------------------------------|
| 0.                 | 12.20        | 0.                           | 0.                            | 0.                            | 0.                               |
| 2.592              |              | 3.533                        | 3.535                         | 3.535                         | 3.535                            |
| 0.                 |              | 0.                           | 0.                            | 0.                            | 0.                               |

CUMULATIVE AREA = 0.00 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SUB-3  
FOR PLAN 1, RATIO = 5.60

TOTAL RAINFALL = 5.60, TOTAL LOSS = 1.53, TOTAL EXCESS = 4.07

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>MAXIMUM AVERAGE FLOW | 24-HR<br>MAXIMUM AVERAGE FLOW | 72-HR<br>MAXIMUM AVERAGE FLOW | 29.90-HR<br>MAXIMUM AVERAGE FLOW |
|--------------------|--------------|------------------------------|-------------------------------|-------------------------------|----------------------------------|
| 0.                 | 12.20        | 0.                           | 0.                            | 0.                            | 0.                               |
| 3.007              |              | 4.074                        | 4.075                         | 4.075                         | 4.075                            |
| 0.                 |              | 0.                           | 0.                            | 0.                            | 0.                               |

CUMULATIVE AREA = 0.00 SQ MI



92 LS

SCS LOSS RATE  
 STRTL 1.00 INITIAL ABSTRACTION  
 CRVNR 60.05 CURVE NUMBER  
 RTIME 24.49 PERCENT IMPERVIOUS AREA  
 SCS DIMENSIONLESS UNITGRAPH  
 TLAG 0.13 LAG

\*\*\*

UNIT HYDROGRAPH  
 8 END-OF-PERIOD ORDINATES

14. 23. 11. 4. 2. 1. 0.  
 TOTAL RAINFALL = 1.00, TOTAL LOSS = 0.76, TOTAL EXCESS = 0.24

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>MAXIMUM AVERAGE FLOW | 24-HR<br>MAXIMUM AVERAGE FLOW | 72-HR<br>MAXIMUM AVERAGE FLOW | 29.90-HR<br>MAXIMUM AVERAGE FLOW |
|--------------------|--------------|------------------------------|-------------------------------|-------------------------------|----------------------------------|
| +                  | 1. 12.30     | 0.                           | 0.                            | 0.                            | 0.                               |
|                    | (INCHES)     | 0.173                        | 0.245                         | 0.245                         | 0.245                            |
|                    | (AC-FT)      | 0.                           | 0.                            | 0.                            | 0.                               |

CUMULATIVE AREA = 0.01 SQ MI

\*\*\*

HYDROGRAPH AT STATION SUB-7  
 FOR PLAN 1, RATIO = 3.20

3.20, TOTAL LOSS = 2.00, TOTAL EXCESS = 1.20

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>MAXIMUM AVERAGE FLOW | 24-HR<br>MAXIMUM AVERAGE FLOW | 72-HR<br>MAXIMUM AVERAGE FLOW | 29.90-HR<br>MAXIMUM AVERAGE FLOW |
|--------------------|--------------|------------------------------|-------------------------------|-------------------------------|----------------------------------|
| +                  | 5. 12.30     | 1.                           | 0.                            | 0.                            | 0.                               |
|                    | (INCHES)     | 0.854                        | 1.196                         | 1.197                         | 1.197                            |
|                    | (AC-FT)      | 0.                           | 1.                            | 1.                            | 1.                               |

CUMULATIVE AREA = 0.01 SQ MI

\*\*\*

HYDROGRAPH AT STATION SUB-7  
 FOR PLAN 1, RATIO = 4.20

4.20, TOTAL LOSS = 2.39, TOTAL EXCESS = 1.81

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>MAXIMUM AVERAGE FLOW | 24-HR<br>MAXIMUM AVERAGE FLOW | 72-HR<br>MAXIMUM AVERAGE FLOW | 29.90-HR<br>MAXIMUM AVERAGE FLOW |
|--------------------|--------------|------------------------------|-------------------------------|-------------------------------|----------------------------------|
| +                  | 7. 12.30     | 1.                           | 0.                            | 0.                            | 0.                               |
|                    | (INCHES)     | 1.331                        | 1.812                         | 1.813                         | 1.813                            |
|                    | (AC-FT)      | 1.                           | 1.                            | 1.                            | 1.                               |

CUMULATIVE AREA = 0.01 SQ MI

\*\*\*  
 HYDROGRAPH AT STATION SUB-7  
 FOR PLAN 1, RATIO = 5.00  
 TOTAL RAINFALL = 5.00, TOTAL LOSS = 2.64, TOTAL EXCESS = 2.36  
 PEAK FLOW TIME  
 (CFS) (HR) MAXIMUM AVERAGE FLOW  
 6-HR 24-HR 72-HR 29.90-HR  
 + 10. 12.30 (CFS) 2. 1. 0. 0.  
 (INCHES) 1.756 2.357 2.359 2.359  
 (AC-FT) 1. 1. 1. 1.  
 CUMULATIVE AREA = 0.01 SQ MI

\*\*\*  
 HYDROGRAPH AT STATION SUB-7  
 FOR PLAN 1, RATIO = 5.60  
 TOTAL RAINFALL = 5.60, TOTAL LOSS = 2.81, TOTAL EXCESS = 2.79  
 PEAK FLOW TIME  
 (CFS) (HR) MAXIMUM AVERAGE FLOW  
 6-HR 24-HR 72-HR 29.90-HR  
 + 12. 12.30 (CFS) 2. 1. 1. 1.  
 (INCHES) 2.098 2.790 2.791 2.791  
 (AC-FT) 1. 1. 1. 1.  
 CUMULATIVE AREA = 0.01 SQ MI

\*\*\*  
 HYDROGRAPH AT STATION SUB-7  
 FOR PLAN 1, RATIO = 7.30  
 TOTAL RAINFALL = 7.30, TOTAL LOSS = 3.20, TOTAL EXCESS = 4.10  
 PEAK FLOW TIME  
 (CFS) (HR) MAXIMUM AVERAGE FLOW  
 6-HR 24-HR 72-HR 29.90-HR  
 + 18. 12.30 (CFS) 3. 1. 1. 1.  
 (INCHES) 3.121 4.100 4.102 4.102  
 (AC-FT) 1. 2. 2. 2.  
 CUMULATIVE AREA = 0.01 SQ MI

\*\*\*\*\*  
 \*  
 \* comb \* COMBINE HYDROGRAPHS SUB-3 & SUB-7  
 \*  
 \*\*\*\*\*  
 94 KK  
 \*\*\*\*\*  
 95 HC HYDROGRAPH COMBINATION



\*\*\* HYDROGRAPH AT STATION Comb  
 FOR PLAN 1, RATIO = 7.30  
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
 (CFS) (HR) 6-HR 24-HR 72-HR 29.90-HR  
 + 18. 12.30 (CFS) 3. 1. 1.  
 (INCHES) 3.146 4.135 4.137 4.137  
 (AC-FT) 1. 2. 2. 2.  
 CUMULATIVE AREA = 0.01 SQ MI

\*\*\*\*\*  
 \* BASIN1 \* ROUTING IN BASIN PRIOR TO DISCHARGE TOWARD "PT-B"  
 \* \*\*\*\*\*  
 96 KK

\*\*\*\*\*  
 \* OUTLET STRUCTURE DATA:  
 \* \*\*\*\*\*  
 \* TOP OF STRUCTURE OVERFLOW LENGTH: 13' LONG AT EL 435.0 \*  
 \* WEIR LENGTH = 2.0' WIDE AT EL 439.0 \*  
 \* ORIFICE #1: 3" DIAMETER AT EL.439.5 \*  
 \* \*\*\*\*\*

HYDROGRAPH ROUTING DATA  
 STORAGE ROUTING  
 NSTPS 1 NUMBER OF SUBREACHES  
 ITPP ELEV TYPE OF INITIAL CONDITION  
 RSVRIC 284.00 INITIAL CONDITION  
 X 0.00 WORKING R AND D COEFFICIENT  
 106 SA AREA 0.1 0.1 0.2 0.2  
 107 SE ELEVATION 284.00 286.00 288.00 289.00  
 108 SQ DISCHARGE 0. 0. 0. 0. 2. 5. 6. 10. 15.  
 109 SE ELEVATION 284.20 284.60 284.80 285.40 285.60 287.20 287.40 287.60 288.20

\*\*\*\*\*  
 COMPUTED STORAGE-ELEVATION DATA  
 STORAGE 0.00 0.20 0.49 0.67  
 ELEVATION 284.00 286.00 288.00 289.00  
 \*\*\*\*\*  
 COMPUTED STORAGE-OUTFLOW-ELEVATION DATA  
 STORAGE 0.00 0.02 0.05 0.07 0.13 0.15 0.20 0.35 0.39 0.42  
 OUTFLOW 0.07 0.07 0.17 0.20 0.27 1.51 2.45 5.43 5.73 6.30  
 ELEVATION 284.00 284.20 284.60 284.80 285.40 285.60 286.00 287.20 287.40 287.60

STORAGE 0.49 0.52 0.67  
 OUTFLOW 9.73 15.29 37.53  
 ELEVATION 288.00 288.20 289.00  
 \*\*\*

HYDROGRAPH AT STATION BASIN1  
 FOR PLAN 1, RATIO = 3.20

| PEAK FLOW | TIME     | 6-HR  | 24-HR | 72-HR | 29.90-HR |
|-----------|----------|-------|-------|-------|----------|
| +         | (CFS)    | 1.    | 0.    | 0.    | 0.       |
| +         | 2.       | 0.678 | 1.142 | 1.215 | 1.215    |
|           | (INCHES) | 0.    | 1.    | 1.    | 1.       |
|           | (AC-FT)  |       |       |       |          |

PEAK STORAGE TIME 29.90-HR  
 + (AC-FT) (HR) 0. 0. 0. 0.  
 0. 12.60

PEAK STAGE TIME 284.62  
 + (FEET) (HR) 285.46 284.77 284.62 284.62  
 12.60

CUMULATIVE AREA = 0.01 SQ MI

\*\*\*

HYDROGRAPH AT STATION BASIN1  
 FOR PLAN 1, RATIO = 4.20

| PEAK FLOW | TIME     | 6-HR  | 24-HR | 72-HR | 29.90-HR |
|-----------|----------|-------|-------|-------|----------|
| +         | (CFS)    | 1.    | 0.    | 0.    | 0.       |
| +         | 4.       | 1.182 | 1.731 | 1.805 | 1.805    |
|           | (INCHES) | 1.    | 1.    | 1.    | 1.       |
|           | (AC-FT)  |       |       |       |          |

PEAK STORAGE TIME 29.90-HR  
 + (AC-FT) (HR) 0. 0. 0. 0.  
 0. 12.60

PEAK STAGE TIME 284.75  
 + (FEET) (HR) 285.61 284.94 284.75 284.75  
 12.60

CUMULATIVE AREA = 0.01 SQ MI

\*\*\*

HYDROGRAPH AT STATION BASIN1  
 FOR PLAN 1, RATIO = 5.00

| PEAK FLOW | TIME     | 6-HR  | 24-HR | 72-HR | 29.90-HR |
|-----------|----------|-------|-------|-------|----------|
| +         | (CFS)    | 2.    | 1.    | 0.    | 0.       |
| +         | 5.       | 1.645 | 2.260 | 2.333 | 2.333    |
|           | (INCHES) | 1.    | 1.    | 1.    | 1.       |
|           | (AC-FT)  |       |       |       |          |

|              |         |        |        |        |          |
|--------------|---------|--------|--------|--------|----------|
|              | (AC-FT) | 1.     | 1.     | 1.     | 1.       |
| PEAK STORAGE | TIME    |        |        |        |          |
| + (AC-FT)    | (HR)    | 6-HR   | 24-HR  | 72-HR  | 29.90-HR |
| 0.           | 12.60   | 0.     | 0.     | 0.     | 0.       |
| PEAK STAGE   | TIME    |        |        |        |          |
| + (FEET)     | (HR)    | 6-HR   | 24-HR  | 72-HR  | 29.90-HR |
| 287.01       | 12.60   | 285.75 | 285.06 | 284.85 | 284.85   |

CUMULATIVE AREA = 0.01 SQ MI

\*\*\* HYDROGRAPH AT STATION BASINI FOR PLAN 1, RATIO = 5.60 \*\*\*

|           |       |       |       |       |          |
|-----------|-------|-------|-------|-------|----------|
|           | (CFS) | 2.    | 1.    | 1.    | 1.       |
| PEAK FLOW | TIME  |       |       |       |          |
| + (CFS)   | (HR)  | 6-HR  | 24-HR | 72-HR | 29.90-HR |
| 6.        | 12.60 | 2.014 | 2.687 | 2.760 | 2.760    |
|           |       | 1.    | 1.    | 1.    | 1.       |

PEAK STORAGE

|            |       |        |        |        |          |
|------------|-------|--------|--------|--------|----------|
| + (AC-FT)  | (HR)  | 6-HR   | 24-HR  | 72-HR  | 29.90-HR |
| 0.         | 12.60 | 0.     | 0.     | 0.     | 0.       |
| PEAK STAGE | TIME  |        |        |        |          |
| + (FEET)   | (HR)  | 6-HR   | 24-HR  | 72-HR  | 29.90-HR |
| 287.41     | 12.60 | 285.87 | 285.14 | 284.92 | 284.92   |

CUMULATIVE AREA = 0.01 SQ MI

\*\*\* HYDROGRAPH AT STATION BASINI FOR PLAN 1, RATIO = 7.30 \*\*\*

|           |       |       |       |       |          |
|-----------|-------|-------|-------|-------|----------|
|           | (CFS) | 3.    | 1.    | 1.    | 1.       |
| PEAK FLOW | TIME  |       |       |       |          |
| + (CFS)   | (HR)  | 6-HR  | 24-HR | 72-HR | 29.90-HR |
| 13.       | 12.50 | 3.109 | 3.994 | 4.069 | 4.069    |
|           |       | 1.    | 2.    | 2.    | 2.       |

PEAK STORAGE

|            |       |        |        |        |          |
|------------|-------|--------|--------|--------|----------|
| + (AC-FT)  | (HR)  | 6-HR   | 24-HR  | 72-HR  | 29.90-HR |
| 1.         | 12.50 | 0.     | 0.     | 0.     | 0.       |
| PEAK STAGE | TIME  |        |        |        |          |
| + (FEET)   | (HR)  | 6-HR   | 24-HR  | 72-HR  | 29.90-HR |
| 288.11     | 12.50 | 286.13 | 285.29 | 285.05 | 285.05   |

CUMULATIVE AREA = 0.01 SQ MI

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\*\*\*\*\*  
 \* TO PTB \*  
 \* \*\*\*\*\*  
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| DT | DIVERSION     | ISTAD | TO PTA | DIVERSION HYDROGRAPH IDENTIFICATION |       |       |      |      |      |      |       |
|----|---------------|-------|--------|-------------------------------------|-------|-------|------|------|------|------|-------|
| DI | INFLOW        | 0.00  | 1.30   | 1.86                                | 2.27  | 4.72  | 6.24 | 7.45 | 8.49 | 9.41 | 10.25 |
|    |               | 11.03 | 11.75  | 12.43                               | 13.08 | 13.69 |      |      |      |      |       |
| DQ | DIVERTED FLOW | 0.00  | 1.09   | 1.58                                | 1.93  | 4.33  | 5.80 | 6.97 | 7.98 | 8.86 | 9.67  |
|    |               | 10.42 | 11.11  | 11.77                               | 12.39 | 12.98 |      |      |      |      |       |

\*\*\*

| PEAK FLOW | TIME  | 6-HR     | 24-HR   | 72-HR   | 29.90-HR |
|-----------|-------|----------|---------|---------|----------|
| 2.        | 12.60 | 0.572    | 0.960   | 1.022   | 1.022    |
| (CFS)     | (HR)  | (INCHES) | (AC-FT) | (AC-FT) | (AC-FT)  |
|           |       | 0.       | 0.      | 0.      | 0.       |

CUMULATIVE AREA = 0.01 SQ MI

\*\*\*

| PEAK FLOW | TIME  | 6-HR     | 24-HR   | 72-HR   | 29.90-HR |
|-----------|-------|----------|---------|---------|----------|
| 0.        | 12.60 | 0.       | 0.      | 0.      | 0.       |
| (CFS)     | (HR)  | (INCHES) | (AC-FT) | (AC-FT) | (AC-FT)  |
|           |       | 0.107    | 0.182   | 0.193   | 0.193    |
|           |       | 0.       | 0.      | 0.      | 0.       |

CUMULATIVE AREA = 0.01 SQ MI

\*\*\*

| PEAK FLOW | TIME  | 6-HR     | 24-HR   | 72-HR   | 29.90-HR |
|-----------|-------|----------|---------|---------|----------|
| 3.        | 12.60 | 1.020    | 1.480   | 1.542   | 1.542    |
| (CFS)     | (HR)  | (INCHES) | (AC-FT) | (AC-FT) | (AC-FT)  |
|           |       | 0.       | 0.      | 0.      | 0.       |
|           |       | 1.       | 1.      | 1.      | 1.       |

CUMULATIVE AREA = 0.01 SQ MI

\*\*\*  
HYDROGRAPH AT STATION TO PTB  
FOR PLAN 1, RATIO = 4.20

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | MAXIMUM AVERAGE FLOW<br>72-HR<br>(CFS) | 29.90-HR<br>(INCHES)<br>(AC-FT) |
|--------------------|--------------|---------------|------------------------------|----------------------------------------|---------------------------------|
| 0.                 | 12.50        | 0.            | 0.                           | 0.                                     | 0.                              |
|                    |              | 0.163         | 0.251                        | 0.263                                  | 0.263                           |
|                    |              | 0.            | 0.                           | 0.                                     | 0.                              |

CUMULATIVE AREA = 0.01 SQ MI

\*\*\*  
DIVERSION HYDROGRAPH TO PTA  
FOR PLAN 1, RATIO = 5.00

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | MAXIMUM AVERAGE FLOW<br>72-HR<br>(CFS) | 29.90-HR<br>(INCHES)<br>(AC-FT) |
|--------------------|--------------|---------------|------------------------------|----------------------------------------|---------------------------------|
| 5.                 | 12.60        | 1.            | 0.                           | 0.                                     | 0.                              |
|                    |              | 1.442         | 1.958                        | 2.020                                  | 2.020                           |
|                    |              | 1.            | 1.                           | 1.                                     | 1.                              |

CUMULATIVE AREA = 0.01 SQ MI

\*\*\*  
HYDROGRAPH AT STATION TO PTB  
FOR PLAN 1, RATIO = 5.00

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | MAXIMUM AVERAGE FLOW<br>72-HR<br>(CFS) | 29.90-HR<br>(INCHES)<br>(AC-FT) |
|--------------------|--------------|---------------|------------------------------|----------------------------------------|---------------------------------|
| 0.                 | 12.50        | 0.            | 0.                           | 0.                                     | 0.                              |
|                    |              | 0.203         | 0.302                        | 0.314                                  | 0.314                           |
|                    |              | 0.            | 0.                           | 0.                                     | 0.                              |

CUMULATIVE AREA = 0.01 SQ MI

\*\*\*  
DIVERSION HYDROGRAPH TO PTA  
FOR PLAN 1, RATIO = 5.60

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | MAXIMUM AVERAGE FLOW<br>72-HR<br>(CFS) | 29.90-HR<br>(INCHES)<br>(AC-FT) |
|--------------------|--------------|---------------|------------------------------|----------------------------------------|---------------------------------|
| 5.                 | 12.60        | 2.            | 1.                           | 0.                                     | 0.                              |
|                    |              | 1.782         | 2.346                        | 2.407                                  | 2.407                           |
|                    |              | 1.            | 1.                           | 1.                                     | 1.                              |

CUMULATIVE AREA = 0.01 SQ MI





PEAK FLOW TIME  
 (CFS) (HR)  
 + 4. 12.30  
 (CFS)  
 (INCHES) 0.509 1. 0. 0.  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = 0.01 SQ MI

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HYDROGRAPH AT STATION SUB-1  
 FOR PLAN 1, RATIO = 4.20

TOTAL RAINFALL = 4.20, TOTAL LOSS = 3.03, TOTAL EXCESS = 1.17

PEAK FLOW TIME  
 (CFS) (HR)  
 + 7. 12.30  
 (CFS)  
 (INCHES) 0.895 1. 0. 0.  
 (AC-FT) 1. 1. 1. 1.  
 CUMULATIVE AREA = 0.01 SQ MI

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HYDROGRAPH AT STATION SUB-1  
 FOR PLAN 1, RATIO = 5.00

TOTAL RAINFALL = 5.00, TOTAL LOSS = 3.39, TOTAL EXCESS = 1.61

PEAK FLOW TIME  
 (CFS) (HR)  
 + 10. 12.30  
 (CFS)  
 (INCHES) 1.253 2. 1. 0.  
 (AC-FT) 1. 1. 1. 1.  
 CUMULATIVE AREA = 0.01 SQ MI

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HYDROGRAPH AT STATION SUB-1  
 FOR PLAN 1, RATIO = 5.60

TOTAL RAINFALL = 5.60, TOTAL LOSS = 3.63, TOTAL EXCESS = 1.97

PEAK FLOW TIME  
 (CFS) (HR)  
 + 12. 12.30  
 (CFS)  
 (INCHES) 1.545 2. 1. 1.  
 (AC-FT) 1. 1. 1. 1.  
 CUMULATIVE AREA = 0.01 SQ MI

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 \*\*\*

HYDROGRAPH AT STATION SUB-1  
 FOR PLAN 1, RATIO = 7.30  
 TOTAL RAINFALL = 7.30, TOTAL LOSS = 4.20, TOTAL EXCESS = 3.10

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | 72-HR<br>MAXIMUM AVERAGE FLOW | 29.90-HR<br>MAXIMUM AVERAGE FLOW |
|--------------------|--------------|---------------|------------------------------|-------------------------------|----------------------------------|
| 19.                | 12.30        | 3.            | 1.                           | 1.                            | 1.                               |
|                    |              | 2.454         | 3.103                        | 3.104                         | 3.104                            |
|                    |              | 2.            | 2.                           | 2.                            | 2.                               |

CUMULATIVE AREA = 0.01 SQ MI

\*\*\*\*\*

\*\*\*\*\*  
 \* LAG-1 \* LAG OFF-1 HYDROGRAPH TO POINT #A  
 \*\*\*\*\*

HYDROGRAPH ROUTING DATA

127 RT TATUM OR STRADDLE-STACGER ROUTING  
 NSTPS 0 NUMBER OF TATUM STEPS  
 NSTDL 0 NUMBER OF ORDINATES TO BE AVERAGED  
 LAG 1 NUMBER OF INTERVALS TO LAG HYDROGRAPH

\*\*\*  
 HYDROGRAPH AT STATION LAG-1  
 FOR PLAN 1, RATIO = 3.20

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | 72-HR<br>MAXIMUM AVERAGE FLOW | 29.90-HR<br>MAXIMUM AVERAGE FLOW |
|--------------------|--------------|---------------|------------------------------|-------------------------------|----------------------------------|
| 4.                 | 12.40        | 1.            | 0.                           | 0.                            | 0.                               |
|                    |              | 0.509         | 0.690                        | 0.690                         | 0.690                            |
|                    |              | 0.            | 0.                           | 0.                            | 0.                               |

CUMULATIVE AREA = 0.01 SQ MI

\*\*\*  
 HYDROGRAPH AT STATION LAG-1  
 FOR PLAN 1, RATIO = 4.20

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>(CFS) | 24-HR<br>(INCHES)<br>(AC-FT) | 72-HR<br>MAXIMUM AVERAGE FLOW | 29.90-HR<br>MAXIMUM AVERAGE FLOW |
|--------------------|--------------|---------------|------------------------------|-------------------------------|----------------------------------|
| 7.                 | 12.40        | 1.            | 0.                           | 0.                            | 0.                               |
|                    |              | 0.895         | 1.167                        | 1.168                         | 1.168                            |
|                    |              | 1.            | 1.                           | 1.                            | 1.                               |

CUMULATIVE AREA = 0.01 SQ MI

```

***          ***          ***          ***
HYDROGRAPH AT STATION LAG-1
FOR PLAN 1, RATIO = 5.00
***
PEAK FLOW          TIME          MAXIMUM AVERAGE FLOW
(CFS)              (HR)              24-HR          72-HR          29.90-HR
+ 10.              12.40             2.              1.              0.
(INCHES)           1.253            1.611           1.611          1.611
(AC-FT)            1.              1.              1.              1.
CUMULATIVE AREA = 0.01 SQ MI
***

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***          ***          ***          ***
HYDROGRAPH AT STATION LAG-1
FOR PLAN 1, RATIO = 5.60
***
PEAK FLOW          TIME          MAXIMUM AVERAGE FLOW
(CFS)              (HR)              24-HR          72-HR          29.90-HR
+ 12.              12.40             2.              1.              1.
(INCHES)           1.545            1.972           1.973          1.973
(AC-FT)            1.              1.              1.              1.
CUMULATIVE AREA = 0.01 SQ MI
***

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***          ***          ***          ***
HYDROGRAPH AT STATION LAG-1
FOR PLAN 1, RATIO = 7.30
***
PEAK FLOW          TIME          MAXIMUM AVERAGE FLOW
(CFS)              (HR)              24-HR          72-HR          29.90-HR
+ 19.              12.40             3.              1.              1.
(INCHES)           2.454            3.103           3.104          3.104
(AC-FT)            2.              2.              2.              2.
CUMULATIVE AREA = 0.01 SQ MI
***

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*****
* SUB-4 * OFFSITE RUNOFF TO POINT #A
*
*****

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*****
* DRAINAGE AREA = 0.15 AC = 0.0002 SQ. MI.          Q=0.48 CFS
* TIME OF CONCENTRATION = 1.0MIN = 0.01 HR * 0.6 = 0.01 (SCS LAG)
*****

```

SUBBASIN RUNOFF DATA



PEAK FLOW TIME  
 (CFS) (HR)  
 + 0. 12.20  
 (CFS)  
 (INCHES) 1.455 2.037 2.037 2.037  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = 0.00 SQ MI

\*\*\*  
 HYDROGRAPH AT STATION SUB-4  
 FOR PLAN 1, RATIO = 4.20  
 TOTAL RAINFALL = 4.20, TOTAL LOSS = 1.30, TOTAL EXCESS = 2.90  
 PEAK FLOW TIME  
 (CFS) (HR)  
 + 0. 12.20  
 (CFS)  
 (INCHES) 2.112 2.900 2.900 2.900  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = 0.00 SQ MI

\*\*\*  
 HYDROGRAPH AT STATION SUB-4  
 FOR PLAN 1, RATIO = 5.00  
 TOTAL RAINFALL = 5.00, TOTAL LOSS = 1.38, TOTAL EXCESS = 3.62  
 PEAK FLOW TIME  
 (CFS) (HR)  
 + 0. 12.20  
 (CFS)  
 (INCHES) 2.667 3.619 3.620 3.620  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = 0.00 SQ MI

\*\*\*  
 HYDROGRAPH AT STATION SUB-4  
 FOR PLAN 1, RATIO = 5.60  
 TOTAL RAINFALL = 5.60, TOTAL LOSS = 1.43, TOTAL EXCESS = 4.17  
 PEAK FLOW TIME  
 (CFS) (HR)  
 + 0. 12.20  
 (CFS)  
 (INCHES) 3.093 4.170 4.171 4.171  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = 0.00 SQ MI



146 LS SCS LOSS RATE 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00

STRFL 1.00 INITIAL ABSTRACTION  
 CRVNR 52.80 CURVE NUMBER  
 RTIMP 0.00 PERCENT IMPERVIOUS AREA  
 SCS DIMENSIONLESS UNITGRAPH  
 TLAG 0.10 LAG

\*\*\*

UNIT HYDROGRAPH  
 7 END-OF-PERIOD ORDINATES  
 0. 0. 0. 0.

8. 8. 3. 1. 1.00, TOTAL LOSS = 1.00, TOTAL EXCESS = 0.00

PEAK FLOW TIME 6-HR 24-HR 72-HR 29.90-HR  
 (CFS) (HR) MAXIMUM AVERAGE FLOW  
 + 0. 0.10 0. 0. 0. 0. 0. 0.  
 (INCHES) 0.000 0.000 0.000 0.000  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SUB-8  
 FOR PLAN 1, RATIO = 3.20

TOTAL RAINFALL = 3.20, TOTAL LOSS = 2.77, TOTAL EXCESS = 0.43

PEAK FLOW TIME 6-HR 24-HR 72-HR 29.90-HR  
 (CFS) (HR) MAXIMUM AVERAGE FLOW  
 + 1. 12.30 0. 0. 0. 0. 0. 0.  
 (INCHES) 0.351 0.434 0.434 0.434  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SUB-8  
 FOR PLAN 1, RATIO = 4.20

TOTAL RAINFALL = 4.20, TOTAL LOSS = 3.36, TOTAL EXCESS = 0.84

PEAK FLOW TIME 6-HR 24-HR 72-HR 29.90-HR  
 (CFS) (HR) MAXIMUM AVERAGE FLOW  
 + 1. 12.30 0. 0. 0. 0. 0. 0.  
 (INCHES) 0.691 0.844 0.844 0.844  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SUB-8  
FOR PLAN 1, RATIO = 5.00

TOTAL RAINFALL = 5.00, TOTAL LOSS = 3.76, TOTAL EXCESS = 1.24

| PEAK FLOW TIME | 6-HR  | 24-HR | 72-HR | 29.90-HR |
|----------------|-------|-------|-------|----------|
| (CFS)          |       |       |       |          |
| +              | 0.    | 0.    | 0.    | 0.       |
| (INCHES)       | 1.014 | 1.237 | 1.237 | 1.237    |
| (AC-FT)        | 0.    | 0.    | 0.    | 0.       |

CUMULATIVE AREA = 0.00 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SUB-8  
FOR PLAN 1, RATIO = 5.60

TOTAL RAINFALL = 5.60, TOTAL LOSS = 4.04, TOTAL EXCESS = 1.56

| PEAK FLOW TIME | 6-HR  | 24-HR | 72-HR | 29.90-HR |
|----------------|-------|-------|-------|----------|
| (CFS)          |       |       |       |          |
| +              | 0.    | 0.    | 0.    | 0.       |
| (INCHES)       | 1.281 | 1.563 | 1.563 | 1.563    |
| (AC-FT)        | 0.    | 0.    | 0.    | 0.       |

CUMULATIVE AREA = 0.00 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SUB-8  
FOR PLAN 1, RATIO = 7.30

TOTAL RAINFALL = 7.30, TOTAL LOSS = 4.70, TOTAL EXCESS = 2.60

| PEAK FLOW TIME | 6-HR  | 24-HR | 72-HR | 29.90-HR |
|----------------|-------|-------|-------|----------|
| (CFS)          |       |       |       |          |
| +              | 1.    | 0.    | 0.    | 0.       |
| (INCHES)       | 2.128 | 2.604 | 2.604 | 2.604    |
| (AC-FT)        | 0.    | 0.    | 0.    | 0.       |

CUMULATIVE AREA = 0.00 SQ MI

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\*\*\*\*\*  
\* SUB-5 \*  
\* SITE RUNOFF TO POINT #A \*  
\*\*\*\*\*

\*\*\*\*\*  
\* DRAINAGE AREA = 0.12 AC = 0.0002 SQ MI. O=0.38 cfs  
\* TIME OF CONCENTRATION = 1.0 MIN = 0.016 HR \* 0.6 = 0.01 (SCS LAG)  
\*\*\*\*\*



FOR PLAN 1, RATIO = 3.20

TOTAL RAINFALL = 3.20, TOTAL LOSS = 1.44, TOTAL EXCESS = 1.76

| PEAK FLOW TIME | 6-HR  | 24-HR | 72-HR | 29.90-HR |
|----------------|-------|-------|-------|----------|
| (CFS)          | 0.    | 0.    | 0.    | 0.       |
| (INCHES)       | 1.239 | 1.762 | 1.762 | 1.762    |
| (AC-FT)        | 0.    | 0.    | 0.    | 0.       |

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SUB-5  
FOR PLAN 1, RATIO = 4.20

TOTAL RAINFALL = 4.20, TOTAL LOSS = 1.75, TOTAL EXCESS = 2.45

| PEAK FLOW TIME | 6-HR  | 24-HR | 72-HR | 29.90-HR |
|----------------|-------|-------|-------|----------|
| (CFS)          | 0.    | 0.    | 0.    | 0.       |
| (INCHES)       | 1.743 | 2.454 | 2.455 | 2.455    |
| (AC-FT)        | 0.    | 0.    | 0.    | 0.       |

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SUB-5  
FOR PLAN 1, RATIO = 5.00

TOTAL RAINFALL = 5.00, TOTAL LOSS = 1.96, TOTAL EXCESS = 3.04

| PEAK FLOW TIME | 6-HR  | 24-HR | 72-HR | 29.90-HR |
|----------------|-------|-------|-------|----------|
| (CFS)          | 0.    | 0.    | 0.    | 0.       |
| (INCHES)       | 2.177 | 3.042 | 3.043 | 3.043    |
| (AC-FT)        | 0.    | 0.    | 0.    | 0.       |

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*

HYDROGRAPH AT STATION SUB-5  
FOR PLAN 1, RATIO = 5.60

TOTAL RAINFALL = 5.60, TOTAL LOSS = 2.10, TOTAL EXCESS = 3.50

| PEAK FLOW TIME | 6-HR  | 24-HR | 72-HR | 29.90-HR |
|----------------|-------|-------|-------|----------|
| (CFS)          | 0.    | 0.    | 0.    | 0.       |
| (INCHES)       | 2.518 | 3.500 | 3.501 | 3.501    |
| (AC-FT)        | 0.    | 0.    | 0.    | 0.       |

CUMULATIVE AREA = 0.00 SQ MI



166 LS SCS LOSS RATE 1.00 INITIAL ABSTRACTION  
 STRTL 53.90 CURVE NUMBER  
 CRVNR 33.45 PERCENT IMPERVIOUS AREA  
 RTMP  
 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00

167 UD SCS DIMENSIONLESS UNITGRAPH  
 TLAG 0.03 LAG  
 \*\*\*

UNIT HYDROGRAPH  
 5 END-OF-PERIOD ORDINATES

22. 6. 1. 0. 0.33  
 TOTAL RAINFALL = 1.00, TOTAL LOSS = 0.67, TOTAL EXCESS = 0.33  
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
 (CFS) 6-HR 24-HR 72-HR 29.90-HR  
 + 1. 12.20 0. 0. 0. 0.  
 (INCHES) 0.236 0.334 0.335 0.335  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = 0.00 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SUB-9  
 FOR PLAN 1, RATIO = 3.20

3. 20. 1.83, TOTAL EXCESS = 1.37  
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
 (CFS) 6-HR 24-HR 72-HR 29.90-HR  
 + 3. 12.20 0. 0. 0. 0.  
 (INCHES) 0.967 1.370 1.370 1.370  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = 0.00 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION SUB-9  
 FOR PLAN 1, RATIO = 4.20

4. 20. 2.22, TOTAL EXCESS = 1.98  
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
 (CFS) 6-HR 24-HR 72-HR 29.90-HR  
 + 5. 12.20 1. 0. 0. 0.  
 (INCHES) 1.425 1.984 1.985 1.985  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = 0.00 SQ MI

\*\*\* \*\*

\*\*\* HYDROGRAPH AT STATION SUB-9  
 FOR PLAN 1, RATIO = 5.00  
 TOTAL RAINFALL = 5.00, TOTAL LOSS = 2.48, TOTAL EXCESS = 2.52

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR     | 24-HR | 72-HR | 29.90-HR |
|--------------------|--------------|----------|-------|-------|----------|
| 6.                 | 12.20        | 1.       | 0.    | 0.    | 0.       |
|                    |              | 1.832    | 2.520 | 2.521 | 2.521    |
|                    |              | (INCHES) |       |       |          |
|                    |              | (AC-FT)  | 1.    | 1.    | 1.       |

CUMULATIVE AREA = 0.00 SQ MI

\*\*\* HYDROGRAPH AT STATION SUB-9  
 FOR PLAN 1, RATIO = 5.60  
 TOTAL RAINFALL = 5.60, TOTAL LOSS = 2.66, TOTAL EXCESS = 2.94

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR     | 24-HR | 72-HR | 29.90-HR |
|--------------------|--------------|----------|-------|-------|----------|
| 7.                 | 12.20        | 1.       | 0.    | 0.    | 0.       |
|                    |              | 2.155    | 2.943 | 2.944 | 2.944    |
|                    |              | (INCHES) |       |       |          |
|                    |              | (AC-FT)  | 1.    | 1.    | 1.       |

CUMULATIVE AREA = 0.00 SQ MI

\*\*\* HYDROGRAPH AT STATION SUB-9  
 FOR PLAN 1, RATIO = 7.30  
 TOTAL RAINFALL = 7.30, TOTAL LOSS = 3.08, TOTAL EXCESS = 4.22

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR     | 24-HR | 72-HR | 29.90-HR |
|--------------------|--------------|----------|-------|-------|----------|
| 11.                | 12.20        | 2.       | 1.    | 0.    | 0.       |
|                    |              | 3.130    | 4.219 | 4.220 | 4.220    |
|                    |              | (INCHES) |       |       |          |
|                    |              | (AC-FT)  | 1.    | 1.    | 1.       |

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*\*\*  
 \* \* \* \* \*  
 168 KK \* Comb \* COMBINE HYDROGRAPHS SUB-5 & SUB-9  
 \* \* \* \* \*  
 \*\*\*\*\*

169 HC HYDROGRAPH COMBINATION



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HYDROGRAPH AT STATION comb  
FOR PLAN 1, RATIO = 7.30

| PEAK FLOW<br>(CFS) | TIME<br>(HR) | 6-HR<br>AVERAGE FLOW | 24-HR<br>AVERAGE FLOW | 72-HR<br>AVERAGE FLOW | 29.90-HR<br>AVERAGE FLOW |
|--------------------|--------------|----------------------|-----------------------|-----------------------|--------------------------|
| 11.                | 12.20        | 2.                   | 1.                    | 0.                    | 0.                       |
|                    |              | 3.147                | 4.246                 | 4.247                 | 4.247                    |
|                    |              | (INCHES)             |                       |                       |                          |
|                    |              | (AC-FT)              |                       |                       |                          |
|                    |              | 1.                   | 1.                    | 1.                    | 1.                       |

CUMULATIVE AREA = 0.00 SQ MI

\*\*\*\*\*

170 KK \* BASINZ \* ROUTING IN BASIN PRIOR TO DISCHARGE TOWARD "PT-B"

\*\*\*\*\*

OUTLET STRUCTURE DATA:  
 \* TOP OF STRUCTURE OVERFLOW LENGTH: 13' LONG AT EL 435.0 \*  
 \* WEIR LENGTH = 2.0' WIDE AT EL 439.0 \*  
 \* ORIFICE #1: 3" DIAMETER AT EL 439.5 \*  
 \*\*\*\*\*

HYDROGRAPH ROUTING DATA

| STORAGE ROUTING<br>NSTES | 1<br>NUMBER OF SUBREACHES                                                                         |
|--------------------------|---------------------------------------------------------------------------------------------------|
| ITYP                     | ELEV TYPE OF INITIAL CONDITION                                                                    |
| RSVRIC                   | 284.00 INITIAL CONDITION                                                                          |
| X                        | 0.00 WORKING R AND D COEFFICIENT                                                                  |
| 179 RS                   | 0.1 0.1 0.1                                                                                       |
| 180 SA                   | 0.1 0.1 0.1                                                                                       |
| 181 SE                   | 284.00 286.00 288.00                                                                              |
| 182 SQ                   | 0. 0. 2. 3. 6. 11.                                                                                |
| 183 SE                   | 284.20 285.00 285.20 285.40 285.60 285.80 286.00 286.20 286.40 286.60 286.80 287.00 287.20 287.40 |

\*\*\*

COMPUTED STORAGE-ELEVATION DATA

|                                         |        |        |        |        |        |        |        |        |        |
|-----------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| STORAGE                                 | 0.00   | 0.16   | 0.41   |        |        |        |        |        |        |
| ELEVATION                               | 284.00 | 286.00 | 288.00 |        |        |        |        |        |        |
| COMPUTED STORAGE-OUTFLOW-ELEVATION DATA |        |        |        |        |        |        |        |        |        |
| STORAGE                                 | 0.00   | 0.07   | 0.08   | 0.10   | 0.12   | 0.16   | 0.25   | 0.27   | 0.30   |
| OUTFLOW                                 | 0.07   | 0.07   | 0.22   | 1.97   | 2.70   | 3.27   | 4.03   | 5.55   | 6.93   |
| ELEVATION                               | 284.00 | 284.20 | 285.00 | 285.20 | 285.40 | 285.60 | 286.00 | 286.80 | 287.00 |
| STORAGE                                 | 0.32   | 0.41   |        |        |        |        |        |        |        |
| OUTFLOW                                 | 10.76  | 22.25  |        |        |        |        |        |        |        |

| ELEVATION    | 287.40                                                   | 288.00                       | ***    |        |          | *** |
|--------------|----------------------------------------------------------|------------------------------|--------|--------|----------|-----|
| ***          | HYDROGRAPH AT STATION BASINZ<br>FOR PLAN 1, RATIO = 3.20 |                              |        |        |          | *** |
| PEAK FLOW    | TIME                                                     | 6-HR                         | 24-HR  | 72-HR  | 29.90-HR |     |
| +            | (CFS)                                                    | 0.                           | 0.     | 0.     | 0.       |     |
| +            | 2. 12.40                                                 | 0.819                        | 1.375  | 1.512  | 1.512    |     |
|              | (INCHES)                                                 | 0.                           | 0.     | 0.     | 0.       |     |
|              | (AC-FT)                                                  | 0.                           | 0.     | 0.     | 0.       |     |
| PEAK STORAGE | TIME                                                     | 6-HR                         | 24-HR  | 72-HR  | 29.90-HR |     |
| +            | (AC-FT)                                                  | 0.                           | 0.     | 0.     | 0.       |     |
| +            | 0. 12.30                                                 | 0.                           | 0.     | 0.     | 0.       |     |
| PEAK STAGE   | TIME                                                     | 6-HR                         | 24-HR  | 72-HR  | 29.90-HR |     |
| +            | (FEET)                                                   | 284.98                       | 284.43 | 284.35 | 284.35   |     |
|              | 285.29                                                   | CUMULATIVE AREA = 0.00 SQ MI |        |        |          |     |
| ***          | ***                                                      |                              |        |        |          | *** |
| ***          | HYDROGRAPH AT STATION BASINZ<br>FOR PLAN 1, RATIO = 4.20 |                              |        |        |          | *** |
| PEAK FLOW    | TIME                                                     | 6-HR                         | 24-HR  | 72-HR  | 29.90-HR |     |
| +            | (CFS)                                                    | 1.                           | 0.     | 0.     | 0.       |     |
| +            | 3. 12.40                                                 | 1.292                        | 1.937  | 2.074  | 2.074    |     |
|              | (INCHES)                                                 | 0.                           | 0.     | 0.     | 0.       |     |
|              | (AC-FT)                                                  | 0.                           | 0.     | 0.     | 0.       |     |
| PEAK STORAGE | TIME                                                     | 6-HR                         | 24-HR  | 72-HR  | 29.90-HR |     |
| +            | (AC-FT)                                                  | 0.                           | 0.     | 0.     | 0.       |     |
| +            | 0. 12.40                                                 | 0.                           | 0.     | 0.     | 0.       |     |
| PEAK STAGE   | TIME                                                     | 6-HR                         | 24-HR  | 72-HR  | 29.90-HR |     |
| +            | (FEET)                                                   | 285.06                       | 284.53 | 284.42 | 284.42   |     |
|              | 285.62                                                   | CUMULATIVE AREA = 0.00 SQ MI |        |        |          |     |
| ***          | ***                                                      |                              |        |        |          | *** |
| ***          | HYDROGRAPH AT STATION BASINZ<br>FOR PLAN 1, RATIO = 5.00 |                              |        |        |          | *** |
| PEAK FLOW    | TIME                                                     | 6-HR                         | 24-HR  | 72-HR  | 29.90-HR |     |
| +            | (CFS)                                                    | 1.                           | 0.     | 0.     | 0.       |     |
| +            | 4. 12.40                                                 | 1.724                        | 2.442  | 2.578  | 2.578    |     |
|              | (INCHES)                                                 | 0.                           | 0.     | 0.     | 0.       |     |
|              | (AC-FT)                                                  | 0.                           | 0.     | 0.     | 0.       |     |

|              |       |        |                              |          |
|--------------|-------|--------|------------------------------|----------|
| PEAK STORAGE | TIME  | 6-HR   | MAXIMUM AVERAGE STORAGE      | 29.90-HR |
| + (AC-FT)    | (HR)  | 0.     | 24-HR                        | 72-HR    |
|              | 12.40 |        | 0.                           | 0.       |
| PEAK STAGE   | TIME  | 6-HR   | MAXIMUM AVERAGE STAGE        | 29.90-HR |
| + (FEET)     | (HR)  | 285.11 | 24-HR                        | 72-HR    |
|              | 12.40 |        | 284.60                       | 284.48   |
|              |       |        | CUMULATIVE AREA = 0.00 SQ MI |          |

\*\*\* HYDROGRAPH AT STATION BASIN2  
FOR PLAN 1, RATIO = 5.60

|           |       |      |                              |          |
|-----------|-------|------|------------------------------|----------|
| PEAK FLOW | TIME  | 6-HR | MAXIMUM AVERAGE FLOW         | 29.90-HR |
| + (CFS)   | (HR)  |      | 24-HR                        | 72-HR    |
|           | 12.40 |      | 0.                           | 0.       |
|           |       |      | 2.847                        | 2.983    |
|           |       |      | CUMULATIVE AREA = 0.00 SQ MI |          |

|              |       |        |                              |          |
|--------------|-------|--------|------------------------------|----------|
| PEAK STORAGE | TIME  | 6-HR   | MAXIMUM AVERAGE STORAGE      | 29.90-HR |
| + (AC-FT)    | (HR)  | 0.     | 24-HR                        | 72-HR    |
|              | 12.40 |        | 0.                           | 0.       |
| PEAK STAGE   | TIME  | 6-HR   | MAXIMUM AVERAGE STAGE        | 29.90-HR |
| + (FEET)     | (HR)  | 285.16 | 24-HR                        | 72-HR    |
|              | 12.40 |        | 284.66                       | 284.53   |
|              |       |        | CUMULATIVE AREA = 0.00 SQ MI |          |

\*\*\* HYDROGRAPH AT STATION BASIN2  
FOR PLAN 1, RATIO = 7.30

|           |       |      |                              |          |
|-----------|-------|------|------------------------------|----------|
| PEAK FLOW | TIME  | 6-HR | MAXIMUM AVERAGE FLOW         | 29.90-HR |
| + (CFS)   | (HR)  |      | 24-HR                        | 72-HR    |
|           | 12.40 |      | 1.                           | 0.       |
|           |       |      | 3.125                        | 4.227    |
|           |       |      | CUMULATIVE AREA = 0.00 SQ MI |          |

|              |       |        |                              |          |
|--------------|-------|--------|------------------------------|----------|
| PEAK STORAGE | TIME  | 6-HR   | MAXIMUM AVERAGE STORAGE      | 29.90-HR |
| + (AC-FT)    | (HR)  | 0.     | 24-HR                        | 72-HR    |
|              | 12.40 |        | 0.                           | 0.       |
| PEAK STAGE   | TIME  | 6-HR   | MAXIMUM AVERAGE STAGE        | 29.90-HR |
| + (FEET)     | (HR)  | 285.31 | 24-HR                        | 72-HR    |
|              | 12.40 |        | 284.81                       | 284.66   |
|              |       |        | CUMULATIVE AREA = 0.00 SQ MI |          |



+ (CFS) (HR) 6-HR 24-HR 72-HR 29.90-HR  
 + 0. 0.10 (CFS) 0. 0. 0. 0.  
 (INCHES) 0.000 0.000 0.000 0.000  
 (AC-FT) 0. 0. 0. 0.  
 CUMULATIVE AREA = 0.00 SQ MI

\*\*\* HYDROGRAPH AT STATION SUB-10  
 FOR PLAN 1, RATIO = 3.20  
 TOTAL RAINFALL = 3.20, TOTAL LOSS = 2.65, TOTAL EXCESS = 0.55

PEAK FLOW TIME 6-HR 24-HR 72-HR 29.90-HR  
 (CFS) (HR) (CFS) (HR) (CFS) (HR) (CFS) (HR)  
 + 0. 12.30 0. 0. 0. 0. 0. 0.  
 (INCHES) 0.444 0.546 0.546 0.546  
 (AC-FT) 0. 0. 0. 0.

CUMULATIVE AREA = 0.00 SQ MI  
 \*\*\* HYDROGRAPH AT STATION SUB-10  
 FOR PLAN 1, RATIO = 4.20

TOTAL RAINFALL = 4.20, TOTAL LOSS = 3.16, TOTAL EXCESS = 1.04

PEAK FLOW TIME 6-HR 24-HR 72-HR 29.90-HR  
 (CFS) (HR) (CFS) (HR) (CFS) (HR) (CFS) (HR)  
 + 0. 12.30 0. 0. 0. 0. 0. 0.  
 (INCHES) 0.855 1.038 1.038 1.038  
 (AC-FT) 0. 0. 0. 0.

CUMULATIVE AREA = 0.00 SQ MI  
 \*\*\* HYDROGRAPH AT STATION SUB-10  
 FOR PLAN 1, RATIO = 5.00

TOTAL RAINFALL = 5.00, TOTAL LOSS = 3.50, TOTAL EXCESS = 1.50

PEAK FLOW TIME 6-HR 24-HR 72-HR 29.90-HR  
 (CFS) (HR) (CFS) (HR) (CFS) (HR) (CFS) (HR)  
 + 0. 12.30 0. 0. 0. 0. 0. 0.  
 (INCHES) 1.237 1.500 1.500 1.500  
 (AC-FT) 0. 0. 0. 0.

CUMULATIVE AREA = 0.00 SQ MI  
 \*\*\* HYDROGRAPH AT STATION SUB-10

FOR PLAN 1, RATIO = 5.60

TOTAL RAINFALL = 5.60, TOTAL LOSS = 3.72, TOTAL EXCESS = 1.88

| PEAK FLOW TIME | 6-HR  | 24-HR | 72-HR | 29.90-HR |
|----------------|-------|-------|-------|----------|
| (CFS)          | 0.    | 0.    | 0.    | 0.       |
| (INCHES)       | 1.548 | 1.878 | 1.878 | 1.878    |
| (AC-FT)        | 0.    | 0.    | 0.    | 0.       |

CUMULATIVE AREA = 0.00 SQ MI

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HYDROGRAPH AT STATION SUB-10  
FOR PLAN 1, RATIO = 7.30

TOTAL RAINFALL = 7.30, TOTAL LOSS = 4.24, TOTAL EXCESS = 3.06

| PEAK FLOW TIME | 6-HR  | 24-HR | 72-HR | 29.90-HR |
|----------------|-------|-------|-------|----------|
| (CFS)          | 0.    | 0.    | 0.    | 0.       |
| (INCHES)       | 2.515 | 3.061 | 3.061 | 3.061    |
| (AC-FT)        | 0.    | 0.    | 0.    | 0.       |

CUMULATIVE AREA = 0.00 SQ MI

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194 KK \* comb \* COMBINE HYDROGRAPHS COMB-1, SITE-3 & OFF-3

195 HC HYDROGRAPH COMBINATION 5 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION comb  
FOR PLAN 1, RATIO = 3.20

| PEAK FLOW TIME | 6-HR  | 24-HR | 72-HR | 29.90-HR |
|----------------|-------|-------|-------|----------|
| (CFS)          | 1.    | 0.    | 0.    | 0.       |
| (INCHES)       | 0.563 | 0.821 | 0.854 | 0.854    |
| (AC-FT)        | 1.    | 1.    | 1.    | 1.       |

CUMULATIVE AREA = 0.02 SQ MI

\*\*\* \*\*

HYDROGRAPH AT STATION Comb  
FOR PLAN 1, RATIO = 4.20

| PEAK FLOW | TIME  | 6-HR                         | 24-HR                | 72-HR | 29.90-HR |
|-----------|-------|------------------------------|----------------------|-------|----------|
| (CFS)     | (HR)  |                              | MAXIMUM AVERAGE FLOW |       |          |
| +         | 11.   | 2.                           | 1.                   | 1.    | 1.       |
|           | 12.40 | 0.966                        | 1.310                | 1.345 | 1.345    |
|           |       | 1.                           | 1.                   | 1.    | 1.       |
|           |       | CUMULATIVE AREA = 0.02 SQ MI |                      |       |          |

\*\*\* \*\*

HYDROGRAPH AT STATION Comb  
FOR PLAN 1, RATIO = 5.00

| PEAK FLOW | TIME  | 6-HR                         | 24-HR                | 72-HR | 29.90-HR |
|-----------|-------|------------------------------|----------------------|-------|----------|
| (CFS)     | (HR)  |                              | MAXIMUM AVERAGE FLOW |       |          |
| +         | 15.   | 3.                           | 1.                   | 1.    | 1.       |
|           | 12.40 | 1.339                        | 1.761                | 1.798 | 1.798    |
|           |       | 1.                           | 2.                   | 2.    | 2.       |
|           |       | CUMULATIVE AREA = 0.02 SQ MI |                      |       |          |

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HYDROGRAPH AT STATION Comb  
FOR PLAN 1, RATIO = 5.60

| PEAK FLOW | TIME  | 6-HR                         | 24-HR                | 72-HR | 29.90-HR |
|-----------|-------|------------------------------|----------------------|-------|----------|
| (CFS)     | (HR)  |                              | MAXIMUM AVERAGE FLOW |       |          |
| +         | 19.   | 4.                           | 1.                   | 1.    | 1.       |
|           | 12.40 | 1.641                        | 2.128                | 2.167 | 2.167    |
|           |       | 2.                           | 2.                   | 2.    | 2.       |
|           |       | CUMULATIVE AREA = 0.02 SQ MI |                      |       |          |

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HYDROGRAPH AT STATION Comb  
FOR PLAN 1, RATIO = 7.30

| PEAK FLOW | TIME  | 6-HR                         | 24-HR                | 72-HR | 29.90-HR |
|-----------|-------|------------------------------|----------------------|-------|----------|
| (CFS)     | (HR)  |                              | MAXIMUM AVERAGE FLOW |       |          |
| +         | 29.   | 6.                           | 2.                   | 1.    | 1.       |
|           | 12.40 | 2.579                        | 3.272                | 3.316 | 3.316    |
|           |       | 3.                           | 4.                   | 4.    | 4.       |
|           |       | CUMULATIVE AREA = 0.02 SQ MI |                      |       |          |

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\*\*\*\*\*  
 \* RTRV \*  
 \* \*\*\*\*\*  
 \* \*\*\*\*\*  
 \* \*\*\*\*\*

RETRIEVE FLOW DIVERTED TO POINT OF INTEREST 'B'

198 DR RETRIEVE DIVERSION HYDROGRAPH  
 ISTDAD TO PTA DIVERSION HYDROGRAPH IDENTIFICATION

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HYDROGRAPH AT STATION RTRV  
 FOR PLAN 1, RATIO = 3.20

| PEAK FLOW | TIME  | 6-HR                         | 24-HR | 72-HR | 29.90-HR |
|-----------|-------|------------------------------|-------|-------|----------|
| (CFS)     |       |                              |       |       |          |
| +         | 12.60 | 1.                           | 0.    | 0.    | 0.       |
|           |       | 0.245                        | 0.411 | 0.438 | 0.438    |
|           |       | 0.                           | 0.    | 0.    | 0.       |
|           |       | CUMULATIVE AREA = 0.00 SQ MI |       |       |          |

\*\*\*

HYDROGRAPH AT STATION RTRV  
 FOR PLAN 1, RATIO = 4.20

| PEAK FLOW | TIME  | 6-HR                         | 24-HR | 72-HR | 29.90-HR |
|-----------|-------|------------------------------|-------|-------|----------|
| (CFS)     |       |                              |       |       |          |
| +         | 12.60 | 1.                           | 0.    | 0.    | 0.       |
|           |       | 0.437                        | 0.634 | 0.661 | 0.661    |
|           |       | 0.                           | 1.    | 1.    | 1.       |
|           |       | CUMULATIVE AREA = 0.00 SQ MI |       |       |          |

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HYDROGRAPH AT STATION RTRV  
 FOR PLAN 1, RATIO = 5.00

| PEAK FLOW | TIME  | 6-HR                         | 24-HR | 72-HR | 29.90-HR |
|-----------|-------|------------------------------|-------|-------|----------|
| (CFS)     |       |                              |       |       |          |
| +         | 12.60 | 1.                           | 0.    | 0.    | 0.       |
|           |       | 0.618                        | 0.839 | 0.866 | 0.866    |
|           |       | 1.                           | 1.    | 1.    | 1.       |
|           |       | CUMULATIVE AREA = 0.00 SQ MI |       |       |          |

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HYDROGRAPH AT STATION RTRV  
 FOR PLAN 1, RATIO = 5.60

| PEAK FLOW | TIME  | 6-HR                         | 24-HR | 72-HR | 29.90-HR |
|-----------|-------|------------------------------|-------|-------|----------|
| (CFS)     |       |                              |       |       |          |
| +         | 12.60 | 1.                           | 0.    | 0.    | 0.       |
|           |       | 0.618                        | 0.839 | 0.866 | 0.866    |
|           |       | 1.                           | 1.    | 1.    | 1.       |
|           |       | CUMULATIVE AREA = 0.00 SQ MI |       |       |          |

\*\*\*

```

+ (CFS) (HR) (CFS) (CFS) (CFS) (CFS)
+ 5. 12.60 (INCHES) 0.764 2. 1. 1. 0. 0.
  (AC-FT) 1. 1.032 1. 1. 1.032 1.
  CUMULATIVE AREA = 0.00 SQ MI
***

```

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***
HYDROGRAPH AT STATION PT-A
FOR PLAN 1, RATIO = 7.30
***
PEAK FLOW TIME 6-HR 24-HR 72-HR 29.90-HR
(CFS) (HR) (CFS)
+ 12. 12.50 (CFS) 3. 1. 1. 1.
  (INCHES) 1.199 1.517 1.544 1.544
  (AC-FT) 1. 2. 2.
  CUMULATIVE AREA = 0.00 SQ MI

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199 KK PT-A * COMBINE HYDROGRAPHS COMB-1, SITE-3 & OFF-3
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200 HC HYDROGRAPH COMBINATION 2 NUMBER OF HYDROGRAPHS TO COMBINE
ICOMP *****

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***
HYDROGRAPH AT STATION PT-A
FOR PLAN 1, RATIO = 3.20
***
PEAK FLOW TIME 6-HR 24-HR 72-HR 29.90-HR
(CFS) (HR) (CFS)
+ 8. 12.40 (CFS) 2. 1. 1. 1.
  (INCHES) 0.807 1.227 1.292 1.292
  (AC-FT) 1. 1. 1.
  CUMULATIVE AREA = 0.02 SQ MI

```

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***
HYDROGRAPH AT STATION PT-A
FOR PLAN 1, RATIO = 4.20
***
PEAK FLOW TIME 6-HR 24-HR 72-HR 29.90-HR
(CFS) (HR) (CFS)
+ 14. 12.40 (CFS) 3. 1. 1. 1.

```

(INCHES) 1.402 1.935 2.006 2.006  
 (AC-FT) 2. 2. 2. 2.

CUMULATIVE AREA = 0.02 SQ MI

\*\*\* \*\*  
 HYDROGRAPH AT STATION PT-A  
 FOR PLAN 1, RATIO = 5.00  
 MAXIMUM AVERAGE FLOW 29.90-HR  
 6-HR 24-HR 72-HR  
 (CFS) 4. 1. 1. 1.  
 (INCHES) 1.954 2.589 2.664 2.664  
 (AC-FT) 2. 3. 3. 3.  
 CUMULATIVE AREA = 0.02 SQ MI

\*\*\* \*\*  
 HYDROGRAPH AT STATION PT-A  
 FOR PLAN 1, RATIO = 5.60  
 MAXIMUM AVERAGE FLOW 29.90-HR  
 6-HR 24-HR 72-HR  
 (CFS) 5. 2. 1. 1.  
 (INCHES) 2.401 3.122 3.198 3.198  
 (AC-FT) 3. 3. 3. 3.  
 CUMULATIVE AREA = 0.02 SQ MI

\*\*\* \*\*  
 HYDROGRAPH AT STATION PT-A  
 FOR PLAN 1, RATIO = 7.30  
 MAXIMUM AVERAGE FLOW 29.90-HR  
 6-HR 24-HR 72-HR  
 (CFS) 8. 3. 2. 2.  
 (INCHES) 3.774 4.778 4.860 4.860  
 (AC-FT) 4. 5. 5. 5.  
 CUMULATIVE AREA = 0.02 SQ MI

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 VOLUME IN ACRE-FEET, TIME TO PEAK IN HOURS

| OPERATION | STATION | AREA  | PLAN | RATIOS APPLIED TO PRECIPITATION |         |         |         |         |
|-----------|---------|-------|------|---------------------------------|---------|---------|---------|---------|
|           |         |       |      | RATIO 1                         | RATIO 2 | RATIO 3 | RATIO 4 | RATIO 5 |
| +         | SUB-2   | 0.000 | 1    | 0.17                            | 0.23    | 0.28    | 0.32    | 0.44    |
|           |         |       |      | 12.20                           | 12.20   | 12.20   | 12.20   | 12.20   |
|           |         |       |      | 3.20                            | 4.20    | 5.00    | 5.60    | 7.30    |



